

— PHYSICS

Future king, the king of future stationary. NOTEBOOK

Future King

塞下秋来风景异

衡阳雁去无留意

四面边声连角起

千嶂里

长烟落日孤城闭

浊酒一杯家万里

燕然未勒归无计

羌管悠悠霜满地

人不寐

将军白发征夫泪

No.

Date

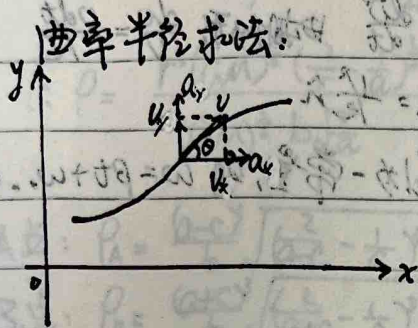
刘昂立

一. 牛顿力学

1. 运动、动力学

① 位置: $\vec{r} = r - r_0$, $v = \frac{d\vec{r}}{dt}$, $\vec{a} = \frac{d\vec{v}}{dt} = \frac{d^2\vec{r}}{dt^2}$: 加速度
 (自然系中 $\vec{a} = \frac{dv_x}{dt}\vec{e}_x + \frac{dv_y}{dt}\vec{e}_y$)

② 角量: $\theta = \varphi_2 - \varphi_1$, $\omega = \frac{d\theta}{dt}$, $\beta = \frac{d\omega}{dt} = \frac{d^2\theta}{dt^2}$, $\vec{v} = \vec{\omega} \times \vec{r}$



$$\rho = \frac{ds}{d\theta} = \frac{|\vec{r}^2|}{|\vec{a} \times \vec{v}|} = \frac{v^2}{a_n}$$

$$\Rightarrow v = \sqrt{(dx)^2 + (dy)^2}$$

$$a_n = a_x \sin\theta - a_y \cos\theta = \frac{d^2x}{dt^2} \frac{dy}{dx} - \frac{d^2y}{dt^2} \frac{1}{\sqrt{1 + (\frac{dy}{dx})^2}}$$

$$= \frac{d(\frac{dx}{dt})}{dt} \frac{dy}{\sqrt{(dx)^2 + (dy)^2}} - \frac{d(\frac{dy}{dt})}{dt} \frac{dx}{\sqrt{(dx)^2 + (dy)^2}}$$

$$\therefore \rho = \frac{v^2}{a_n} = \frac{(dx)^2 + (dy)^2}{(\frac{dx}{dt})^2}$$

$$= \frac{1}{\frac{d}{dt} \sqrt{(dx)^2 + (dy)^2}} \left[d\left(\frac{dx}{dt}\right) dy - \frac{dx}{dt} d\left(\frac{dy}{dt}\right) \right]$$

$$= \frac{[(dx)^2 + (dy)^2]^{\frac{3}{2}}}{dt \left[d\left(\frac{dx}{dt}\right) dy - \frac{dx}{dt} d\left(\frac{dy}{dt}\right) \right]}$$

$$= \frac{[(dx)^2 + (dy)^2]^{\frac{3}{2}}}{d\left(\frac{dy}{dx}\right) (dx)^2}$$

对于椭圆 $\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1$, 有

$$\rho = \frac{[(dx)^2 + \frac{b^2}{a^2} \frac{x^2 dx^2}{a^2 x^2}]^{\frac{3}{2}}}{\frac{b}{a} \left(\sqrt{a^2 - x^2} + \frac{x^2}{a^2 - x^2} \right) dx (dx)^2} = \frac{(1 + \frac{b^2}{a^2} \frac{x^2}{a^2 x^2})^{\frac{3}{2}}}{\frac{b}{a} \frac{a^2}{(a^2 - x^2)^{\frac{3}{2}}}} = \frac{(a^2 - x^2)^{\frac{3}{2}}}{a^2 b} \begin{cases} x=0 \text{ 时}, \rho = \frac{a^2}{b} \\ x=a \text{ 时}, \rho = \frac{b^2}{a} \end{cases}$$

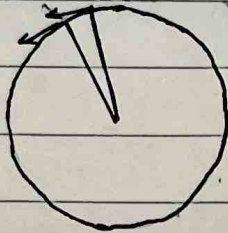
运动学

③ 典例:

1) 匀速直线: $\vec{s} = \vec{v}t = \vec{v}t$

2) 匀加速直线: $\vec{v} = \vec{a}t + \vec{v}_0$; $\vec{s} = \int \vec{v} dt = \vec{s}_0 + \vec{v}_0 t + \frac{1}{2} \vec{a} t^2$

3) 圆周: $\vec{v} = \vec{\omega} \times \vec{r}$; $\vec{a} = \frac{d\vec{v}}{dt}$

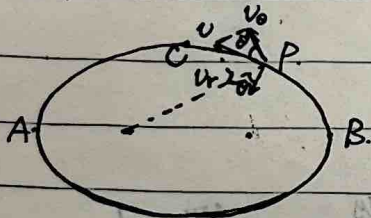


$\vec{a}_n = \frac{dv}{dt}$ 由相似形 $\frac{dv}{v} = \frac{v dt}{R}$

$\therefore \vec{a}_n = \frac{v^2}{R} \hat{n}$

若 $|\vec{a}_n|$ 为常量, 则 $\omega = \beta t + \omega_0$, $\theta = \theta_0 + \omega t + \frac{1}{2} \beta t^2$

4) $F = \frac{GMm}{r^2}$ 的椭圆



$\frac{v_t}{v_r} = \frac{r \frac{d\theta}{dt}}{\frac{dr}{dt}} = \frac{r \dot{\theta}}{\dot{r}} = q$

$\frac{r^2 \dot{\theta}}{r \dot{r}} = q$

设 v_t 为横向速度, v_r 为径向速度.

$L = m v_t r$

$E = \frac{1}{2} m v^2 - \frac{GMm}{r} = \frac{1}{2} m (v_t^2 + v_r^2) - \frac{GMm}{r}$

在 AB 两处, $v_r = 0$, $v_t = \frac{L}{mr}$

$\therefore E = \frac{1}{2} m \frac{L^2}{m^2 r_0^2} - \frac{GMm}{r_0}$ 整理得 $r_0^3 + \frac{GMm}{E} r_0 - \frac{L^2}{2mE} = 0$

又: 在 AB 两 $r_0 = a+c$ 或 $a-c$

$\therefore \begin{cases} r_1 + r_2 = 2a = -\frac{GMm}{E} \\ r_1 \cdot r_2 = a^2 - c^2 = b^2 = -\frac{L^2}{2mE} \end{cases}$

解得 $\begin{cases} E = -\frac{GMm}{2a} \\ L = mb \sqrt{\frac{GM}{a}} \end{cases} \Rightarrow \begin{cases} a = -\frac{GMm}{2E} \\ b = \sqrt{-\frac{L^2}{2mE}} \end{cases}$

故椭圆方程为 $\frac{x^2}{(-\frac{GMm}{2E})} + \frac{y^2}{(-\frac{L^2}{2mE})} = 1$

曲率半径:

$$\frac{GMm}{r^2} \cos\theta = m \frac{v^2}{\rho}$$

$$\text{而 } m v \cos\theta r = m b \sqrt{\frac{GM}{a}}, \quad \therefore \cos\theta = \frac{b}{r} \sqrt{\frac{GM}{a}}$$

$$\therefore \rho = \frac{r^2 v^2}{GM \cos\theta} = \frac{r^2 v^2}{GM b \sqrt{\frac{GM}{a}}}$$

$$\text{而 } \frac{1}{2} m v^2 - \frac{GMm}{r} = -\frac{GMm}{2a}, \quad \therefore v = \sqrt{GM} \sqrt{\frac{2}{r} - \frac{1}{a}}$$

$$\therefore \rho = \frac{r^3 (GM)^{\frac{3}{2}} \left(\frac{2}{r} - \frac{1}{a}\right)^{\frac{3}{2}}}{(GM)^{\frac{3}{2}} b \sqrt{a}} = \frac{r^3}{b} \sqrt{\left(\frac{2}{r} - \frac{1}{a}\right)^3 a}$$

$$A \text{ 点: } \rho_A = \frac{(a-c)^3}{b} \sqrt{\left(\frac{2}{a-c} - \frac{1}{a}\right)^3 a} = \frac{(a-c)^3}{ab} \sqrt{\frac{(a+c)^3}{(a-c)^3}} = \frac{b^2}{a}$$

$$B \text{ 点: } \rho_B = \frac{(a+c)^3}{b} \sqrt{\left(\frac{2}{a+c} - \frac{1}{a}\right)^3 a} = \frac{(a+c)^3}{ab} \sqrt{\frac{(a-c)^3}{(a+c)^3}} = \frac{b^2}{a}$$

$$C \text{ 点: } \rho_C = \frac{a^3}{b} \sqrt{\left(\frac{2}{a} - \frac{1}{a}\right)^3 a} = \frac{a^2}{b}$$

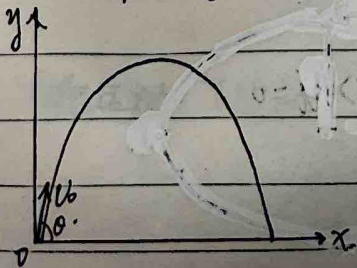
周期: 由于单位时间矢径扫过的面积 $\frac{ds}{dt} = \frac{1}{2} |\mathbf{r} \times \mathbf{v}| \cdot dt/dt = \frac{1}{2} r v \sin\theta = \frac{1}{2} r v \cos\theta$

$$\therefore \cos\theta = \frac{b}{r} \sqrt{\frac{GM}{a}}$$

$$\therefore \frac{ds}{dt} = \frac{1}{2} r v \frac{b}{r} \sqrt{\frac{GM}{a}} = \frac{1}{2} \sqrt{\frac{GM}{a}}$$

$$\therefore \pi a b = \frac{1}{2} \sqrt{\frac{GM}{a}} \quad \therefore T = 2\pi \sqrt{\frac{a^3}{GM}}$$

5) 抛体运动:



$$u_x = v_0 \cos\theta_0, \quad u_y = v_0 \sin\theta_0 - gt$$

$$x = v_0 \cos\theta_0 t, \quad y = v_0 \sin\theta_0 t - \frac{1}{2} g t^2$$

$$\text{射程 } x = \frac{v_0^2 \sin 2\theta_0}{g}, \quad \text{射高 } y = \frac{v_0^2 \sin^2 \theta_0}{2g}$$

轨道方程: $x = v_0 \cos\theta_0 t$ 和 $y = v_0 \sin\theta_0 t - \frac{1}{2} g t^2$ (消去 t 得)

$$y = -\frac{g}{2v_0^2 \cos^2 \theta_0} x^2 - \frac{g}{\sin 2\theta_0} x = -\frac{g(1+\tan^2 \theta_0)}{2v_0^2} x^2 + \tan \theta_0 x$$

此方程中参数有 x, y, v_0, θ_0 (已知可求四, 知二可求最)

$$\text{曲率半径: } \rho = \frac{v^2}{a_n} = \frac{v_0^2 - 2v_0 g \sin\theta_0 t + g^2 t^2}{g \sqrt{v_x^2 + v_y^2}} = \frac{v_0^2 - 2v_0 g \sin\theta_0 t + g^2 t^2}{g \cdot v_0 \cos\theta_0}$$

包络线方程1: 各初速度各方向.

最高点 $\begin{cases} x = \frac{v_0^2 \sin 2\theta}{2g} \\ y = \frac{v_0^2 \sin^2 \theta}{2g} = \frac{v_0^2}{4g} (1 - \cos 2\theta) \end{cases}$

消去 θ , 得 $(\frac{2g}{v_0^2} x)^2 + (1 - \frac{4g}{v_0^2} y)^2 = 1$

变形得 $\frac{x^2}{(\frac{v_0^2}{2g})^2} + \frac{(y - \frac{v_0^2}{4g})^2}{(\frac{v_0^2}{4g})^2} = 1$

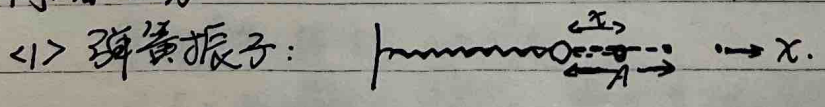
中心坐标 $(0, \frac{v_0^2}{4g})$, $a = \frac{v_0^2}{2g}$, $b = \frac{v_0^2}{4g}$

包络线方程2: 同方向, 各初速度.

最高点 $\begin{cases} x = \frac{v_0^2 \sin 2\theta}{2g} \\ y = \frac{v_0^2}{4g} (1 - \cos 2\theta) \end{cases}$

消去 v_0^2 , $\frac{y}{x} = \frac{1}{2} \frac{1 - \cos 2\theta}{\sin 2\theta} = \frac{1}{2} \tan \theta$

6) 简谐运动.



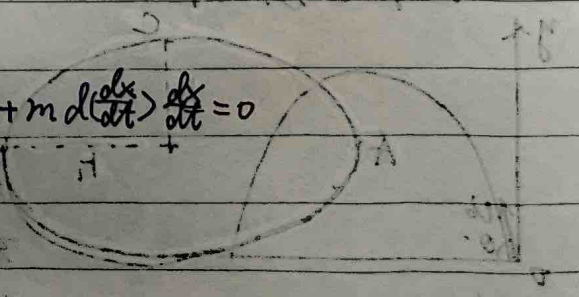
$\vec{F} = -k\vec{x} = m \frac{d^2\vec{x}}{dt^2}$
 $\therefore kx + m \frac{d^2x}{dt^2} = 0$

积分得 $\frac{1}{2} kx^2 - \frac{1}{2} kA^2 + \frac{1}{2} m (\frac{dx}{dt})^2 = 0$

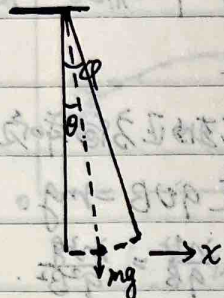
$\frac{dx}{\sqrt{A^2 - x^2}} = \sqrt{\frac{k}{m}} dt$

令 $x = A \cos \theta$, 代入上式得 $\theta = \sqrt{\frac{k}{m}} t$, $\therefore x = A \cos(\sqrt{\frac{k}{m}} t) \Rightarrow T = 2\pi \sqrt{\frac{m}{k}}$

$\begin{cases} v = \frac{dx}{dt} = -A \sqrt{\frac{k}{m}} \sin(\sqrt{\frac{k}{m}} t) \\ a = \frac{dv}{dt} = -A \frac{k}{m} \cos(\sqrt{\frac{k}{m}} t) \end{cases}$



12) 单摆



$$\begin{cases} \vec{F} = -mg\vec{e}_r \times -mg\vec{e}_z = m\frac{d\vec{v}}{dt} \\ mgl(1-\cos\varphi) = \frac{1}{2}mv^2 + mgl(1-\cos\varphi) \end{cases}$$

$$\therefore v = \sqrt{2gl(\cos\theta - \cos\varphi)} \approx \sqrt{gl(\varphi^2 - \theta^2)}$$

令 $\theta = \varphi \cos\alpha$, 代入上式得 $v = \sqrt{gl} \varphi \sin\alpha$

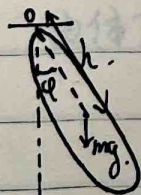
$$\therefore dv = -\frac{\sqrt{gl} \varphi d\alpha}{\sqrt{\varphi^2 - \theta^2}} \quad \varphi dv = -g\theta dt$$

$$\therefore dt = \sqrt{\frac{g}{l}} \frac{d\alpha}{\sqrt{\varphi^2 - \theta^2}} = \sqrt{\frac{g}{l}} \frac{d\alpha}{\varphi \sin\alpha} = \sqrt{\frac{g}{l}} \frac{-\varphi \cos\alpha d\alpha}{\varphi \sin\alpha} = -\sqrt{\frac{g}{l}} d\alpha$$

$\therefore \alpha = -\sqrt{\frac{g}{l}} \cdot t$ (代入前式得)

$$\begin{cases} \theta = \varphi \cos\sqrt{\frac{g}{l}} t \\ v = -\varphi \sqrt{gl} \sin\sqrt{\frac{g}{l}} t \\ a = -\varphi g \cos\sqrt{\frac{g}{l}} t \end{cases} \Rightarrow T = 2\pi\sqrt{\frac{l}{g}}$$

13) 复摆

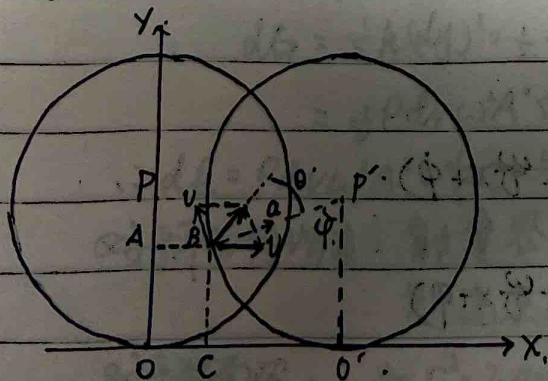


$$m \times -mgh\theta = I \frac{d\omega}{dt}$$

$$mgh(1-\cos\varphi) = \frac{1}{2}I\omega^2 + mgh(1-\cos\varphi)$$

同理 $T = 2\pi\sqrt{\frac{I}{mgh}}$

14) 圆轮运动: (纯滚)



在梯形 ABPP' 中: $AB = x = PP' - R\sin\varphi = R(\varphi - \sin\varphi)$

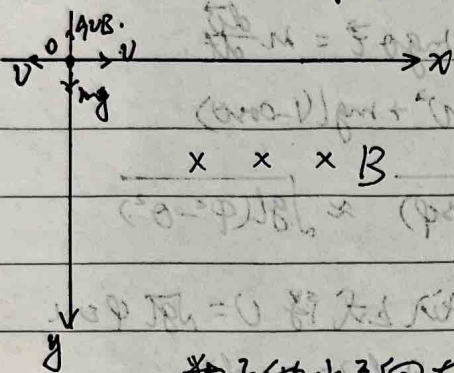
在梯形 BCOP' 中: $BC = y = PO' - R\cos\varphi = R(1 - \cos\varphi)$

曲率半径: $a = \frac{d|\vec{v}|}{dt} + v\frac{d\theta}{dt}$

$$\frac{d|\vec{v}|}{dt} = \frac{v^2}{R} \quad \text{而 } v_{\text{合}}^2 = 2v^2(1 + \cos\varphi)$$

$$\therefore \rho = \frac{2v^2(1 + \cos\varphi)}{\frac{v^2}{R} \sin\varphi} = \frac{2v^2(1 + \cos\varphi)}{\frac{v^2}{R} \sin\varphi} = 4R \frac{\cos^2\frac{\varphi}{2}}{\sin\varphi}$$

8). 重力场与磁场结合问题.



质量为 m , 带电量为 $+q$ 的粒子从原点
无初速度释放.

给粒子附加沿 x 轴正方向和负方向
各一个速度 v , 使 $qvB = mg$.

$$v = \frac{mg}{qB}, \quad R = \frac{mv}{qB} = \frac{m^2g}{q^2B^2}$$

粒子做水平向右匀速直线运动和匀速圆周运动.

$$x = vt - R\omega t, \quad y = R - R\cos\omega t$$

$$v = \frac{mg}{qB} = \frac{qBR}{m}, \quad \omega = \frac{v}{R} = \frac{qB}{m}$$

$$\begin{cases} x = \frac{mg}{qB}t - R\omega\left(\frac{qB}{m}t\right) = \frac{mg}{qB}t - \frac{m^2g}{q^2B^2}\omega\left(\frac{qB}{m}t\right) \\ y = R - R\cos\left(\frac{qB}{m}t\right) = \frac{m^2g}{q^2B^2} - \frac{m^2g}{q^2B^2}\cos\left(\frac{qB}{m}t\right) \end{cases}$$

9) 波动.

横波: 振动方向与传播方向垂直 (固体中传播)

纵波: 振动方向与传播方向相同 (液体、气体中传播)

$$y(x, t) = A\cos(\omega t - \frac{\omega}{v}x + \varphi)$$

$$= A\cos(\omega t - kx + \varphi) \quad k: \text{波矢.}$$

$$= A\cos 2\pi\left(\frac{t}{T} - \frac{x}{\lambda} + \frac{\varphi}{2\pi}\right)$$

当 $x = x_0$ 时, 方程表示该点振动方程.

$$y(t) = A\cos(\omega t - \frac{\omega}{v}x_0 + \varphi)$$

当 $t = t_0$ 时, 方程表示该时刻波形.

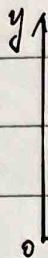
$$y(x) = A\cos(\omega t_0 - \frac{\omega}{v}x + \varphi)$$

$$\langle 1 \rangle \text{ 波速: } \frac{\partial y(x, t)}{\partial t} = -\omega A\sin(\omega t - \frac{\omega}{v}x + \varphi)$$

$$\frac{\partial^2 y(x, t)}{\partial x^2} = -\frac{\omega^2}{v^2} A\cos(\omega t - \frac{\omega}{v}x + \varphi)$$

$$\frac{\partial^2 y}{\partial t^2} = v^2 \frac{\partial^2 y}{\partial x^2}$$

轻质柔弦的横波方程:



$$\begin{cases} T_2 \sin \alpha_2 - T_1 \sin \alpha_1 = \rho ds \frac{\partial^2 y}{\partial t^2} \\ T_2 \cos \alpha_2 - T_1 \cos \alpha_1 = 0 \end{cases}$$

$$\begin{cases} \cos \alpha_1 \approx \cos \alpha_2 \approx 1 \\ \sin \alpha_1 \approx \tan \alpha_1 = \left. \frac{\partial y}{\partial x} \right|_x, \quad \sin \alpha_2 \approx \tan \alpha_2 = \left. \frac{\partial y}{\partial x} \right|_{x+dx} \end{cases}$$

$$\therefore \frac{\partial^2 y}{\partial t^2} = \frac{T}{\rho} \frac{\partial^2 y}{\partial x^2}$$

$$\therefore v = \sqrt{\frac{T}{\rho}}$$

稀薄气体中的声速:

气体可以在传播过程中经历绝热过程. $PV^\gamma = C$

$$\therefore V^\gamma dp + \gamma PV^{\gamma-1} dV = 0 \Rightarrow \frac{dp}{p} = -\gamma \frac{dV}{V}$$

由体变模量定义, $dp = -B \frac{dV}{V} \Rightarrow B = -V \frac{dp}{dV} = \gamma P$

$$\therefore v = \sqrt{\frac{B}{\rho}} = \sqrt{\frac{\gamma P}{\rho}} = \sqrt{\frac{\gamma RT}{M}}$$

② 波的能量和能流

$$\left\{ \begin{array}{l} \text{动能: } dE_k = \frac{1}{2} dm \cdot v^2 = \frac{1}{2} \rho dV \left(\frac{\partial y}{\partial t} \right)^2 = \frac{1}{2} \rho dV \omega^2 A^2 \sin^2(\omega t - \frac{\omega}{v} x) \\ \text{势能: } \frac{dE_p}{dV} = Y \frac{dy}{dx} \Rightarrow F = \frac{Ys}{dx} dy = k dy \end{array} \right.$$

$$dE_p = \frac{1}{2} k (dy)^2 = \frac{1}{2} \frac{Ys}{dx} (dy)^2 = \frac{1}{2} \left(\frac{dy}{dx} \right)^2 (s dx) Y = \frac{1}{2} \left(\frac{dy}{dx} \right)^2 Y dV$$

$$= \frac{1}{2} \rho dV \omega^2 A^2 \sin^2(\omega t - \frac{\omega}{v} x)$$

$$\therefore dE = \rho dV \omega^2 A^2 \sin^2(\omega t - \frac{\omega}{v} x)$$

对于平面简谐波: 能量密度 $\epsilon = \frac{dE}{dV} = \rho \omega^2 A^2 \sin^2(\omega t - \frac{\omega}{v} x)$

(1) 能流密度 $\vec{I} = \epsilon \vec{v}$, $I = \bar{\epsilon} v = \frac{1}{2} \rho A^2 \omega^2 v$

对于平面波: $I_1 = 4\pi r_1^2 = I_2 = 4\pi r_2^2$, $\therefore \frac{I_1}{I_2} = \frac{r_2^2}{r_1^2} = \frac{A_2^2}{A_1^2}$, $\therefore y = \frac{A_0 r_0}{r} \cos(\omega t - kr)$

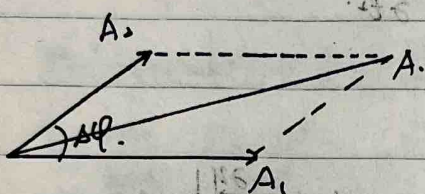
③ 波的干涉:

$$y_1(x, t) = A_1 \cos(\omega t - \frac{\omega}{v}x_1 + \varphi_1)$$

$$y_2(x, t) = A_2 \cos(\omega t - \frac{\omega}{v}x_2 + \varphi_2)$$

在某点P, 两列波的合成仍为简谐运动, 有

$$y(t) = y_1(x, t) + y_2(x, t) = A \cos(\omega t + \varphi)$$



$$\Delta\varphi = (\varphi_1 - \varphi_2) - \frac{2\pi}{\lambda}(x_1 - x_2)$$

$$A = \sqrt{A_1^2 + A_2^2 + 2A_1A_2 \cos \Delta\varphi}$$

当 $\Delta\varphi = 2k\pi$ 时, 干涉相长, $A = A_1 + A_2$.

当 $\Delta\varphi = (2k+1)\pi$ 时, 干涉相消, $A = |A_1 - A_2|$.

④ 驻波: 实质为波的干涉

左行波 $y_1(x, t) = A \cos(\omega t + \frac{2\pi x}{\lambda})$

右行波 $y_2(x, t) = A \cos(\omega t - \frac{2\pi x}{\lambda})$

$$\therefore y(x, t) = y_1(x, t) + y_2(x, t) = 2A \cos \frac{2\pi x}{\lambda} \cos \omega t$$

当 $\frac{2\pi x}{\lambda} = k\pi$, 即 $x = k\frac{\lambda}{2}$ 时, 振幅取得最大, 为波腹.

当 $\frac{2\pi x}{\lambda} = (2k+1)\frac{\pi}{2}$, 即 $x = (2k+1)\frac{\lambda}{4}$ 时, 振幅为零, 为波节.

(*) 绳波中两个端点必然是驻波节点, 故绳长 $L = k\frac{\lambda}{2}$

核外电子绕原子核的运动为物质波, 轨道周长满足 $2\pi R = k\lambda$.

⑤ 质点动力学

瞬时效应: $\vec{F} = m\vec{a} = m \frac{d\vec{v}}{dt}$

时间积累: $\vec{F} dt = m d\vec{v} \Rightarrow \int_{t_1}^{t_2} \vec{F} dt = m(\vec{v}_2 - \vec{v}_1)$

空间积累: $\vec{F} d\vec{s} = m\vec{v} d\vec{v} \Rightarrow \int_{s_1}^{s_2} \vec{F} d\vec{s} = \frac{1}{2}m(v_2^2 - v_1^2)$

$p = \frac{dW}{dt} = \vec{F} \cdot \vec{v}$

⑤ 刚体动力学: $\vec{M} = \vec{r} \times \vec{F}$

瞬时效应: $M = I\beta = I \frac{d\omega}{dt}$ ($I = \int r^2 dm$, r : dm 到转轴的垂直距离)

时间积累: $M dt = I d\omega \Rightarrow \int_{\omega_1}^{\omega_2} M dt = I(\omega_2 - \omega_1)$

空间积累: $M d\theta = I \omega d\omega \Rightarrow \int_{\omega_1}^{\omega_2} M d\theta = \frac{1}{2} I(\omega_2^2 - \omega_1^2)$

$$p = \frac{dW}{dt} = \vec{M} \cdot \vec{\omega}$$

1) 转动惯量平行轴定理: $I = I_c + ml^2$

(I_c : 刚体对过质心转轴的转动惯量,

I : 刚体对与过质心转轴相距 l 的另一条平行转轴的转动惯量)

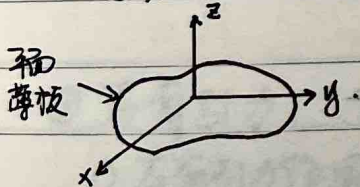
$$I = \int r^2 dm = \int (\vec{r}_c - \vec{l})^2 dm = I_c + ml^2 - 2\vec{l} \cdot \int \vec{r}_c dm$$

$$= I_c + ml^2$$

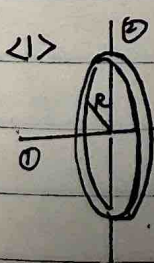
2) 转动惯量垂直轴定理: $I_z = I_x + I_y$

$$I_z = \int r^2 dm = \int (x^2 + y^2) dm$$

$$= \int x^2 dm + \int y^2 dm = I_x + I_y$$



3) 典型几何体转动惯量:



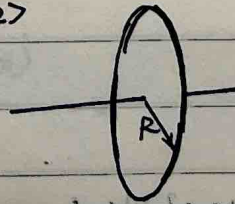
$$I_1 = \int r^2 dm = mR^2$$

$$I_2 = 4 \int_0^{\frac{\pi}{2}} \int_0^R r^2 \frac{\rho d\theta dr}{2\pi R} \cdot m$$

$$= 4 \int_0^{\frac{\pi}{2}} \int_0^R \frac{\rho r^3 d\theta dr}{2\pi} \cdot m$$

$$= \frac{2mR^2}{\pi} \int_0^{\frac{\pi}{2}} \frac{1 + \cos 2\theta}{2} d\theta$$

$$= \frac{1}{2} mR^2$$



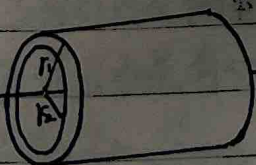
$$I = \int r^2 dm$$

$$= \int_0^R r \cdot \frac{2\pi r dt}{2\pi R} \cdot m$$

$$= \frac{2m}{R^2} \int_0^R r^3 dt$$

$$= \frac{1}{2} mR^2$$

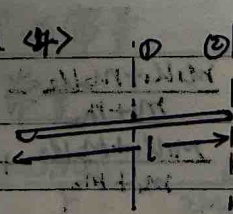
3)



$$I = \int_{r_2}^{r_1} \frac{2\pi r dt}{2\pi(r_1^2 - r_2^2)} \cdot m$$

$$= \frac{2m}{r_1^2 - r_2^2} \int_{r_2}^{r_1} r^3 dt$$

$$= \frac{1}{2} m(r_1^2 + r_2^2)$$



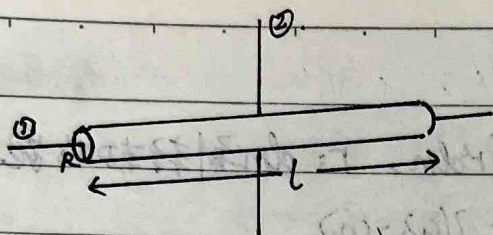
$$I_1 = \int_{-\frac{l}{2}}^{\frac{l}{2}} r^2 \cdot dm$$

$$= \frac{1}{2} ml^2$$

$$I_2 = I_1 + m(\frac{l}{2})^2$$

$$= \frac{1}{3} ml^2$$

57.



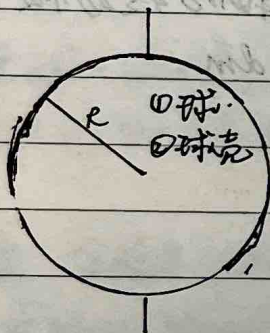
$$I_1 = \int_0^R r^2 \frac{2\pi r dr \cdot l}{\pi R^2 l} m = \frac{1}{2} m R^2$$

$$I_2 = \int \left[\frac{dm}{12} + dm (R \cos \theta)^2 \right] = \frac{1}{12} m l^2 + 2 \int_0^{\frac{\pi}{2}} \frac{(2R \cos \theta)(R d\theta \cos \theta)}{\pi R^2} m (R \cos \theta)^2$$

$$= \frac{1}{12} m l^2 + \frac{4mR^2}{\pi} \int_0^{\frac{\pi}{2}} \cos^3 \theta \sin^2 \theta d\theta$$

$$= \frac{1}{12} m l^2 + \frac{1}{4} m R^2$$

67.



$$I_1 = \int_0^{\frac{\pi}{2}} \frac{(2R \cos \theta)(2\pi R \sin \theta)(R d\theta \cos \theta)}{\frac{4}{3}\pi R^3} m (R \cos \theta)^2$$

$$= 3mR^2 \int_0^{\frac{\pi}{2}} \cos^3 \theta \sin^2 \theta d\theta = -3mR^2 \int_0^{\frac{\pi}{2}} \cos^2 \theta (1 - \cos^2 \theta) d\cos \theta$$

$$= \frac{2}{5} m R^2$$

$$I_2 = 2 \int_0^{\frac{\pi}{2}} \frac{R d\theta (2\pi R \sin \theta)}{4\pi R^2} m (R \cos \theta)^2$$

$$= mR^2 \int_0^{\frac{\pi}{2}} \sin^2 \theta d\theta = -mR^2 \int_0^{\frac{\pi}{2}} (1 - \cos^2 \theta) d\cos \theta$$

$$= \frac{2}{5} m R^2$$

碰撞

1) 正碰

$$\begin{cases} m_1 u_1 + m_2 u_2 = m_1 v_1 + m_2 v_2 \\ v_2 - v_1 = e(u_1 - u_2) \end{cases}$$

$e=1$ 完全弹性碰撞
 $e \in (0, 1)$ 一般非弹性碰撞
 $e=0$ 完全非弹性碰撞

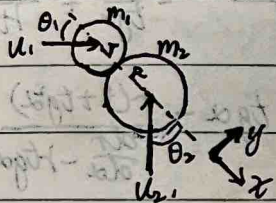
解得: $v_1 = \frac{m_1 u_1 + m_2 u_2}{m_1 + m_2} - \frac{m_2}{m_1 + m_2} e(u_1 - u_2)$

$v_2 = \frac{m_1 u_1 + m_2 u_2}{m_1 + m_2} + \frac{m_1}{m_1 + m_2} e(u_1 - u_2)$

第一项为质心速度： $\frac{m_1 u_1 + m_2 u_2}{m_1 + m_2}$ 。由于动量守恒，这一项不变。
 第二项为相对质心的运动速度，能量在质心系中由于二体作用而损耗。

$$\begin{aligned} \Delta E &= \frac{1}{2} m_1 v_1^2 + \frac{1}{2} m_2 v_2^2 - \frac{1}{2} m_1 u_1^2 - \frac{1}{2} m_2 u_2^2 \\ &= \frac{1}{2} \frac{m_1 m_2}{m_1 + m_2} (u_1 - u_2)^2 - \frac{1}{2} \frac{m_1 m_2}{m_1 + m_2} [d(u_1 - u_2)]^2 \\ &= \frac{1}{2} (1 - e^2) \frac{m_1 m_2}{m_1 + m_2} (u_1 - u_2)^2 \end{aligned}$$

2) 斜碰。



$$v_{1x} - v_{2x} = e(u_1 \cos \theta_1 - u_2 \cos \theta_2)$$

$$m_1 u_1 \cos \theta_1 + m_2 u_2 \cos \theta_2 = m_1 v_{1x} + m_2 v_{2x}$$

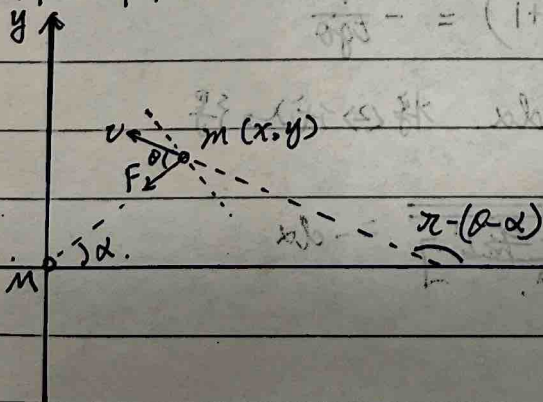
$$-m_1 u_1 \sin \theta_1 + m_1 v_{1y} = N \Delta t_1$$

$$-m_1 u_1 \sin \theta_1 + m_2 v_{2y} = \mu N \Delta t_2$$

$$m_1 u_1 \sin \theta_1 + m_2 u_2 \sin \theta_2 = m_1 v_{1y} + m_2 v_{2y}$$

① 万有引力。

1) 万有引力作用下质点的运动轨迹。



由上图， $\frac{y}{x} = \tan \alpha$ ， $\frac{dy}{dx} = \tan[\pi - (\theta - \alpha)] = \tan(\alpha - \theta) = \frac{\tan \alpha - \tan \theta}{1 + \tan \alpha \tan \theta}$ (1)

由于万有引力是保守力： $E = \frac{1}{2} m v^2 - \frac{GMm}{r}$ 为常量。

由于万有引力是有心力： $L = m v r \sin \theta$ 为常量。

$$\frac{1}{2} E = \frac{1}{2} m \frac{L^2}{m^2 r^2 \sin^2 \theta} - \frac{GMm}{r} = \frac{L^2 (1 + \tan^2 \theta)}{2m r^2 \sin^2 \theta} - \frac{GMm}{r} = \frac{L^2}{2m r^2 \sin^2 \theta} - \frac{GMm}{r}$$

$$\text{解得 } \tan^2 \alpha = \frac{L^2}{2mr^2} \left(E + \frac{GMm}{r} - \frac{L^2}{2mr^2} \right)$$

$$= \frac{L^2}{2mr^2 E + 2GMm^2 r - L^2}$$

$$\therefore \tan \alpha = \sqrt{\frac{L}{2mE \left[r + \frac{GMm}{2E} \right]^2 - \frac{(GMm)^2 + \frac{2EL^2}{m}}{4E^2}}} \quad (2)$$

由 $y = r \sin \alpha$, $x = r \cos \alpha$, (1) 式变为

$$\frac{r \sin \alpha dr + r \cos \alpha d\alpha}{\cos \alpha dr - r \sin \alpha d\alpha} = \frac{\tan \alpha - \frac{1}{\tan \alpha} (\tan \alpha \tan \alpha + 1) + \frac{1}{\tan \alpha}}{1 + \tan \alpha \tan \alpha} = -\frac{1}{\tan \alpha} + \frac{\frac{1}{\tan \alpha} + \tan \alpha}{1 + \tan \alpha \tan \alpha}$$

$$= \frac{\tan \alpha \frac{dr}{d\alpha} + r}{\frac{dr}{d\alpha} - r \tan \alpha} = \frac{\tan \alpha \left(\frac{dr}{d\alpha} - r \tan \alpha \right) + r(1 + \tan^2 \alpha)}{\frac{dr}{d\alpha} - r \tan \alpha} = \tan \alpha + \frac{r(1 + \tan^2 \alpha)}{\frac{dr}{d\alpha} - r \tan \alpha}$$

$$\therefore \tan \alpha + \frac{1}{\tan \alpha} + \frac{r(1 + \tan^2 \alpha)}{\frac{dr}{d\alpha} - r \tan \alpha} = \frac{\tan \alpha + \frac{1}{\tan \alpha}}{1 + \tan \alpha \tan \alpha}$$

两边消去 $1 + \tan^2 \alpha$, 得

$$\frac{1}{\tan \alpha} + \frac{r}{\frac{dr}{d\alpha} - r \tan \alpha} = \frac{1}{\tan \alpha}$$

$$\therefore \frac{dr}{d\alpha} = r \tan \alpha \left(\frac{1}{1 + \tan \alpha \tan \alpha} - 1 + 1 \right) = -\frac{r}{\tan \alpha}$$

分离变量得 $\frac{dr}{r} \tan \alpha = -d\alpha$. 将 (2) 代入, 得

$$\frac{L dr}{r \sqrt{2mE \left[r + \frac{GMm}{2E} \right]^2 - \frac{(GMm)^2 + \frac{2EL^2}{m}}{4E^2}}} = -d\alpha \quad (3)$$

令 $u = \frac{1}{r}$, 得

$$(1) \quad L \left(-\frac{du}{u^2} \right) = -d\alpha$$

$$\frac{L}{u} \sqrt{2mE \left[\frac{1}{u} + \frac{GMm}{2E} \right]^2 - \frac{(GMm)^2 + \frac{2EL^2}{m}}{4E^2}} = -d\alpha$$

$$\text{化简得 } \frac{du}{\sqrt{\frac{2mEL^2}{L^4} + \frac{(GMm)^2}{L^2} - \left(u - \frac{GMm}{L^2} \right)^2}} = d\alpha \quad (4)$$

令 $(u - \frac{GMm^2}{L^2}) = \sqrt{\frac{2mEL^2 + (GMm^2)^2}{L^4}} \cos\beta$ 得.

$$d\beta = -d\alpha.$$

$$\therefore u - \frac{GMm^2}{L^2} = \sqrt{\frac{2mEL^2 + (GMm^2)^2}{L^4}} \cos\alpha.$$

将 $u = \frac{1}{\sqrt{x^2+y^2}}$ 和 $\cos\alpha = \frac{x}{\sqrt{x^2+y^2}}$ 代入上式, 得.

$$\frac{1}{\sqrt{x^2+y^2}} = \frac{GMm^2}{L^2} + \sqrt{\frac{2mEL^2 + (GMm^2)^2}{L^4}} \frac{x}{\sqrt{x^2+y^2}} \quad (5)$$

整理得 $\frac{y^2}{\frac{L^2}{2mE}} + \frac{(x - \frac{\sqrt{(GMm^2)^2 + 2mEL^2}}{2mE})^2}{(\frac{GMm^2}{2E})^2} = 1 \quad (6)$

1. 若 $E=0$, 对于(5)式有

$$\frac{1}{\sqrt{x^2+y^2}} = \frac{GMm^2}{L^2} + \frac{GMm^2}{L^2} \frac{x}{\sqrt{x^2+y^2}}, \text{化简得}$$

$$1 - \frac{2GMm^2}{L^2} x = (\frac{GMm^2}{L^2})^2 y^2$$

此为一抛物线方程.

2. 若 $E > 0$, 对于(6)式有, $-\frac{L^2}{2mE} < 0$

$$\therefore \frac{(x - \frac{\sqrt{(GMm^2)^2 + 2mEL^2}}{2mE})^2}{(\frac{GMm^2}{2E})^2} - \frac{y^2}{(\frac{L^2}{2mE})^2} = 1. \text{ 双曲线} \quad (7)$$

3. 若 $E < 0$, 对于(6)式有, $-\frac{L^2}{2mE} > 0$.

$$\therefore \frac{(x - \frac{\sqrt{(GMm^2)^2 + 2mEL^2}}{2mE})^2}{(\frac{GMm^2}{2E})^2} + \frac{y^2}{(\frac{L^2}{2mE})^2} = 1. \text{ 椭圆} \quad (8)$$

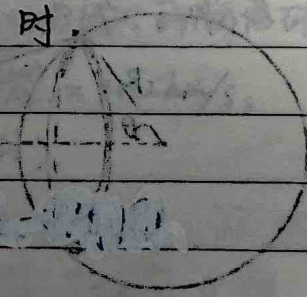
△ 当 $(GMm^2)^2 + 2mEL^2 = 0$, 即 $E = -\frac{(GMm^2)^2}{2mL^2} = -\frac{(GMm)^2}{2L^2}$ 时.

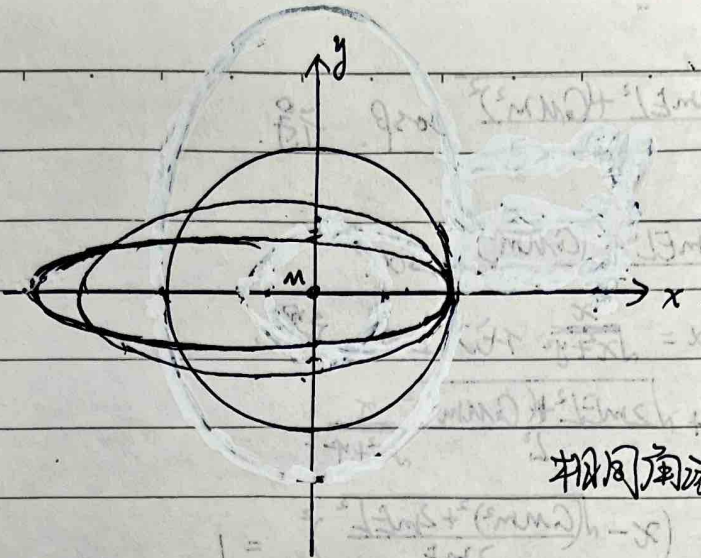
$$(9) \text{式变为 } x^2 + y^2 = (\frac{GMm}{2E})^2$$

此为一圆方程

△ 当 $E < -\frac{GMm}{2L^2}$ 时, 此情况不存在, $\Delta < 0$.

综上所述, 所有情况如下页图.





相同角动量不同能量对应的轨道

2) 引力势能 (无限远处 $E_p=0$)

① 均匀球体 (半径 R , 质量 M)

1) 当 $r \geq R$ 时

$$E_p = \int_{\infty}^r \frac{Gmm}{r^2} dr = -\frac{Gmm}{r} \Big|_{\infty}^r = -\frac{Gmm}{r}$$

2) 当 $r < R$ 时

$$E_p = \int_{\infty}^R \frac{Gmm}{r^2} dr + \int_R^r G \left(\frac{M}{R^3} m \right) \frac{m}{r^2} dr = -\frac{Gmm}{R} - \frac{Gmm(R^2 - r^2)}{2R^3}$$

② 薄球壳 (半径 R , 质量 M)

1) 当 $r \geq R$ 时

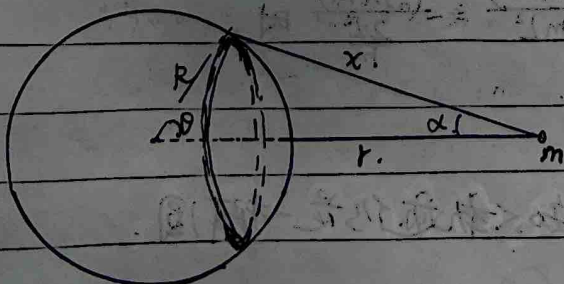
$$E_p = -\frac{Gmm}{r}$$

2) 当 $r < R$ 时

$$E_p = -\frac{Gmm}{R}$$

3) 引力场强: 高斯定理: $\oint \vec{E} \cdot d\vec{s} = \sum q_i$

① 薄球壳 (半径 R , 质量 M)



$$dE = G \frac{2\pi R^2 \epsilon_0 R d\theta \cos \alpha}{x^2}$$

$$\because \cos \alpha = \frac{x^2 + r^2 - R^2}{2rx}, \quad x^2 = R^2 + r^2 - 2Rr \cos \alpha$$

$$\therefore x dx = Rr \sin \alpha d\alpha$$

$$\therefore dE = \frac{2\pi R^2 G_0}{Rr} x dx \cdot \frac{x^2 + r^2 - R^2}{2rx} \cdot \frac{1}{x^2}$$

$$= \frac{2\pi R^2 G_0}{2r^2} \left(\frac{r^2 - R^2}{x^2} + 1 \right) dx$$

1) 当 $r \geq R$ 时

$$\therefore \int_{rR}^{rR} \left(\frac{r^2 - R^2}{x^2} + 1 \right) dx = 4R \quad \therefore E = \frac{GM}{r^2}$$

2) 当 $r < R$ 时

$$\therefore \int_{rR}^{rR} \left(\frac{r^2 - R^2}{x^2} + 1 \right) dx = 0, \quad \therefore E = 0.$$

② 均匀球体 (半径 R , 质量 M)

1) 当 $r \geq R$ 时

$$E = \int_0^R \frac{G \cdot 4\pi r^2 \rho dr}{r^2} = G \cdot \frac{4}{3}\pi R^3 \cdot \frac{M}{\frac{4}{3}\pi R^3} = \frac{GM}{r^2}$$

2) 当 $r < R$ 时

$$E = G \frac{M r^3}{R^3} = \frac{GM r}{R^3}$$

4) 宇宙速度

① 第一宇宙速度: (环绕的最小速度)

$$E = \frac{1}{2}mv^2 - \frac{GMm}{r}, \quad \text{向 } \frac{mv^2}{r} = \frac{GMm}{r^2}$$

$$\therefore E = \frac{1}{2}mv^2 - mv^2 = -\frac{1}{2}mv^2$$

可见 v 越大 E 越小, 对于半径为 R 的星球, $v_{\max} = \sqrt{\frac{GM}{R}}$

$$\therefore E_{\min} = -\frac{GMm}{2R}, \quad \text{此时物体作圆周运动}$$

$$\text{又: 地球上 } g = \frac{GM}{R^2}, \quad \therefore v_1 = \sqrt{gR} = 7.9 \text{ km/s}$$

② 第二宇宙速度: (逃逸的最小速度)

$$E = \frac{1}{2}mv^2 - \frac{GMm}{r}, \quad \text{当 } E \geq 0 \text{ 时, 轨迹为抛物线或双曲线, 即脱离环绕}$$

故 $E=0$ 时, 逃逸所需速率最小: 对于地球 $v_2 = \sqrt{\frac{2GM}{R}} = 11.2 \text{ km/s}$

$$\text{对于黑洞 } v_2 = \sqrt{\frac{2GM}{R_s}} = c, \quad \text{故 } R_s = \frac{2GM}{c^2} \text{ (史瓦西半径)}$$

③ 第三宇宙速度: (飞出太阳系)

$$\text{若地球不公转, 则 } \frac{1}{2}mv^2 - \frac{GMm}{R_{\text{地}}} = 0$$

得 $v = \sqrt{\frac{2GM}{R_{地}}} = 42.2 \text{ km/s}$.

以地球为参考系 (地球公转速 29.8 km/s), 有

$$\frac{1}{2} m v_{地}^2 - \frac{GMm}{R_{地}} = \frac{1}{2} m (42.2 \text{ km/s} - 29.8 \text{ km/s})^2$$

解得 $v_{地} = \sqrt{(42.2 - 29.8)^2 + 11.2^2} \text{ km/s} = 16.7 \text{ km/s}$.

专题: 质心系

1. 定义:
$$\sum m_i \vec{r}_{i0} = 0$$

求得
$$\frac{\sum m_i \vec{v}_{i0}}{\sum m_i} = 0$$
, 即 $\sum m_i \vec{v}_{i0} = 0$, 故质心系又称零动量系.

2. 柯尼希定理

孤立二体系统中质点 1, 2 在地面系中速度分别为 \vec{v}_1, \vec{v}_2 .

在质心系中速度分别为 \vec{v}'_1, \vec{v}'_2 , 质心系相对地面速度为 \vec{v}_c .

$\therefore \vec{v}_1 = \vec{v}'_1 + \vec{v}_c, \vec{v}_2 = \vec{v}'_2 + \vec{v}_c$

\therefore 地面系中的动能 $E_k = \frac{1}{2} m_1 v_1^2 + \frac{1}{2} m_2 v_2^2$

$$= \frac{1}{2} m_1 (\vec{v}'_1 + \vec{v}_c)^2 + \frac{1}{2} m_2 (\vec{v}'_2 + \vec{v}_c)^2$$

$$= \frac{1}{2} m_1 v_1'^2 + \frac{1}{2} m_1 v_c^2 + m_1 \vec{v}'_1 \cdot \vec{v}_c + \frac{1}{2} m_2 v_2'^2 + \frac{1}{2} m_2 v_c^2 + m_2 \vec{v}'_2 \cdot \vec{v}_c$$

$$= E_1 + E_2 + \frac{1}{2} (m_1 + m_2) v_c^2 + (m_1 \vec{v}'_1 + m_2 \vec{v}'_2) \cdot \vec{v}_c$$

\therefore 质心系中总动量为零, $\therefore m_1 \vec{v}'_1 + m_2 \vec{v}'_2 = 0$.

$$\therefore E_k = E_1 + E_2 + \frac{1}{2} (m_1 + m_2) v_c^2$$

其中, E_1, E_2 分别为 1, 2 在质心系中的动能, $\vec{v}_c = \frac{m_1 \vec{v}'_1 + m_2 \vec{v}'_2}{m_1 + m_2}$.

推广到 n 质点孤立系统, $E_k = \frac{1}{2} M v_c^2 + \sum E_{i \text{ 质心系}}$

设 $\vec{u} = \vec{v}_1 - \vec{v}_2 = \vec{v}'_1 - \vec{v}'_2$ 为两质点的相对速度.

联立 $\vec{u} = \vec{v}'_1 - \vec{v}'_2, m_1 \vec{v}'_1 + m_2 \vec{v}'_2 = 0$, 解得:

$$\begin{cases} \vec{v}_1 = \frac{m_2 \vec{u}}{m_1 + m_2} \\ \vec{v}_2 = -\frac{m_1 \vec{u}}{m_1 + m_2} \end{cases}$$

$$\begin{aligned} \therefore E_k &= \frac{1}{2} m_1 \frac{m_2^2 u^2}{(m_1 + m_2)^2} + \frac{1}{2} m_2 \frac{m_1^2 u^2}{(m_1 + m_2)^2} + \frac{1}{2} (m_1 + m_2) u^2 \\ &= \frac{1}{2} \frac{m_1 m_2}{m_1 + m_2} u^2 + \frac{1}{2} (m_1 + m_2) u^2 \end{aligned}$$

注：①对于动量守恒的孤立二体系统，相互作用只可能损失质心系中的动能，即 $\frac{1}{2} \frac{m_1 m_2}{m_1 + m_2} u^2$ 一项，而质心动能 $\frac{1}{2} (m_1 + m_2) \left(\frac{m_1 \vec{v}_1 + m_2 \vec{v}_2}{m_1 + m_2} \right)^2$ 不变；

②对于受到外力的二体系统，设 m_1 所受外力 \vec{F}_1 ， m_2 所受外力 \vec{F}_2 。

则 $\vec{F}_1 + \vec{F}_2 = (m_1 + m_2) \vec{a}_c = (m_1 + m_2) \frac{d\vec{u}}{dt}$ 。这是对柯尼希定理中第二项的作用；而对第一项的作用，可由 $m_1 \frac{d\vec{v}_1}{dt} + m_2 \frac{d\vec{v}_2}{dt} = 0$ 。

$$\vec{F}_1 + \vec{F}_1 = m_1 \frac{d\vec{v}_1}{dt}, \quad \vec{F}_2 - \vec{F}_1 = m_2 \frac{d\vec{v}_2}{dt}, \quad \vec{v}_1 - \vec{v}_2 = \vec{v}_1 - \vec{v}_2 = \vec{u} \text{ 求得,}$$

$$\therefore \frac{\vec{F}_1 + \vec{F}_1}{m_1} - \frac{\vec{F}_2 - \vec{F}_1}{m_2} = \frac{d(\vec{v}_1 - \vec{v}_2)}{dt} = \frac{d\vec{u}}{dt}$$

$$= \frac{\vec{F}_1}{m_1} - \frac{\vec{F}_2}{m_2} + \frac{m_1 + m_2}{m_1 m_2} \vec{F}_1. \text{ 可以看出, 若 } \vec{F}_1 \text{ 和 } \vec{F}_2 \text{ 为 } 0, \text{ 有 } \vec{F}_1 = \frac{m_1 m_2}{m_1 + m_2} \frac{d\vec{u}}{dt}.$$

③刚体的转动不存在柯尼希定理。

$$\text{地面系中 } E_k = \frac{1}{2} I_1 \omega_1^2 + \frac{1}{2} I_2 \omega_2^2$$

$$\text{质心系中 } E_k = \frac{1}{2} I_1' \omega_1^2 + \frac{1}{2} I_2' \omega_2^2, \quad I_1' \omega_1 + I_2' \omega_2 \neq 0$$

3. 质心系角动量定理：

$$\frac{d\vec{L}}{dt} = \vec{M} + \sum \vec{r}_{ci} \times \vec{f}_{ci} \text{ (惯性力)} = \vec{M} + \sum \vec{r}_{ci} \times (-m_i \vec{a}_c)$$

$$= \vec{M} - \left(\sum m_i \vec{r}_{ci} \right) \times \vec{a}_c = \vec{M}$$

4. 角动量柯尼希定理：

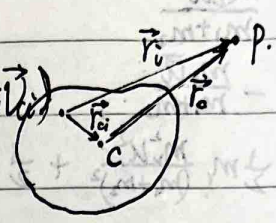
设 \vec{r}_i 和 \vec{v}_i 分别是刚体上 m_i 对 P 点的位矢和速度，

$$\vec{L} = \sum (\vec{r}_i \times m_i \vec{v}_i)$$

$$= \sum [(\vec{r}_c + \vec{r}_{ci}) \times m_i(\vec{v}_c + \vec{v}_{ci})]$$

$$= \sum (\vec{r}_c \times m_i \vec{v}_c + \vec{r}_c \times m_i \vec{v}_{ci} + \vec{r}_{ci} \times m_i \vec{v}_c + \vec{r}_{ci} \times m_i \vec{v}_{ci})$$

$$= \vec{r}_c \times m \vec{v}_c + \vec{r}_c \times (\sum m_i \vec{v}_{ci}) + (\sum m_i \vec{r}_{ci}) \times \vec{v}_c + \sum (\vec{r}_{ci} \times m_i \vec{v}_{ci})$$



$$\therefore \sum m_i \vec{v}_{ci} = 0, \quad \sum m_i \vec{r}_{ci} = 0$$

$$\therefore \vec{L} = \vec{r}_c \times m \vec{v}_c + \sum (\vec{r}_{ci} \times m_i \vec{v}_{ci})$$

质心的角动量 质心系中的角动量

5. 质心系中惯性力做功为零，惯性力力矩做功为零。

$$W_{惯} = \int (-m_i \vec{a}_c) \cdot d\vec{r}_{ci}$$

$$W_{惯} = \int |\vec{r}_{ci} \times (-m_i \vec{a}_c)| \cdot d\vec{\theta}$$

$$= -\vec{a}_c \int m_i d\vec{r}_{ci} = 0$$

$$= -\int (m_i \vec{r}_{ci}) \times \vec{a}_c \cdot d\vec{\theta} = 0$$

6. 应用典例

① 碰撞

$$\text{质心系中, } m_1 v_{1c} + m_2 v_{2c} = m_1 u_{1c} + m_2 u_{2c} = 0$$

$$v_1 - v_2 = v_{1c} - v_{2c} = e(u_{2c} - u_{1c}) = e(u_2 - u_1)$$

$$\text{解得 } \begin{cases} u_{1c} = -e u_{2c} \\ v_{2c} = -e u_{1c} \end{cases}$$

② 天体运动周期

$$G \frac{Mm}{R^2} = \frac{Mm}{M+m} \frac{4\pi^2}{T^2} R$$

$$\therefore T = 2\pi \sqrt{\frac{R^3}{G(M+m)}}$$

二. 狭义相对论

1. 伽利略变换

$$\textcircled{1} \begin{cases} x = x' + vt' \\ y = y' \\ z = z' \\ t = t' \end{cases}$$

$$\textcircled{2} \vec{F} = \vec{F}' + \vec{F}_{\text{相}} \quad \text{绝对} = \text{相对} + \text{牵连}$$

$$\therefore \vec{v} = \vec{v}' + \vec{v}_{\text{相}}$$

$$\therefore \vec{a} = \vec{a}' + 0 \quad \because m = m' \quad \therefore \vec{F} = \vec{F}'$$

$$\text{平移惯性力: } \vec{F} = -m\vec{a}$$

$$\text{转动惯性力: } \vec{F} = -m\vec{\omega} \times (\vec{\omega} \times \vec{r})$$

$$\text{科里奥利力: } \vec{F} = -2m\vec{\omega} \times \vec{v}_{\text{相}}$$

③ 多普勒效应

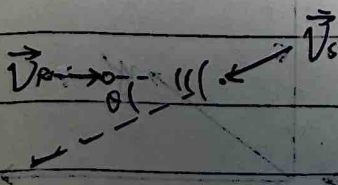
1) 观察者以 v 运动

$$\lambda_k = \frac{v + v_k}{\nu} = \frac{v + v_k}{v \nu} = \frac{v + v_k}{v} \cdot \nu \quad (v_k \text{ 相向为正, 远离为负})$$

2) 波源相对介质以 v_s 运动

$$\lambda_s = \frac{v}{\nu - \frac{v_s}{\nu}} = \frac{v}{\nu - v_s} = \frac{v}{v - v_s} \cdot \nu \quad (v_s \text{ 相向为正, 远离为负})$$

3) 一般情况



$$\lambda' = \frac{v + v_k \cos \theta}{v - v_s} \cdot \nu$$

只有纵向多普勒效应

没有横向多普勒效应

2. 洛伦兹变换

① 基本假设:

1) 所有惯性系平权 (惯性定律成立的参考系是惯性系) — 相对性原理

2) 所有惯性系中真空光速不变 — 光速不变原理

洛伦兹变换 二

② 洛伦兹变换：保证所有物理定律具有协变性的坐标变换公式。

1) 设惯性系 K' 相对于惯性系 K 沿 x 方向以 v 运动。

$$x = x' = 0 \text{ 时, } y = y' = 0, z = z' = 0, t = t' = 0.$$

2) 相对性原理要求，由 $K(x, y, z, t)$ 到 $K'(x', y', z', t')$ 的坐标变换应是对称的，即正、逆变换都是同一种函数。此要求来源于空间的均匀性，满足这一要求的变换应是一次函数。

$$\begin{cases} x' = ax + bt \\ t' = px + qt \end{cases} \Rightarrow \begin{cases} x = \frac{q}{aq - bp} x' - \frac{b}{aq - bp} t' \\ t = \frac{p}{bp - aq} x' - \frac{a}{bp - aq} t' \end{cases}$$

由于相对运动只发生在 x 方向，故

$$\begin{cases} y' = y \\ z' = z \end{cases}$$

3) 光速不变原理要求，若在 $t = t' = 0$ 时刻由原点发出一闪光，在两惯性系中有

$$\begin{cases} x^2 + y^2 + z^2 - ct^2 = 0 \\ x'^2 + y'^2 + z'^2 - ct'^2 = 0 \end{cases}$$

对于任意一事件，令 $x^2 + y^2 + z^2 - ct^2 = \lambda(x'^2 + y'^2 + z'^2 - ct'^2 + A)$

由对称性和连续性，得 $x^2 + y^2 + z^2 - ct^2 = \lambda(x'^2 + y'^2 + z'^2 - ct'^2)$

4) 在 K 系中， K' 系的原点 O' 满足

$$\begin{cases} \frac{dx'}{dt} = a \frac{dx}{dt} + b \\ \frac{dt'}{dt} = p \frac{dx}{dt} + q \end{cases}$$

$$\therefore \frac{dx'}{dt} = 0$$

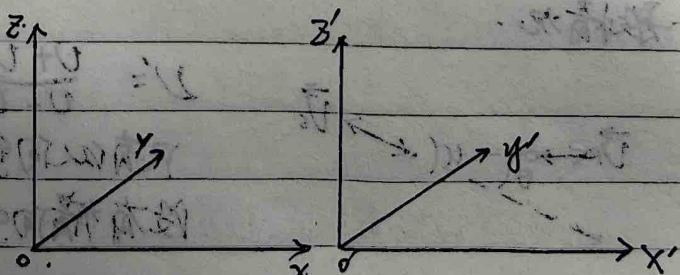
$$\therefore dx = b dt, dt' = q dt$$

$$\therefore \frac{dx}{dt} = \frac{b}{q} = -v$$

(K' 系中 K 系原点朝 $-x'$ 方向运动，故 v 为负)。

在 K' 系中， K 系的原点 O 满足

$$\begin{cases} \frac{dx}{dt'} = -\frac{q}{aq - bp} \frac{dx'}{dt'} - \frac{b}{aq - bp} \\ \frac{dt}{dt'} = \frac{p}{bp - aq} \frac{dx'}{dt'} - \frac{a}{bp - aq} \end{cases}$$



$$\therefore \frac{dx}{dt} = 0$$

$$\therefore dx = -\frac{b}{aq-bp} dt', \quad dt = -\frac{a}{bp-aq} dt'$$

$$\therefore \frac{dx}{dt} = -\frac{b}{p} = v \quad (\text{K系中K系原点朝+x方向运动, 故v为正}).$$

所以 $b = -av$, $a = q$. 代入变换式, 得

$$\begin{cases} x' = ax - avt \\ t' = px + at. \end{cases}$$

代入事件间隔恒等式, 得

$$x^2 + y^2 + z^2 - c^2 t^2 = (x - avt)^2 + y^2 + z^2 - c^2 (px + at)^2$$

化简得:

$$x^2 - c^2 t^2 = (a^2 - c^2 p^2) x^2 + (a^2 v^2 - a^2 c^2) t^2 - (2a^2 v + 2apc^2) xt.$$

由于同类项前系数相等:

$$\begin{cases} 1 = a^2 - c^2 p^2 \\ -c^2 = a^2 v^2 - a^2 c^2 \\ 0 = 2a^2 v + 2apc^2 \end{cases} \Rightarrow \begin{cases} a = \frac{1}{\sqrt{1-v^2/c^2}} \\ p = -\frac{v}{c} \sqrt{\frac{1}{c^2-v^2}} \end{cases}$$

代入变换式, 得

$$\begin{cases} x' = \frac{1}{\sqrt{1-v^2/c^2}} (x - vt) \\ y' = y \\ z' = z \\ t' = \frac{1}{\sqrt{1-v^2/c^2}} (t - \frac{v}{c^2} x) \end{cases} \quad \begin{cases} x = \frac{1}{\sqrt{1-v^2/c^2}} (x' + vt') \\ y = y' \\ z = z' \\ t = \frac{1}{\sqrt{1-v^2/c^2}} (t' + \frac{v}{c^2} x') \end{cases}$$

注: (1) 注意推导的前提是 $x = x' = 0, y = y' = 0, z = z' = 0, t = t' = 0$

此前提不失一般性, 但由两原理推出的式子只适合这一前提,

对于 $t = t' = 0$ 时刻原点不重合的情况两式不符合。

(2) 由于空间的均匀性, 所有惯性系平权, 只有线性的变换方程才能

体现这一原理。

(3) 光速不变原理本质要求是 $(dv)^2 + (dy)^2 + (dz)^2 - (cdt)^2 = (dx)^2 + (dy)^2 + (dz)^2 - (cdt)^2$

$$= ds^2 = \sqrt{c^2 dt^2 - (dl)^2} \quad \text{L为固有长, l为固有长. } \therefore dl_0 = 0 \quad \therefore dt = \frac{ds}{c}$$

③ 相对论时空观

1) 时序的相对性与因果关系

设事件A、B在K系中发生的地点与时间分别是 (x_1, t_1) 和 (x_2, t_2) 。

则在K系中，事件A、B发生的时间：

$$t_1 = \frac{t_1' + \frac{v}{c^2} x_1'}{\sqrt{1 - v^2/c^2}}, \quad t_2 = \frac{t_2' + \frac{v}{c^2} x_2'}{\sqrt{1 - v^2/c^2}}$$

$$\therefore t_2 - t_1 = \frac{(t_2' - t_1') + \frac{v}{c^2}(x_2' - x_1')}{\sqrt{1 - v^2/c^2}} = \frac{(t_2' - t_1')(1 + \frac{v}{c^2} \cdot \frac{x_2' - x_1'}{t_2' - t_1'})}{\sqrt{1 - v^2/c^2}}$$

类时间隔事件： $\frac{x_2' - x_1'}{t_2' - t_1'} > -c$ 可能有因果关系，有则因果不会倒置。

类空间隔事件： $\frac{x_2' - x_1'}{t_2' - t_1'} < -c$ 可能无因果关系，时间顺序不会颠倒。
无因果关系，时间顺序可能颠倒。
(若有，则要么观察超光速要么因果任意起理)

2) ① 同时的相对性：

若K系中在t时刻 x_1' 和 x_2' 处同时发生了两事件A、B，在K系中，有

$$t_1 = \frac{t + \frac{v}{c^2} x_1'}{\sqrt{1 - v^2/c^2}}, \quad t_2 = \frac{t + \frac{v}{c^2} x_2'}{\sqrt{1 - v^2/c^2}}$$

对K系而言，这两事件不一定同时发生，A、B在K系中时间间隔为

$$\Delta t = t_2 - t_1 = \frac{v}{c^2} \frac{x_2' - x_1'}{\sqrt{1 - v^2/c^2}}$$

故只能在一个坐标系中对钟，或在两个坐标系中两个相接触点时钟。

② 时间间隔相对性：

若K系中在x处于 t_1' 和 t_2' 时刻发生了两事件A、B，在K系中，有

$$t_1 = \frac{t_1' + \frac{v}{c^2} x}{\sqrt{1 - v^2/c^2}}, \quad t_2 = \frac{t_2' + \frac{v}{c^2} x}{\sqrt{1 - v^2/c^2}}$$

$$\Delta t = t_2 - t_1 = \frac{t_2' - t_1'}{\sqrt{1 - v^2/c^2}} = \frac{\Delta t'}{\sqrt{1 - v^2/c^2}} > \Delta t'$$

故在不同参考系中A、B时间间隔为固有时(原时间间隔)最短。

③ 同地的相对性

若K系中在x处于 t_1 和 t_2 时刻发生了两事件A、B, 在K'系中, 有

$$x_1 = \frac{x' + vt_1'}{\sqrt{1 - v^2/c^2}}, \quad x_2 = \frac{x' + vt_2'}{\sqrt{1 - v^2/c^2}}$$

$$\Delta x = x_2 - x_1 = \frac{v(t_2' - t_1')}{\sqrt{1 - v^2/c^2}}$$

对K系而言, 这两事件不同地发生, 原因是K相对K'有速度!

④ 长度的相对性

在K'系中沿x'方向放有一静止直尺, 两端坐标为 x_1' , x_2' , 其固有长度 $l' = |x_2' - x_1'|$. 在K系中测量的时刻为t, (在动参考系中异地对钟), 有

$$x_1 = \frac{x_1' - vt}{\sqrt{1 - v^2/c^2}}, \quad x_2 = \frac{x_2' - vt}{\sqrt{1 - v^2/c^2}}$$

$$\text{故在K系中, } l = |x_2 - x_1| = |x_2' - x_1'| \sqrt{1 - v^2/c^2} = l' \sqrt{1 - v^2/c^2}$$

但在静系K'中, x_1' 与 x_2' 两处时刻并不相同, 有时差 $\Delta t' = \frac{1}{\sqrt{1 - v^2/c^2}} (\Delta t - \frac{v}{c^2} \Delta x)$

由于在动系K中测量时 x_1, x_2 处时刻相同, 故 $\Delta t = 0 \therefore \Delta t' = \frac{v}{c} \frac{l}{\sqrt{1 - v^2/c^2}} = \frac{v}{c^2} l'$

④ 四维矢量: [$u = (u_x, u_y, u_z, u_t)$: 四维速度; $v = (v_x, v_y, v_z)$: 三维速度; V : 参考系速]

1) 闵可夫斯基空间

$$x' = \gamma(x + i\beta(ict))$$

$$y' = y$$

$$z' = z$$

$$ict' = \gamma(ict - i\beta x)$$

洛伦兹不变量:

$$x'^2 + y'^2 + z'^2 + (ict')^2$$

$$= \gamma^2(x - \beta ct)^2 + y^2 + z^2 + \gamma^2(-1)(ct - \beta x)^2$$

$$= x^2 + y^2 + z^2 + (ict)^2 = -s^2$$

2) 四维速度

$$\text{固有时 } dt = \frac{ds}{c}$$

$$\text{定义四维速度 } u_x = \frac{dx}{dt}, \quad u_y = \frac{dy}{dt}, \quad u_z = \frac{dz}{dt}, \quad u_t = \frac{d(ict)}{dt}$$

$$\therefore u_x = \frac{dx}{dt} \frac{dt}{dt} = \gamma \frac{dx}{dt} = \frac{u_x}{\sqrt{1 - v^2/c^2}}, \quad \text{同理, } u_y = \frac{u_y}{\sqrt{1 - v^2/c^2}}, \quad u_z = \frac{u_z}{\sqrt{1 - v^2/c^2}}$$

以上 U_x, U_y, U_z 为 K 系中物体的三维速度。

$$\text{对于四维速度的最后一分量, } U_t = \frac{d(\text{ict})}{dt} = ic\gamma = \frac{ic}{\sqrt{1-v^2/c^2}}$$

$$\therefore U = (U_x, U_y, U_z, U_t) = (\gamma U_x, \gamma U_y, \gamma U_z, ic\gamma)$$

由于 $dx, dy, dz, d(\text{ict})$ 服从洛伦兹变换, 且 dt 是不变量, 所以

$$\begin{cases} U_x' = \gamma_0(U_x + i\beta U_t) \\ U_y' = U_y \\ U_z' = U_z \\ U_t' = \gamma_0(U_t - i\beta U_x) \end{cases} \quad \text{洛伦兹不变量:}$$

$$U_x^2 + U_y^2 + U_z^2 + U_t^2 = \gamma_0^2(U_x^2 + U_y^2 + U_z^2 - c^2)$$

$$= \frac{U_x^2 + U_y^2 + U_z^2 - c^2}{1 - v^2/c^2}$$

$$\therefore \gamma' U_x' = \gamma_0 \gamma (U_x - c\beta) = \frac{U_x^2 - c^2}{1 - v^2/c^2} = -c^2$$

$$\gamma' U_y' = \gamma U_y$$

$$\gamma' U_z' = \gamma U_z$$

$$c\gamma' = \gamma_0 \gamma (c - \beta U_x)$$

其中 $\gamma_0 = \frac{1}{\sqrt{1-\beta^2}}$, $\gamma = \frac{1}{\sqrt{1-v^2/c^2}}$ (v 为 K 系中速度) $\gamma' = \frac{1}{\sqrt{1-v'^2/c^2}}$ (v' 为 K' 系中速度)

$$\frac{\gamma_0 \gamma}{\gamma'} = \frac{1}{1 - \beta U_x/c} = \frac{1}{1 - \frac{v U_x}{c^2}} \quad (\beta = \frac{v}{c}, v \text{ 为 } K \text{ 与 } K' \text{ 的相对速度})$$

将此式代入前三式, 得

$$\begin{cases} U_x' = \frac{\gamma_0 \gamma}{\gamma'} (U_x - c\beta) = \frac{U_x - v}{1 - \frac{v U_x}{c^2}} \\ U_y' = \frac{\gamma}{\gamma'} U_y = \frac{U_y \sqrt{1 - v^2/c^2}}{1 - \frac{v U_x}{c^2}} \\ U_z' = \frac{\gamma}{\gamma'} U_z = \frac{U_z \sqrt{1 - v^2/c^2}}{1 - \frac{v U_x}{c^2}} \end{cases}$$

(速度变换律可直接将洛伦兹变换微分得出, 即 $dx = \frac{dx' + v dt'}{\sqrt{1 - v^2/c^2}}$, $dy = dy'$, $dz = dz'$, $dt = \frac{dt' + \frac{v}{c^2} dx'}{\sqrt{1 - v^2/c^2}}$. 用四式除前三式即得: 只是用四维速度导出更简且具代表性).

3). 四维动量:

定义四维动量 $P_x = m_0 U_x, P_y = m_0 U_y, P_z = m_0 U_z, P_t = m_0 U_t$

$$\therefore P = (P_x, P_y, P_z, P_t) = (\gamma m_0 U_x, \gamma m_0 U_y, \gamma m_0 U_z, i m_0 c \gamma)$$

显然, 四维动量服从洛伦兹变换:

$$\left\{ \begin{array}{l} P'_x = \frac{P_x + i\beta P_t}{\sqrt{1-v^2/c^2}} = \frac{P_x - \frac{vE}{c^2}}{\sqrt{1-v^2/c^2}} \\ P'_y = P_y \\ P'_z = P_z \\ P'_t = \frac{P_t - i\beta P_x}{\sqrt{1-v^2/c^2}} = \frac{P_t - \frac{v}{c} P_x}{\sqrt{1-v^2/c^2}} \end{array} \right. \quad \begin{array}{l} \text{洛伦兹不变量:} \\ P_x^2 + P_y^2 + P_z^2 + P_t^2 \\ = \frac{m_0^2 (U_x^2 + U_y^2 + U_z^2 - c^2)}{1 - v^2/c^2} \\ = -m_0^2 c^2 \end{array}$$

⑤ 狭义相对论动力学. $U = (U_x, U_y, U_z, U_t)$: 四维速度; $V = (V_x, V_y, V_z)$: 三维速度;
 V : 参考系相对速度.

1) 质量: $m = \frac{m_0}{\sqrt{1-v^2/c^2}}$

2) 动量: $\vec{p} = m\vec{v} = \frac{m_0\vec{v}}{\sqrt{1-v^2/c^2}}$; 力: $\vec{F} = \frac{d\vec{p}}{dt} = \frac{d}{dt} \left(\frac{m_0\vec{v}}{\sqrt{1-v^2/c^2}} \right)$

3) 能量: $dE_k = \vec{F} \cdot d\vec{s} = \frac{d(m\vec{v})}{dt} \cdot d\vec{s} = v^2 dm + m dv$

又: $m^2 c^2 = m_0^2 c^2 = m^2 v^2$, $\therefore 2m c^2 dm = 2m v^2 dm + 2v m^2 dv$

$\therefore c^2 dm = v^2 dm + m dv$ 代入前式, 得

$dt_k = c^2 dm$

$\therefore E_k = mc^2 - m_0 c^2$. \therefore 总能量 $E = mc^2$; 功率: $P = \frac{dE_k}{dt} = \vec{F} \cdot \vec{v}$.

且有 $E^2 = m_0^2 c^4 + p^2 c^2$.

4) 力的变换公式:

定义三维力: $f_x = \frac{dP_x}{dt}$, $f_y = \frac{dP_y}{dt}$, $f_z = \frac{dP_z}{dt}$, $f_t = \frac{dP_t}{dt}$.

$\therefore f'_x = \frac{dP'_x}{dt'} = \frac{dP_x}{dt} \frac{dt}{dt'} = \frac{dP_x}{dt} \frac{1}{\sqrt{1-v^2/c^2}} = f_x / \sqrt{1-v^2/c^2}$

$f'_y = f_y / \sqrt{1-v^2/c^2}$, $f'_z = f_z / \sqrt{1-v^2/c^2}$

$f'_t = \frac{dP'_t}{dt'} = \frac{dP_t - i\beta dP_x}{dt} \frac{dt}{dt'} = \frac{dP_t}{dt} \frac{1}{\sqrt{1-v^2/c^2}} - \frac{i\beta m_0 c}{\sqrt{1-v^2/c^2}} \frac{d}{dt} \left(\frac{v}{\sqrt{1-v^2/c^2}} \right) = \frac{f_t \cdot \vec{v}}{c \sqrt{1-v^2/c^2}}$

$\therefore f'_x = \frac{f_x + i\beta f_t}{\sqrt{1-v^2/c^2}} = \frac{f_x - \frac{v}{c^2} \vec{F} \cdot \vec{v}}{\sqrt{1-v^2/c^2}}$

$\therefore \frac{f'_x}{\sqrt{1-v^2/c^2}} = \frac{f_x}{\sqrt{1-v^2/c^2}} - \frac{v}{c^2} \frac{\vec{F} \cdot \vec{v}}{\sqrt{1-v^2/c^2}}$ 根据 $\gamma_{0x} = \frac{1}{1 - \frac{vU_x}{c^2}}$

$\therefore f'_x = \frac{f_x - \frac{v}{c^2} \vec{F} \cdot \vec{v}}{1 - \frac{vU_x}{c^2}}$

$\therefore f'_y = f_y$

$\therefore \frac{F'_y}{\sqrt{1-v^2/c^2}} = \frac{F_y}{\sqrt{1-v^2/c^2}} \quad \therefore F'_y = \frac{F_y \sqrt{1-v^2/c^2}}{1 - \frac{v v_x}{c^2}}$

同理 $F'_z = \frac{F_z \sqrt{1-v^2/c^2}}{1 - \frac{v v_x}{c^2}}$

$f'_t = \frac{f_t - v \beta f_x}{\sqrt{1-v^2/c^2}} \dots$

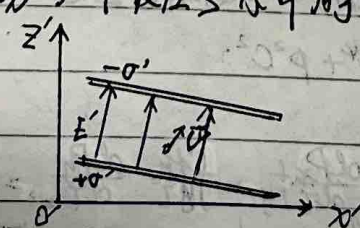
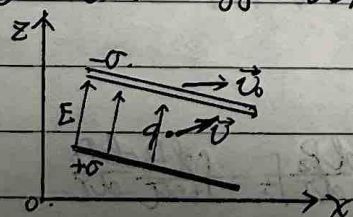
综合上几式，有：F_x, F_y, F_z 皆为三维力。

$$\begin{cases} F'_x = \frac{F_x - \frac{v}{c} \vec{F} \cdot \vec{v}}{1 - \frac{v v_x}{c^2}} \\ F'_y = \frac{F_y \sqrt{1-v^2/c^2}}{1 - \frac{v v_x}{c^2}} \\ F'_z = \frac{F_z \sqrt{1-v^2/c^2}}{1 - \frac{v v_x}{c^2}} \end{cases}$$

应用举例：磁场的来源：

带电平行平板在 S 系中以 $\vec{v}_0 = v_0 \vec{i}$ 运动，板间有 - 电荷 ρ_0 以速度

$\vec{v} = v_x \vec{i} + v_y \vec{j} + v_z \vec{k}$ 运动；平板在 S' 系中静止， ρ_0 在 S' 系中 $\vec{v}' = v'_x \vec{i}' + v'_y \vec{j}' + v'_z \vec{k}'$



S' 系中 $F'_x = qE'_x = q(\frac{\sigma'}{\epsilon_0}) = q(\frac{\sigma_0}{\epsilon_0})_x = qE_x$

$U'_x = \frac{v_x - v_0}{1 - \frac{v_0 v_x}{c^2}}$

$F'_y = qE'_y = q(\frac{\sigma'}{\epsilon_0})_y = q(\frac{\sigma_0 \sqrt{1-v_0^2/c^2}}{\epsilon_0})_y = qE_y \sqrt{1-v_0^2/c^2}$

$U'_y = \frac{v_y}{1 - \frac{v_0 v_x}{c^2}} \sqrt{1-v_0^2/c^2}$

$F'_z = qE'_z = q(\frac{\sigma'}{\epsilon_0})_z = q(\frac{\sigma_0 \sqrt{1-v_0^2/c^2}}{\epsilon_0})_z = qE_z \sqrt{1-v_0^2/c^2}$

$U'_z = \frac{v_z}{1 - \frac{v_0 v_x}{c^2}} \sqrt{1-v_0^2/c^2}$

根据力的变换公式，在 S 系中。

$$F_x = \frac{F'_x + \frac{v_0}{c} (F'_y U'_y + F'_z U'_z)}{1 + \frac{v_0 v_x}{c^2}} = \frac{qE_x + \frac{q v_0}{c} [E_y \frac{v_y - v_0}{1 - \frac{v_0 v_x}{c^2}} + (E_z \frac{v_z - v_0}{1 - \frac{v_0 v_x}{c^2}}) \sqrt{1-v_0^2/c^2}]}{1 + \frac{v_0 v_x}{c^2}}$$

$$= qE_x + q(E_y v_y + E_z v_z) \frac{v_0}{c^2}$$

$$F_y = \frac{qE_y \sqrt{1-v_0^2/c^2} \cdot \sqrt{1-v_0^2/c^2}}{1 + \frac{v_0 v_y - v_y^2}{c^2 - v_0 v_y}} = qE_y - \frac{q v_0 v_y E_y}{c^2}$$

$$F_z = qE_z - \frac{q v_0 v_z E_z}{c^2}$$

定义 $\vec{B} = \frac{1}{c} \vec{v} \times \vec{E}$

$$\therefore \vec{F} = \vec{F}_x + \vec{F}_y + \vec{F}_z = q(\vec{E}_x + \vec{E}_y + \vec{E}_z) + q \cdot \vec{v} \times \vec{B} = q\vec{E} + q\vec{v} \times \vec{B}$$

⑥ 核反应和粒子反应

1) 原子核: $M = N + Z$ (M : 质量数, N : 中子数, Z : 质子数)

$$\left\{ \begin{array}{l} \alpha \text{ 衰变: } {}_Z^M X \rightarrow {}_{Z-2}^{M-4} Y + {}_2^4 \text{He} : \text{放出 } \alpha \text{ 粒子} \\ \beta \text{ 衰变: } {}_Z^M X \rightarrow {}_{Z+1}^M Y + {}_{-1}^0 e : \text{放出 } \beta \text{ 粒子} \end{array} \right\} \text{放出 } \gamma \text{ 光子}$$

$$N = N_0 e^{-\lambda t}, \text{半衰期 } T: N = \frac{N_0}{2}, \therefore e^{-\lambda T} = \frac{1}{2}, T = \frac{\ln 2}{\lambda}$$

$$\therefore N = N_0 e^{t(-\frac{\ln 2}{T})} = N_0 (e^{\frac{\ln 2}{T}})^{-\frac{t}{T}} = N_0 \left(\frac{1}{2}\right)^{\frac{t}{T}}$$

$$\left\{ \begin{array}{l} \text{质子的发现: } {}_7^{14} \text{N} + {}_2^4 \text{He} \rightarrow {}_8^{17} \text{O} + {}_1^1 \text{H} \\ \text{中子的发现: } {}_4^9 \text{Be} + {}_2^4 \text{He} \rightarrow {}_6^{12} \text{C} + {}_0^1 \text{n} \\ \text{正电子的发现: } {}_{15}^{30} \text{P} \rightarrow {}_{14}^{30} \text{Si} + {}_{+1}^0 e \end{array} \right.$$

$$\left\{ \begin{array}{l} \text{核裂变: } {}_{92}^{235} \text{U} + {}_0^1 \text{n} \rightarrow {}_{56}^{141} \text{Ba} + {}_{36}^{92} \text{Kr} \\ \text{核聚变: } {}_1^2 \text{H} + {}_1^3 \text{H} \rightarrow {}_2^4 \text{He} + {}_0^1 \text{n} \end{array} \right.$$

$$\left\{ \begin{array}{l} \text{核裂变: } {}_{92}^{235} \text{U} + {}_0^1 \text{n} \rightarrow {}_{56}^{141} \text{Ba} + {}_{36}^{92} \text{Kr} \\ \text{核聚变: } {}_1^2 \text{H} + {}_1^3 \text{H} \rightarrow {}_2^4 \text{He} + {}_0^1 \text{n} \end{array} \right.$$

$$\left\{ \begin{array}{l} \text{核裂变: } {}_{92}^{235} \text{U} + {}_0^1 \text{n} \rightarrow {}_{56}^{141} \text{Ba} + {}_{36}^{92} \text{Kr} \\ \text{核聚变: } {}_1^2 \text{H} + {}_1^3 \text{H} \rightarrow {}_2^4 \text{He} + {}_0^1 \text{n} \end{array} \right.$$

$$\left\{ \begin{array}{l} \text{核裂变: } {}_{92}^{235} \text{U} + {}_0^1 \text{n} \rightarrow {}_{56}^{141} \text{Ba} + {}_{36}^{92} \text{Kr} \\ \text{核聚变: } {}_1^2 \text{H} + {}_1^3 \text{H} \rightarrow {}_2^4 \text{He} + {}_0^1 \text{n} \end{array} \right.$$

2) 两体衰变: $A \rightarrow A_1 + A_2$

$$P_1 = P_2$$

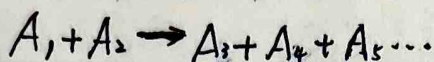
$$m_0 c^2 = \sqrt{P_1^2 c^2 + m_{10}^2 c^4} + \sqrt{P_2^2 c^2 + m_{20}^2 c^4}$$

$$\text{解得 } P_1 = P_2 = \frac{c}{2m_0} \sqrt{[m_0^2 - (m_{10} + m_{20})^2] [m_0^2 - (m_{10} - m_{20})^2]}$$

$$E_1 = \sqrt{P_1^2 c^2 + m_{10}^2 c^4} = \frac{m_0^2 + m_{10}^2 - m_{20}^2}{2m_0} c^2$$

$$E_2 = \sqrt{P_2^2 c^2 + m_{20}^2 c^4} = \frac{m_0^2 + m_{20}^2 - m_{10}^2}{2m_0} c^2$$

3) 两体反应、动能



在动心系 (动量中心系: 相对论中, 动心系一般不与质心系重合) 中:

- (1) $P_1' = P_2'$
 - (2) $P_1' = \gamma(P_1 - \beta \frac{E_1}{c})$
 - (3) $E_1' = \gamma(E_1 - \beta P_1 c)$
 - (4) $P_2' = \gamma \beta m_{20} c$
 - (5) $E_2' = \gamma m_{20} c^2$
- } 高能粒子
} 靶粒子 (在实验室系中静止)

(由四维动量变换的最后一式可得 $E' = (E - v P_x) \sqrt{1 - v^2/c^2}$.)

由(1)(2)(3)式解得 $\beta = \frac{P_1 c}{E_1 + m_{20} c^2}$

$$\therefore E_1' + E_2' = \gamma (E_1 - \beta P_1 c + m_{20} c^2) = \frac{1}{\sqrt{1 - \beta^2}} (E_1 - \frac{P_1^2 c^2}{E_1 + m_{20} c^2} + m_{20} c^2)$$

$$= \frac{1}{\sqrt{1 - \frac{E_1^2 - m_{20}^2 c^4}{(E_1 + m_{20} c^2)^2}}} (E_1 - \frac{E_1^2 - m_{20}^2 c^4}{E_1 + m_{20} c^2} + m_{20} c^2)$$

$$= \sqrt{m_{20}^2 c^4 + m_{20}^2 c^4 + 2 E_1 m_{20} c^2}$$

这是动心系中的总能量 E' 的表达式. 在动心系中, 这部分能量可完全转化为生成物的静质能, 即反应产物在动心系中全部静止, 没有动能. 故这个能量 E' 也叫反应有效能.

设发生这种阈能反应时, 入射粒子 m_0 的能量阈值为 E_m , 在动心系中的动能为 E_{km} .

$$\therefore \sqrt{m_0^2 c^4 + m_{20}^2 c^4 + 2 E_m m_{20} c^2} = \sum_{i=3}^n m_i c^2 \quad (\text{反应后所有生成物的静质能})$$

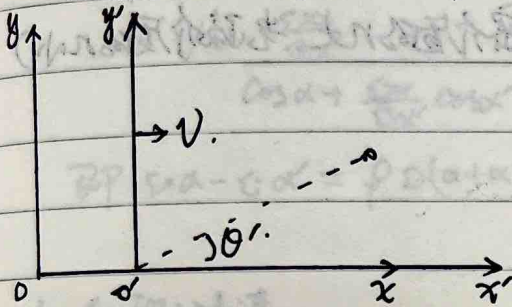
$$\text{解得 } E_m = \frac{(\sum_{i=3}^n m_i c^2)^2 - (m_0^2 c^4 + m_{20}^2 c^4)}{2 m_{20} c^2} \quad \therefore E_{km} = E_m - m_0 c^2 =$$

$$\frac{(\sum_{i=3}^n m_i c^2)^2 - (m_0 c^2 + m_{20} c^2)^2}{2 m_{20} c^2} = \frac{(\sum_{i=3}^n m_i + m_0 + m_{20}) (\sum_{i=3}^n m_i - m_0 - m_{20}) c^2}{2 m_{20}}$$

$$= \left[- (m_0 + m_{20} - \sum_{i=3}^n m_i) c^2 \right] \cdot \frac{\sum_{i=3}^n m_i}{2 m_{20}} \quad [Q = (m_0 + m_{20} - \sum_{i=3}^n m_i) c^2 \text{ 反应能}]$$

④ 多普勒效应

设光源相对K系静止, 观察者相对K'系静止, K'系以速度 v 沿K系 x 轴正向运动, K系中光源到观察者的连线与 x 轴的夹角为 θ' .



$$\begin{aligned} \text{在K'系中光子沿} x' \text{轴的分量 } p_x' &= p' \cos \theta' \\ &= \frac{E'}{c} \cos \theta' = \frac{h\nu'}{c} \cos \theta' \end{aligned}$$

$$\text{由洛伦兹变换 } E = \frac{1}{\sqrt{1-\beta^2}} (E' + \beta c p_x')$$

$$\therefore h\nu = \frac{1}{\sqrt{1-\beta^2}} (h\nu' + h\nu' \beta \cos \theta')$$

$$\therefore \frac{\nu}{\nu'} = \frac{1}{1 - \beta \cos \theta'}$$

$$\left\{ \begin{array}{l} \theta' = 0 \text{ 时, } \frac{\nu}{\nu'} = \sqrt{\frac{1+\beta}{1-\beta}} \approx 1 + \beta \\ \theta' = \frac{\pi}{2} \text{ 时, } \frac{\nu}{\nu'} = \sqrt{1-\beta^2} \approx 1 - \frac{1}{2}\beta^2 \end{array} \right.$$

三. 几何光学

$$1. \text{ 光程} = \Delta = ct = nvt = ns$$

$$\text{光程差: } \delta = n_1 s_1 - n_2 s_2$$

$$(\text{光速 } c = \frac{1}{\sqrt{\mu_0 \epsilon_0}}, v = \frac{c}{\sqrt{\epsilon_r \mu_r}}, n = \sqrt{\epsilon_r \mu_r})$$

费马原理: 光沿最短或最长光程传播, $\int_a^b n ds = \text{极值}$.

2. 光的反射

$$\Delta = n_1 \sqrt{(x_1 - x)^2 + y_1^2} + n_2 \sqrt{(x_2 - x)^2 + y_2^2}$$

$$\frac{d\Delta}{dx} = n_1 \cdot \frac{1}{2} \frac{2(x-x_1)(-dx)}{\sqrt{(x-x_1)^2 + y_1^2}} + n_2 \cdot \frac{1}{2} \frac{2(x_2-x)(-dx)}{\sqrt{(x_2-x)^2 + y_2^2}} = 0$$

$$\therefore \frac{x-x_1}{\sqrt{(x-x_1)^2 + y_1^2}} = \frac{x_2-x}{\sqrt{(x_2-x)^2 + y_2^2}} \quad \therefore i_1 = i_2$$

3. 光的折射

$$\Delta = n_1 \sqrt{(x_1 - x)^2 + y_1^2} + n_2 \sqrt{(x_2 - x)^2 + y_2^2}$$

$$\frac{d\Delta}{dx} = n_1 \cdot \frac{1}{2} \frac{-2(x-x_1)dx}{\sqrt{(x-x_1)^2 + y_1^2}} + n_2 \cdot \frac{1}{2} \frac{-2(x_2-x)dx}{\sqrt{(x_2-x)^2 + y_2^2}} = 0$$

$$\frac{n_1(x-x_1)}{\sqrt{(x-x_1)^2 + y_1^2}} = \frac{n_2(x_2-x)}{\sqrt{(x_2-x)^2 + y_2^2}} \quad \therefore \sin i_1 \cdot n_1 = \sin i_2 \cdot n_2$$

4. 全反射

$\frac{\sin i}{\sin r} = n$, 当 $i = 90^\circ$, 即折射角为 90° 时, 发生全反射.

此时 $\sin \alpha = \frac{1}{n}$, $\alpha = \arcsin \frac{1}{n}$ ($n = \frac{c}{v}$, 光密介质的 n 大, 光疏介质的 n 小)

专题: 光子

1. 理论基础:

$$E = h\nu, p = \frac{h\nu}{c} = \frac{h}{\lambda}$$

$$\because E^2 = p^2 c^2 + m_0^2 c^4, \text{ 而 } m_0 = 0 \therefore p = \frac{E}{c}$$

$$\begin{aligned} \therefore m &= \frac{m_0}{\sqrt{1 - v^2/c^2}} = \sqrt{\frac{E^2 - p^2 c^2}{c^4}} = \sqrt{\frac{E^2 - p^2 c^2}{c^2(c^2 - v^2)}} = \sqrt{\frac{h^2 \nu^2 - p^2 c^2}{c^2(c^2 - v^2)}} \\ &= \sqrt{\frac{\frac{h^2 c^2}{\lambda^2} - m^2 c^4}{c^2(c^2 - v^2)}} = \sqrt{\frac{\frac{h^2}{\lambda^2} - m^2 c^2}{c^2 - v^2}} \end{aligned}$$

$$\therefore m^2(c^2 - v^2) = \frac{h^2}{\lambda^2} - m^2 c^2 \quad \therefore m^2(c^2 - v^2) = \frac{h^2}{\lambda^2}$$

$$\therefore v = c, \quad \therefore m = \frac{h}{c\lambda} = \frac{h\nu}{c^2} \quad \text{此为光子的动质量.}$$

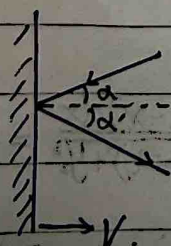
2. 光压: 一群光子的动量 $p = \frac{N h \nu}{c} = \frac{\Phi}{c}$

若壁的反射系数 p , 则 $\Delta I_1 = p \frac{\Phi}{c} - (-p \frac{\Phi}{c}) = 2p \frac{\Phi}{c}$.

余下 $(1-p)N$ 个光子被壁吸收, 则 $\Delta I_2 = (1-p) \frac{\Phi}{c}$

$$\therefore \text{光压} = \Delta I_1 + \Delta I_2 = (1+p) \frac{\Phi}{c}$$

3. 反射定律推广:



$$\begin{cases} h\nu + \frac{1}{2} M V^2 = h\nu' + \frac{1}{2} M V'^2 & (1) \end{cases}$$

$$\begin{cases} M V - \frac{h\nu \cos \alpha}{c} = M V' + \frac{h\nu' \cos \alpha'}{c} & (2) \end{cases}$$

$$\begin{cases} h\nu \sin \alpha = h\nu' \sin \alpha' & (3) \end{cases}$$

$$\text{由(1)得 } h(\nu' - \nu) = \frac{1}{2} M (V^2 - V'^2)$$

$$\text{由(2)得 } \frac{h}{c} (\nu \cos \alpha + \nu' \cos \alpha') = M (V - V')$$

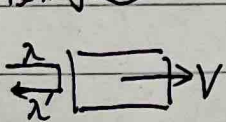
$$\therefore c \frac{v'-v}{v \cos \alpha + v' \cos \alpha'} = \frac{1}{2}(v+v') \approx v$$

由(3)得 $v' = \frac{\sin \alpha}{\sin \alpha'} v$, 代入上式得:

$$v = \frac{\frac{\sin \alpha}{\sin \alpha'} - 1}{\cos \alpha + \frac{\sin \alpha}{\sin \alpha'} \cos \alpha'} c = \frac{\sin \alpha - \sin \alpha'}{\sin \alpha' \cos \alpha + \sin \alpha \cos \alpha'} c = \frac{\sin \alpha - \sin \alpha'}{\sin(\alpha + \alpha')} c$$

即 $\sin \alpha - \sin \alpha' = \rho \sin(\alpha + \alpha')$. 若 v 与 v' 成 ϕ 角, 则 $\sin \alpha - \sin \alpha' = \rho \sin \phi \sin(\alpha + \alpha')$.

4. 红移测速.



$$\begin{cases} \frac{h}{\lambda} + Mv = -\frac{h}{\lambda'} + Mv' \\ \frac{hc}{\lambda} + \frac{1}{2}Mv^2 = \frac{hc}{\lambda'} + \frac{1}{2}Mv'^2 \end{cases}$$

$$\therefore h\left(\frac{1}{\lambda} + \frac{1}{\lambda'}\right) = M(v'-v)$$

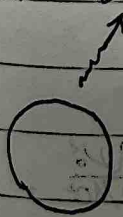
$$\therefore c \frac{\lambda - \lambda'}{\lambda + \lambda'} = \frac{1}{2}(v'+v) \approx v$$

$$hc\left(\frac{1}{\lambda} - \frac{1}{\lambda'}\right) = \frac{1}{2}M(v'^2 - v^2)$$

$$\therefore v = \frac{\lambda' - \lambda}{\lambda + \lambda'} \cdot c$$

$$\text{又: 红移量 } \frac{\lambda' - \lambda}{\lambda} = z, \therefore v = \frac{z}{2+z} \cdot c$$

5. 引力红移.

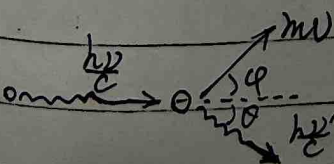


$$h\nu - \frac{GMm}{r} = h\nu' - \frac{GMm'}{r}$$

$$\therefore h\nu\left(1 - \frac{GM}{c^2 r}\right) = h\nu'\left(1 - \frac{GM}{c^2 r}\right)$$

$$\therefore \nu' = \frac{1 - \frac{GM}{c^2 r}}{1 - \frac{GM}{c^2 r}} \nu$$

6. 康普顿效应



由动量守恒和余弦定理:

$$(m v')^2 = \left(\frac{h\nu}{c}\right)^2 + \left(\frac{h\nu'}{c}\right)^2 - 2 \frac{h\nu}{c} \frac{h\nu'}{c} \cos \theta$$

由能量守恒:

$$m_0 c^2 + h\nu = m c^2 + h\nu'$$

由 $m = \frac{m_0}{\sqrt{1-v^2/c^2}}$, 得 $mc^2 = m^2 v^2 + m_0^2 c^2$. $\therefore (mc^2)^2 = (mv)^2 c^2 + m_0^2 c^4$.

将前式代入此式.

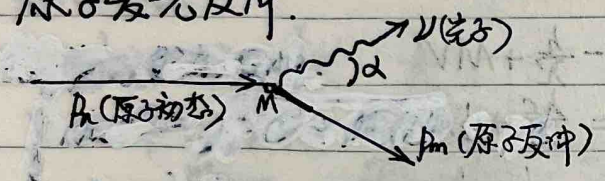
$$(m_0 c^2 + h\nu - h\nu')^2 = \left[\left(\frac{h\nu}{c}\right)^2 + \left(\frac{h\nu'}{c}\right)^2 - \frac{2h^2 \nu \nu' \cos\theta}{c^2} \right] c^2 + m_0^2 c^4$$

展开, 得: $m_0^2 c^4 + 2m_0 c^2 h(\nu - \nu') + h^2 (\nu - \nu')^2 = h^2 \nu^2 + h^2 \nu'^2 - 2h^2 \nu \nu' \cos\theta + m_0^2 c^4$

$$\therefore m_0 c^2 (\nu - \nu') = h \nu \nu' (1 - \cos\theta)$$

$$\therefore \frac{\nu - \nu'}{\nu \nu'} \approx \frac{\Delta \nu}{\nu^2} = \frac{2h}{m_0 c^2} \nu^2 \frac{\theta}{2}$$

7. 原子发光反冲



忽略原子质量变化, 由能量守恒和动量守恒, 得:

$$\begin{cases} \frac{P_n^2}{2M} + E_n = \frac{P_m^2}{2M} + E_m + h\nu \\ P_m^2 = P_n^2 + p^2 - 2P_n p \cos\alpha \end{cases}$$

$$\therefore \nu = \frac{E_n - E_m}{h} + \frac{2P_n p \cos\alpha}{2Mh} - \frac{p^2}{2Mh} \quad \because P_n = Mv_n, \quad p = \frac{h\nu}{c}$$

$$\therefore \nu = \nu_0 + \frac{v_n}{c} \nu_0 \cos\alpha - \frac{h\nu_0^2}{2Mc^2} \approx \nu_0 + \frac{v_n}{c} \nu_0 \cos\alpha - \frac{h\nu_0^2}{2Mc^2}$$

第一项为玻尔频率,

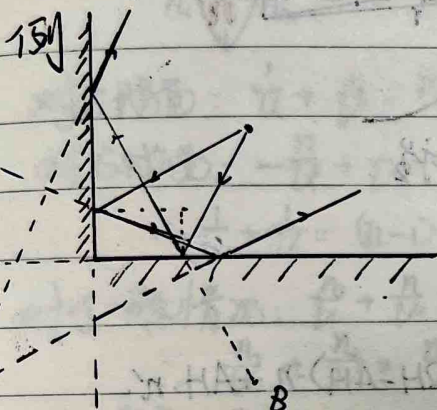
第二项为多普勒效应, 当 $v_n = 0$ 时, 此项为零. $\nu = \nu_0 - \frac{h\nu_0^2}{2Mc^2}$

第三项为原子反冲的结果.

5. 反射镜成像

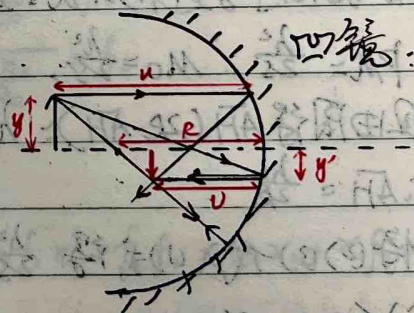
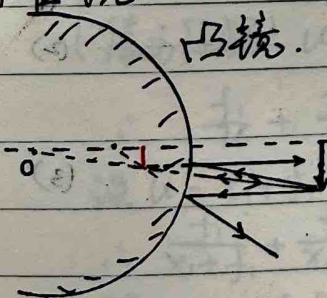
① 平面镜:

判断虚像个数: 让物向每面镜发出一条光线, 让光线在镜组间反射直至射出系统, 每条反射光线的反向延长线必经过一虚像。



实像: 实际光线汇聚成的像。
虚像: 光线反向延长线汇聚成的像。

② 球面镜



由图得 $\frac{u-R}{R-v} = \frac{y}{y'} \approx \frac{u-R+\frac{R}{2}}{\frac{R}{2}} = \frac{u-\frac{R}{2}}{\frac{R}{2}}$

得 $\frac{1}{u} + \frac{1}{v} = \frac{2}{R} = \frac{1}{f}$, ($f = \frac{R}{2}$: 对近轴光线的近似)

符号法则: 物在镜前 (能反射的一侧), $u > 0$; 物在镜后, $u < 0$ 。

实像 $v > 0$; 虚像 $v < 0$ (在对侧设为正, 解出后有正号)。

凹镜 $f > 0$; 凸镜 $f < 0$ 。

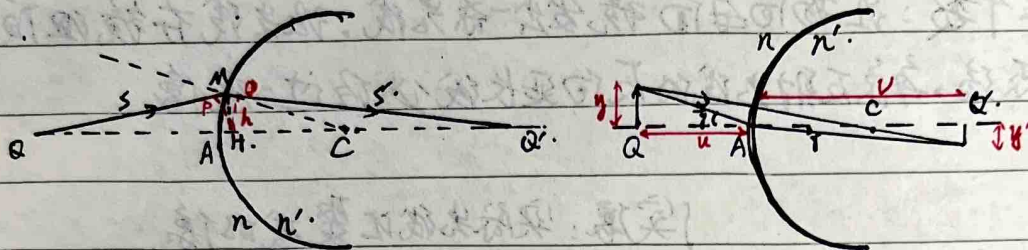
放大率: 设倒立的像高为 y'

$\therefore \frac{y'}{y} = \frac{u-R}{u-R} = \frac{v-\frac{R}{2}}{u-\frac{R}{2}} = \frac{v-\frac{R}{2}}{u-\frac{R}{2}} = -\frac{v}{u}$

即 $K = -\frac{v}{u}$

6. 透镜成像.

① 单球面折射.



根据费马原理, 光路 $QM Q'$ 与 $QAHCQ'$ 等光程.

$$\therefore QM \cdot n + MQ \cdot n' = QA \cdot n + AQ' \cdot n'$$

$$\because QH = QP, QH = QO.$$

$$\therefore QP \cdot n + PM \cdot n + MO \cdot n' = QA \cdot n + AH \cdot n' = (QH - AH) \cdot n + AH \cdot n'.$$

$$\therefore PM \cdot n + MO \cdot n' = AH(n' - n) \quad (1)$$

根据几何学近似公式, 对于近轴光线 $QM Q'$ 有

$$PM = \frac{h^2}{2s}, \quad MO = \frac{h^2}{2s'},$$

$$\text{且由图得 } AH(2R - AH) = h^2 \approx AH \cdot 2R$$

$$\therefore AH = \frac{h^2}{2R} \quad (2)$$

$$\text{将(2)(3)代入(1)式得 } \frac{h^2}{2s} \cdot n + \frac{h^2}{2s'} \cdot n' = \frac{h^2}{2R}(n' - n)$$

$$\because s \approx u, \quad s' \approx v$$

$$\therefore \frac{n}{u} + \frac{n'}{v} = \frac{n' - n}{R}$$

$$\text{焦距: } \begin{cases} \text{物方焦距: } v \rightarrow \infty \text{ 时, } u = \frac{Rn}{n' - n} = f_1; \\ \text{像方焦距: } u \rightarrow \infty \text{ 时, } v = \frac{Rn'}{n' - n} = f_2. \end{cases}$$

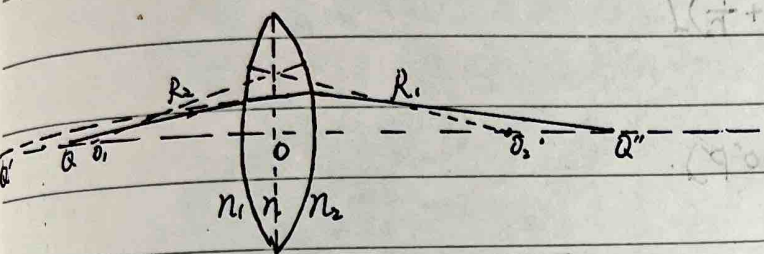
符号法则: 公式中 $n' - n$ 的顺序不变, P 有 u, v, R 的符号变.

$\left\{ \begin{array}{l} Q(\text{物}) \text{ 在顶点 } A \text{ 左, } u > 0, \text{ 否则为负;} \\ Q'(\text{像}) \text{ 在顶点 } A \text{ 右, } v > 0, \text{ 否则为负;} \\ C(\text{球心}) \text{ 在 } A \text{ 右, 规定 } R > 0, \text{ 反之为负.} \end{array} \right.$

$$\text{放大率: } K = \frac{v'}{u} = -\frac{v'f_1}{u v} = -\frac{v'}{u} \frac{n}{n'}$$

② 薄透镜成像:

$$\frac{1}{f} = \frac{1}{R_1} - \frac{1}{R_2} = \frac{n-1}{R_1} - \frac{n-1}{R_2} = (n-1) \left(\frac{1}{R_1} - \frac{1}{R_2} \right)$$



对左球面: $\frac{1}{u} + \frac{n}{v} = \frac{n-1}{R_1}$

对右球面: $-\frac{n}{v} + \frac{1}{v'} = \frac{1-n}{R_2}$

$\therefore \frac{1}{u} + \frac{1}{v} = (n-1) \left(\frac{1}{R_1} + \frac{1}{R_2} \right), f = \frac{1}{(n-1) \left(\frac{1}{R_1} + \frac{1}{R_2} \right)}$

对于一般情况: $\frac{n_1}{u} + \frac{n}{v} = \frac{n-n_1}{R_1}, -\frac{n}{v} + \frac{n_2}{v'} = \frac{n_2-n}{R_2}$

$\therefore \frac{n_1}{u} + \frac{n_2}{v} = \frac{n-n_1}{R_1} + \frac{n-n_2}{R_2}$

当 $\frac{n-n_1}{R_1} + \frac{n-n_2}{R_2} > 0$ 时, 为会聚透镜, 反之为发散透镜.

物距/物方焦距: $v \rightarrow \infty$ 时, $u = \frac{n_1}{\frac{n-n_1}{R_1} + \frac{n-n_2}{R_2}} = f_1$

像方焦距: $u \rightarrow \infty$ 时, $v = \frac{n_2}{\frac{n-n_1}{R_1} + \frac{n-n_2}{R_2}} = f_2$

$\therefore \frac{f_1}{u} + \frac{f_2}{v} = 1$

设 $u = x_1 + f_1, v = x_2 + f_2$

$\therefore \frac{f_1}{x_1 + f_1} + \frac{f_2}{x_2 + f_2} = 1 \quad \therefore f_1 x_2 + f_1 f_2 + f_2 x_1 + f_2 f_1 = x_1 x_2 + x_1 f_2 + f_1 x_2 + f_1 f_2$

得 $x_1 x_2 = f_1 f_2$

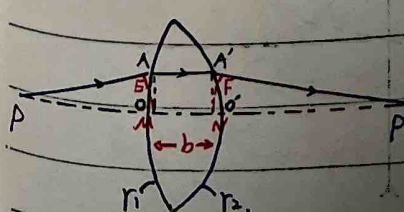
符号法则: 实物 $u > 0$, 虚物 $u < 0$

实像 $v > 0$, 虚像 $v < 0$

凸透镜 $f > 0$, 凹透镜 $f < 0$

放大率: $K = K_1 \cdot K_2 = \left(-\frac{v'}{u} \right) \cdot \left(-\frac{v}{u'} \right) = -\frac{v}{u}$

薄透镜近轴光线成像光程的证明:



$\Delta(PAA'P') = \Delta P'OO'P' = (PA + nAA' + A'P') - (P'O + n.OO' + O'P')$

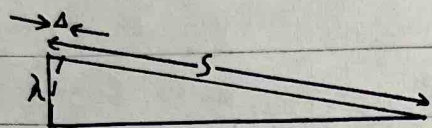
$= (PE + EA + n.AA' + AF + FR) - [PM - OM + n(OM + MN + NO) + NP' - NO']$

$\because AA' \approx MN = b, PE = PM, P'F = P'N$

原式 = $EA + A'F + OM + NO' - n \cdot OM - n \cdot NO'$

$$\begin{aligned} &\approx \frac{h^2}{2 \cdot PA} + \frac{h^2}{2PA'} + \frac{h^2}{2f_1} + \frac{h^2}{2f_2} - n \frac{h^2}{2f_1} + n \frac{h^2}{2f_2} \\ &= \frac{h^2}{2} \left[\frac{1}{u} + \frac{1}{v} + (1-n) \left(\frac{1}{f_1} + \frac{1}{f_2} \right) \right] \\ &= \frac{h^2}{2} \left(\frac{1}{u} + \frac{1}{v} - \frac{1}{f} \right) \\ &= 0 \quad \therefore \Delta(PAA'P') = \Delta(P00'P') \end{aligned}$$

($\Delta \approx \frac{h^2}{2}$ 的证明)



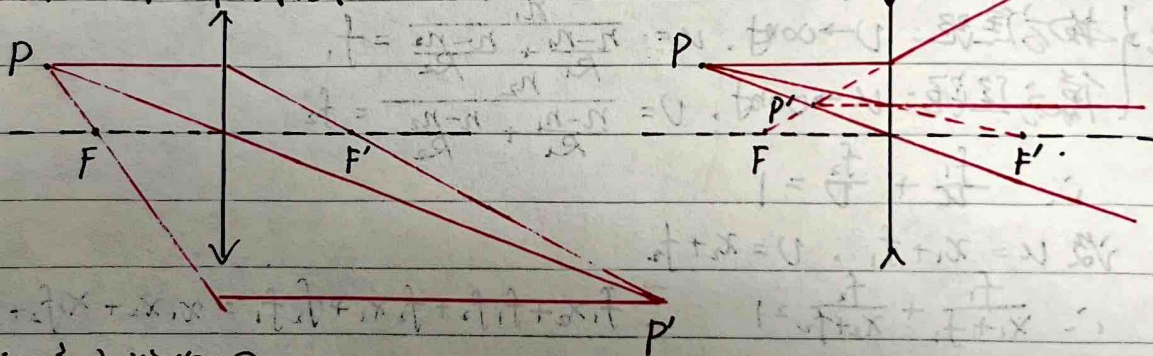
$$\because \sqrt{S^2 - h^2} = S - \Delta$$

$$\therefore S^2 - h^2 = S^2 - 2S\Delta + \Delta^2$$

$$\because \Delta^2 \approx 0 \quad \therefore \Delta = \frac{h^2}{2S}$$

③ 作图法:

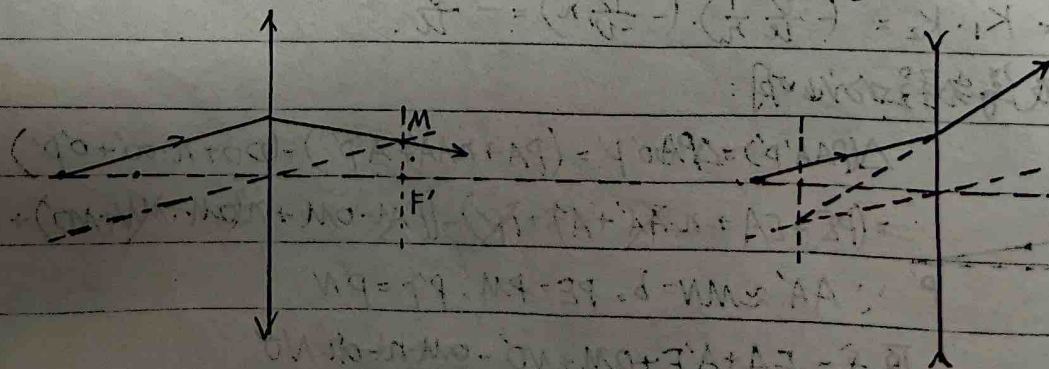
1) 特征光线作图法:



2) 任意光线作图法:

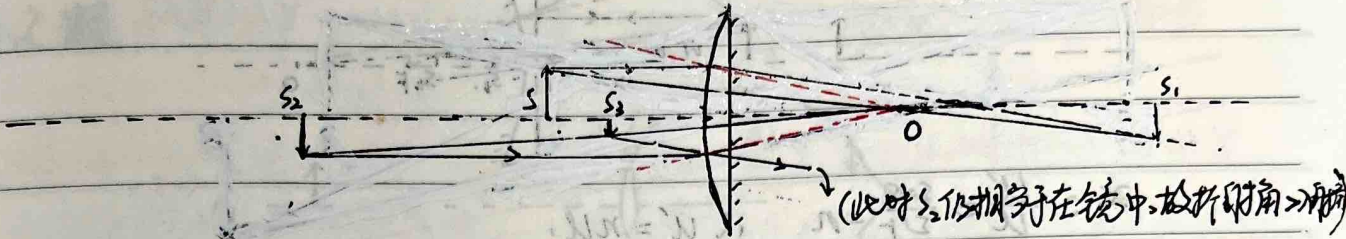
平行于副光轴的光线经透镜折射后通过焦平面与副光轴交点。

证明: 将 M 看成一实物, 由于它在焦平面上, 它必成不了像, 即由它发出的光线经折射后与它和光心的连线平行, 如图:



专题：镀银透镜

1. 凸平薄透镜 (半径 R , 折射率 n)



$$\frac{1}{u} + \frac{n}{v} = \frac{n-1}{R}, \text{ 经反射 } u' = -v \therefore -\frac{n}{v} + \frac{1}{v} = \frac{1-n}{R} \text{ (正方向反向)}$$

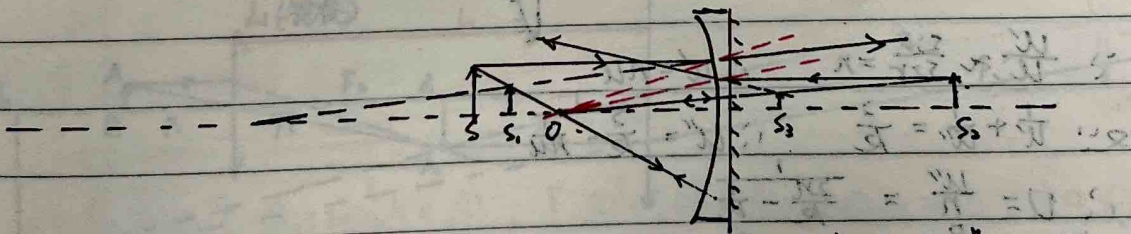
$$\text{解得 } v' = \frac{1}{\frac{1}{u} + \frac{2(n-1)}{R}}$$

$$\text{放大率 } k = \left(-\frac{v'}{u}\right) \cdot (-\frac{v}{v'}) = -\frac{v'}{u}$$

焦距：当平行光射入时：

$$\left. \begin{cases} \frac{1}{\infty} + \frac{n}{v} = \frac{n-1}{R} \\ -\frac{n}{v} + \frac{1}{f} = \frac{1-n}{R} \end{cases} \right\} f = \frac{R}{2(n-1)}$$

2. 凹平薄透镜 (半径 R , 折射率 n)



$$\frac{1}{u} + \frac{n}{v} = \frac{n-1}{R}, \text{ 经反射 } u' = -v, \therefore -\frac{n}{v} + \frac{1}{v} = \frac{1-n}{R} \text{ (正方向反向)}$$

$$\text{解得 } v' = \frac{1}{\frac{1}{u} + \frac{2(n-1)}{R}}$$

$$\text{放大率 } k = \left(-\frac{v'}{u}\right) \cdot (-\frac{v}{v'}) = -\frac{v'}{u}$$

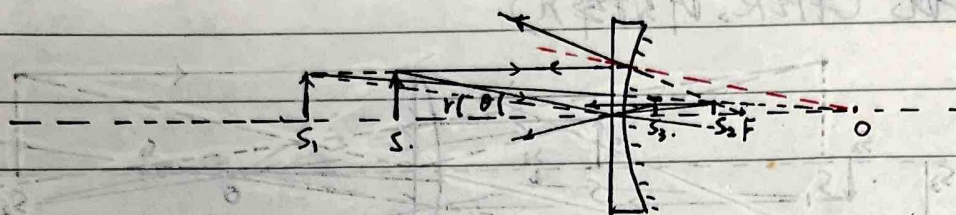
焦距：当平行光射入时：

$$\left. \begin{cases} \frac{1}{\infty} + \frac{n}{v} = \frac{n-1}{R} \\ -\frac{n}{v} + \frac{1}{f} = \frac{1-n}{R} \end{cases} \right\} f = \frac{R}{2(n-1)}$$

3. 平凸薄透镜 (半径 R , 折射率 n)

No.

Date



$$\therefore \frac{u'}{u} \approx \frac{s'O}{s_1 O} = n \quad \therefore u' = nu$$

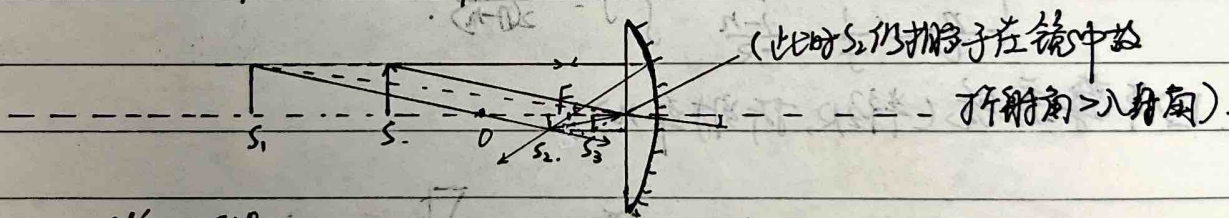
$$\therefore \frac{1}{u} + \frac{1}{u'} = -\frac{2}{R} \quad \therefore u' = -\frac{2}{R} - \frac{1}{nu}$$

$$\therefore \nu = \frac{u'}{u} = -\frac{2n}{R} - \frac{1}{u}$$

$$\text{焦距: } \frac{R}{f} \approx n, \quad \therefore f = -\frac{R}{2n}$$

$$\text{放大率: } k = -\frac{u'}{u} = \frac{2}{R} + \frac{1}{nu} \quad \frac{1}{nu} = \left(\frac{2nu}{R} + 1 \right)^{-1}$$

4. 平凹薄透镜 (半径 R, 折射率 n)



$$\therefore \frac{u'}{u} \approx \frac{s'O}{s_1 O} = n \quad \therefore u' = nu$$

$$\therefore \frac{1}{u} + \frac{1}{u'} = \frac{2}{R} \quad \therefore u' = \frac{2}{R} - \frac{1}{nu}$$

$$\therefore \nu = \frac{u'}{u} = \frac{2n}{R} - \frac{1}{u}$$

$$\text{焦距: } \frac{R}{f} = n, \quad \therefore f = \frac{R}{2n}$$

$$\text{放大率: } k = -\frac{u'}{u} = \frac{2nu}{R} - 1$$

5. 凸凹薄透镜 (半径 R1, R2, 折射率 n) ...



$$\frac{1}{u} + \frac{1}{v_1} = \frac{n-1}{R_1}, \quad \therefore v_1 = \frac{n}{\frac{n-1}{R_1} - \frac{1}{u}}, \quad \therefore u_2 = -v_1, \quad \frac{1}{v_2} + \frac{1}{v_3} = \frac{2}{R_2}$$

$$\therefore v_2 = \frac{2}{\frac{2}{R_2} + \frac{1}{v_1}} = \frac{2}{\frac{2}{R_2} + \frac{1}{n} - \frac{1}{nu}} \quad \therefore u_3 = -v_2, \quad \frac{1}{v_3} + \frac{1}{v_3} = \frac{1-n}{R_1} \quad (\text{正方向反向})$$

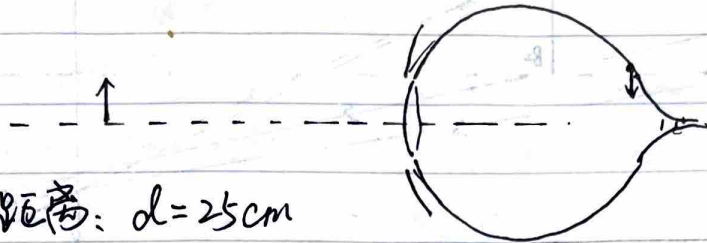
$$\therefore v_3 = \frac{2(n-1)}{\frac{2(n-1)}{R_1} + \frac{2n}{R_2} - \frac{1}{u}}$$

$$\text{焦距: } u \rightarrow \infty \text{ 时, } f = \frac{2(n-1)}{\frac{2(n-1)}{R_1} + \frac{2n}{R_2}}$$

$$\text{放大率: } k = \left(-\frac{v_2}{u}\right) \left(-\frac{v_3}{v_2}\right) \left(-\frac{v_3}{v_3}\right) = -\frac{v_3}{u}$$

7. 光学仪器.

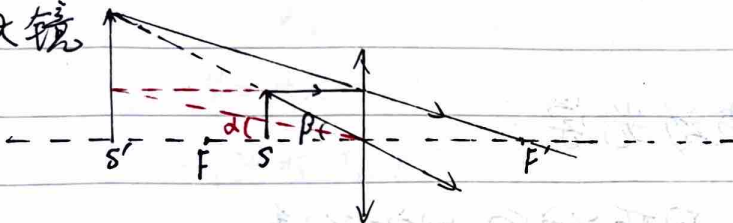
① 人眼



明视距离: $d = 25\text{cm}$

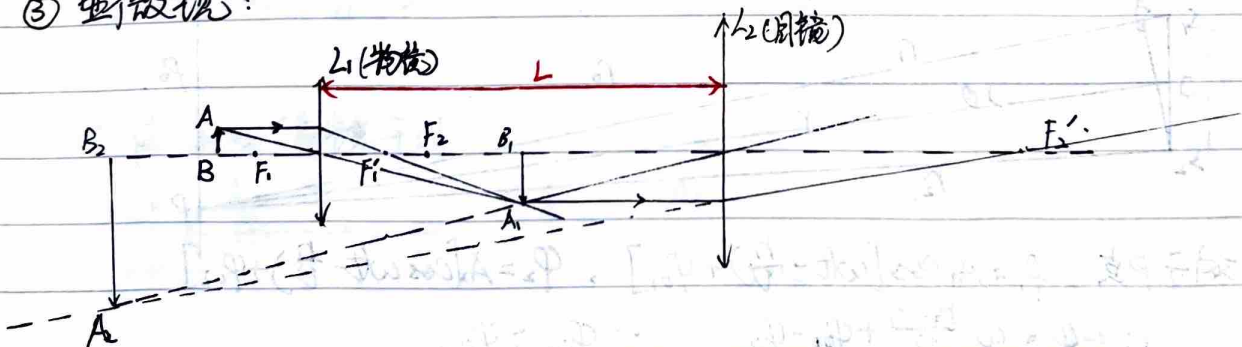
即眼能看清像的最小距离, 为一般光学仪器中像到眼或目镜的距离.

② 放大镜



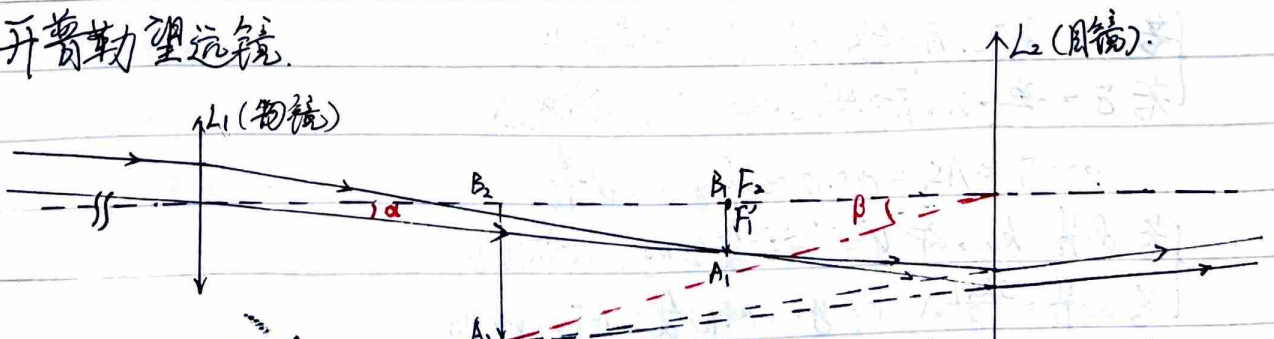
$$k = \frac{\beta}{\alpha} \approx \frac{h/d}{h/f} = \frac{d}{f} \quad (d: \text{明视距离}, f: \text{焦距})$$

③ 显微镜:



$$k = \frac{\beta}{\alpha} \approx \frac{A_1 B_1 / d}{AB / f_1} \approx \frac{A_1 B_1 / f_2}{AB / f_1} = \frac{v_1}{f_1} \cdot \frac{d}{f_2} \approx \frac{L}{f_1} \cdot \frac{d}{f_2} = \frac{Ld}{f_1 f_2}$$

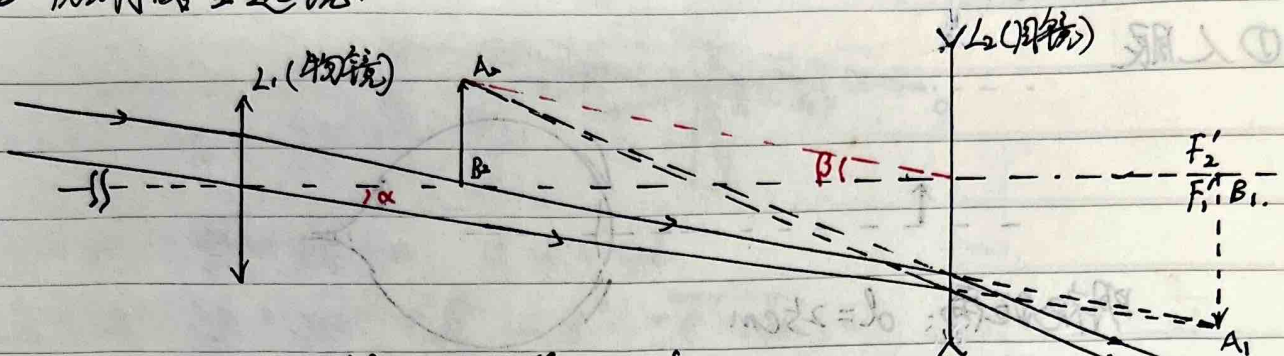
④ 开普勒望远镜



$$k = \frac{\beta}{\alpha} \approx \frac{A_2 B_2 / d}{A_1 B_1 / f_1} \approx \frac{A_1 B_1 / f_2}{A_1 B_1 / f_1} = \frac{f_1}{f_2}$$

目镜 f_2 越小, 物镜 f_1 越大, k 越大.

⑤ 伽利略望远镜.

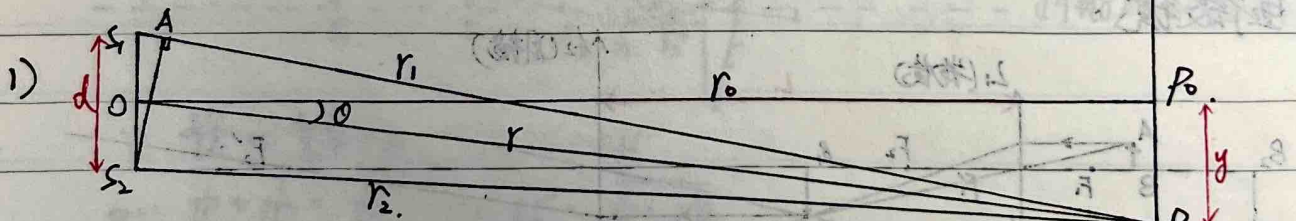


$$K = \frac{\beta}{\alpha} = \frac{A_1 B_1 / f_1}{A B / f_1} = \frac{A_1 B_1 / f_2}{A B / f_1} = \frac{f_1}{f_2} \quad \therefore \text{目镜(凹) } f_2 \text{ 越小 } K \text{ 越大}$$

四. 波动光学

1. 光的干涉: 同频率, 同振动方向, 固定相位差.

① 杨氏双缝干涉:



对于P点, $\varphi_1 = A_1 \cos[\omega t - \frac{r_1}{v}] + \varphi_{01}$, $\varphi_2 = A_2 \cos[\omega t - \frac{r_2}{v}] + \varphi_{02}$

$$\therefore \Delta\varphi = \omega \frac{r_2 - r_1}{v} + \varphi_{01} - \varphi_{02} \quad \because \varphi_{01} = \varphi_{02}$$

$$\therefore \Delta\varphi = \omega \frac{r_2 - r_1}{v} = \frac{2\pi}{\lambda} (r_2 - r_1) = \frac{2\pi}{\lambda} \delta$$

$$\therefore \delta = \frac{\Delta\varphi}{2\pi} \lambda$$

若 $\delta = k\lambda$, 即 $\frac{\Delta\varphi}{2\pi} = k$ 时, 干涉相长

若 $\delta = \frac{2k+1}{2}\lambda$, 即 $\frac{\Delta\varphi}{2\pi} = \frac{2k+1}{2}$ 时, 干涉相消

$$\because \delta \approx AS_1 = d \sin \theta \approx d \tan \theta = d \frac{y}{l}$$

若 $d \frac{y}{l} = k\lambda$, 即 $y = (2k)$ 处时, 干涉相长

若 $d \frac{y}{l} = \frac{2k+1}{2}\lambda$, 即 $y = (2k+1)$ 处时, 干涉相消.

\therefore 明暗条纹间距 $\Delta y = \frac{l}{d} \lambda$

2) 精确解:

若P点干涉相长, 即振动最强, 则P到两点光源 S_1, S_2 的距离差

$$\delta = 2k \cdot \frac{\lambda}{2} \quad (k = 0, 1, 2, \dots)$$

若 k 一定, 则 δ 是一定值, 到两点距离差是定值的点的集合是双曲线,

故两光源为双曲线两焦点. 以 S_1, S_2 所在直线为 y 轴, OP_0 所在直线为 x 轴.

$$\therefore 2a = \delta = 2k \cdot \frac{\lambda}{2}, \therefore a = k \cdot \frac{\lambda}{2} \quad \text{又} \because c = \frac{d}{2}$$

$$\therefore \frac{y^2}{(k \frac{\lambda}{2})^2} - \frac{x^2}{(\frac{d}{2})^2 - (k \frac{\lambda}{2})^2} = 1$$

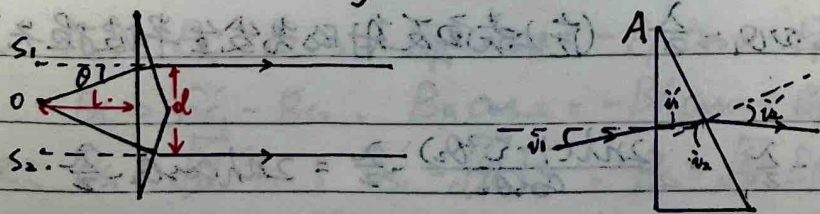
$$\text{当 } x = r_0 \text{ 时, } y = \pm k \cdot \frac{\lambda}{2} \sqrt{1 + \frac{r_0^2}{(\frac{d}{2})^2 - (k \frac{\lambda}{2})^2}}$$

同理, 若P点干涉相消, 即振动最弱, 有

$$\frac{y^2}{(\frac{2k+1}{2} \frac{\lambda}{2})^2} - \frac{x^2}{(\frac{d}{2})^2 - (\frac{2k+1}{2} \frac{\lambda}{2})^2} = 1$$

$$\text{当 } x = r_0 \text{ 时, } y = \pm \frac{2k+1}{2} \frac{\lambda}{2} \sqrt{1 + \frac{r_0^2}{(\frac{d}{2})^2 - (\frac{2k+1}{2} \frac{\lambda}{2})^2}}$$

3) 菲涅尔双棱镜干涉:



取半劈作为研究对象: $n_1 i_1 \approx i_1, n_2 i_2 \approx i_2, i_1 + i_2 = A \cdot \Delta n$

$$\therefore \theta = (i_1 - i_1') + (i_2 - i_2') = (n-1)i_1 + (n-1)i_2 = (n-1)A$$

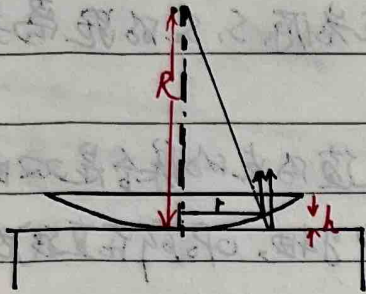
$$\text{又} \because \theta \approx \frac{d}{2l}, \therefore d = 2l(n-1)A$$

$$\text{若 } 2l(n-1)A \cdot \frac{y}{l+f} = k\lambda \text{ 时, 干涉相长}$$

$$2l(n-1)A \frac{y}{l+f} = \frac{2k+1}{2} \lambda \text{ 时, 干涉相消}$$

$$\Delta y = \frac{l+f}{2l(n-1)A} \cdot \lambda$$

③ 牛顿环干涉



$$\delta = 2h - \frac{\lambda}{2}$$

由于透过凸透镜而在平玻璃板上发生反射的光发生半波损失，光程差减去 $\frac{\lambda}{2}$ 。

$\therefore 2h - \frac{\lambda}{2} = 2k \cdot \frac{\lambda}{2}$, $h = (2k+1) \frac{\lambda}{4}$ 时, 干涉相长

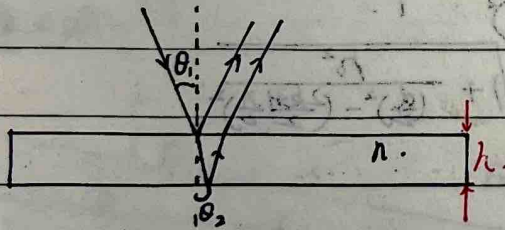
此时 $r^2 = h(2R-h) \approx 2Rh$, $r = \sqrt{2R(2k+1) \frac{\lambda}{4}}$

$2h - \frac{\lambda}{2} = (2k-1) \frac{\lambda}{2}$, $h = (2k) \frac{\lambda}{4}$ 时, 干涉相消

此时 $r = \sqrt{2R \cdot 2k \cdot \frac{\lambda}{4}} = \sqrt{Rk\lambda}$

④ 薄膜干涉

1) 等倾干涉 (非平行光斜入射平玻璃)



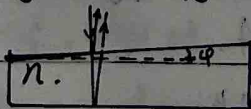
$$\delta = n \cdot \frac{2h}{\cos \theta_2} - 2 \cdot h \tan \theta_2 \cdot \sin \theta_1 - \frac{\lambda}{2} \quad (\text{在上表面反射的光发生半波损失})$$

$$\therefore \sin \theta_1 = n \sin \theta_2$$

$$\therefore \delta = \frac{2nh - 2h \sin \theta_2 \cos \theta_1}{\cos \theta_2} - \frac{\lambda}{2} = \frac{2nh(1 - \sin^2 \theta_2)}{\cos \theta_2} - \frac{\lambda}{2} = 2nh \cos \theta_2 - \frac{\lambda}{2}$$

$\therefore \begin{cases} 2nh \cos \theta_2 - \frac{\lambda}{2} = 2k \cdot \frac{\lambda}{2}, \text{ 即 } 2nh \cos \theta_2 = (2k+1) \frac{\lambda}{2} \text{ 时, 干涉相长.} \\ 2nh \cos \theta_2 - \frac{\lambda}{2} = (2k-1) \frac{\lambda}{2}, \text{ 即 } 2nh \cos \theta_2 = 2k \cdot \frac{\lambda}{2} \text{ 时, 干涉相消.} \end{cases}$

2) 等厚干涉 (光平行垂直入射倾斜小角度的玻璃)

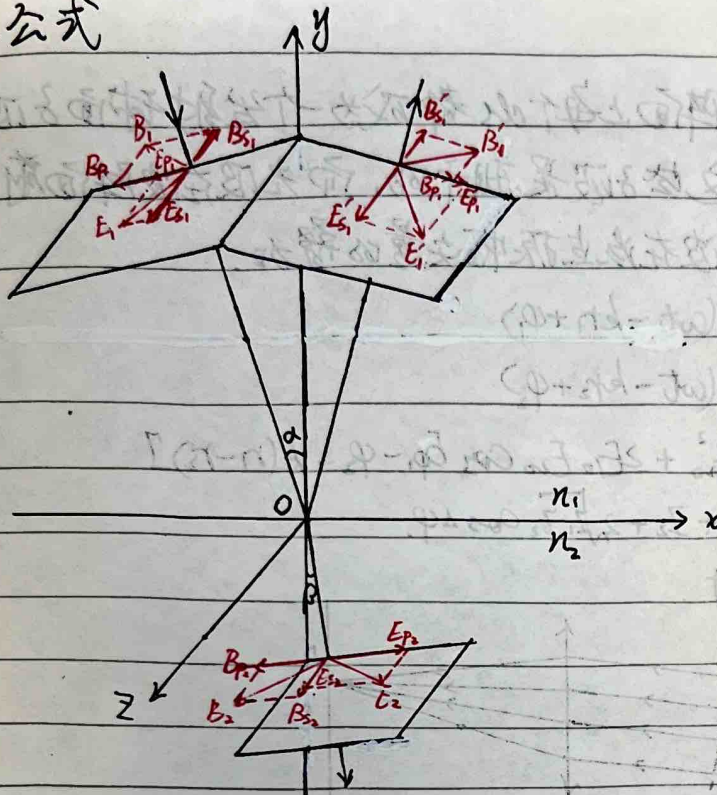


$h = (2k+1) \frac{\lambda}{4n \cos \theta} \approx (2k+1) \frac{\lambda}{4n}$ 时, 干涉相长

$h = 2k \cdot \frac{\lambda}{4n \cos \theta} \approx 2k \cdot \frac{\lambda}{4n}$ 时, 干涉相消

$\therefore \Delta h = \frac{\lambda}{4n}$, $\Delta x = \frac{\Delta h}{\sin \phi} \approx \frac{\lambda}{4n \phi} = \frac{\lambda}{4n \phi}$, 相邻明纹间距 $2\Delta x = \frac{\lambda}{2n \phi}$

⑤ 菲涅耳公式



入射光、反射光、折射光的速度或电矢量 \vec{E} 与磁矢量 \vec{B} 成右手螺旋关系，图中 \vec{E} 、 \vec{E}' 、 \vec{E}'' 已定，取任给一组 \vec{E}_1 、 \vec{E}_2 、 \vec{E}_1' 、 \vec{E}_2' 、 \vec{E}_1'' 、 \vec{E}_2'' 就可给出，将 \vec{E} 分解为各分量的连续性（在临界面处发生反射和折射后不会突变），得：

$$E_{s1} = E_{s1}' + E_{s1}'', \quad E_p \cos \alpha = -E_{p1}' \cos \alpha - E_{p2} \cos \beta. \quad (1)$$

$$B_{s1} = B_{s1}' - B_{s2}, \quad B_p \cos \alpha = -B_{p1}' \cos \alpha + B_{p2} \cos \beta. \quad (2)$$

$$\because B_{s1} = \sqrt{\epsilon_1} E_{s1}, \quad B_{s1}' = \sqrt{\epsilon_1} E_{s1}', \quad B_{s2} = \sqrt{\epsilon_2} E_{s2}. \quad \text{对于波，} \mu_1 = \mu_2 = \mu_0.$$

$$\therefore \sqrt{\epsilon_1} E_{s1} = \sqrt{\epsilon_1} E_{s1}' - \sqrt{\epsilon_2} E_{s2} \quad \therefore n_1 E_{s1} = n_1 E_{s1}' - n_2 E_{s2}$$

$$\because n_1 \sin \alpha = n_2 \sin \beta \quad \therefore E_{s1} = E_{s1}' - \frac{\sin \alpha}{\sin \beta} E_{s2}. \quad (3)$$

$$\text{联立 (1)、(3) 得 } E_p \cos \alpha = -\cos \alpha (E_{s1}' + \frac{\sin \alpha}{\sin \beta} E_{s2}) - E_{p2} \cos \beta.$$

$$\therefore \frac{E_{s2}}{E_{s1}'} = -\frac{2 \cos \alpha \sin \beta}{\sin \alpha \cos \alpha + \sin \beta \cos \beta} = -\frac{2 \cos \alpha \sin \beta}{\sin(\alpha + \beta)} = \frac{2 \cos \alpha \sin \beta}{\sin(\alpha + \beta) \cos(\alpha - \beta)}$$

$$\text{同理，} E_p \cos \alpha = -E_{p1}' \cos \alpha - \frac{\sin \beta}{\sin \alpha} (E_{s1} - E_{s1}') \cos \beta$$

$$\therefore \frac{E_{s1}'}{E_{s1}} = -\frac{\sin \alpha \cos \alpha - \sin \beta \cos \beta}{\sin \alpha \cos \alpha + \sin \beta \cos \beta} = \frac{\tan(\alpha - \beta)}{\tan(\alpha + \beta)}$$

$$\text{还可证：} \frac{E_{s1}'}{E_{s1}} = \frac{\sin(\alpha - \beta)}{\sin(\alpha + \beta)}$$

$$\frac{E_{s2}}{E_{s1}} = \frac{2 \sin \beta \cos \alpha}{\sin(\alpha + \beta)}$$

由此可解释光从射向光密的光层反射产生的半波损失。

2. 光的衍射:

由光源发出的光, 其波阵面上每个 ds 都成为一个发射球面子波的波源, 对局部波阵面来说, 这些子波是相干的, 而光波在波阵面前方某点的振幅矢量是这些子波在该点振幅矢量的叠加.

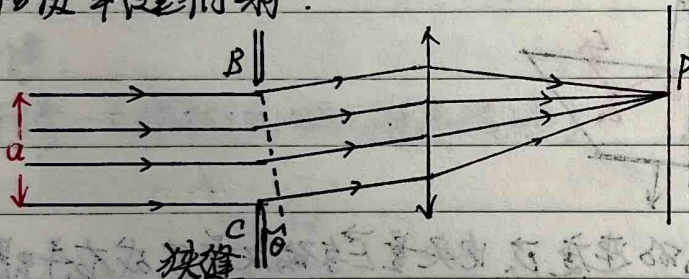
$$E_1 = E_0 \cos(\omega t - kr_1 + \varphi_1)$$

$$E_2 = E_0 \cos(\omega t - kr_2 + \varphi_2)$$

$$\therefore E^2 = E_1^2 + E_2^2 + 2E_1 E_2 \cos[\varphi_1 - \varphi_2 - k(r_1 - r_2)]$$

$$\because I \propto E^2 \quad \therefore I = I_1 + I_2 + 2\sqrt{I_1 I_2} \cos \Delta\varphi$$

① 夫琅和费单缝衍射



P点光强 $I = I_0 \left(\frac{\sin \beta}{\beta}\right)^2$, $\beta = \pi a \sin \theta \Rightarrow \sin \theta = \frac{\beta}{\pi a}$ (由惠更斯菲涅尔原理)

明纹: $\frac{d}{d\beta} \left(\frac{\sin \beta}{\beta}\right) = 0$, 得 $\tan \beta = \beta$

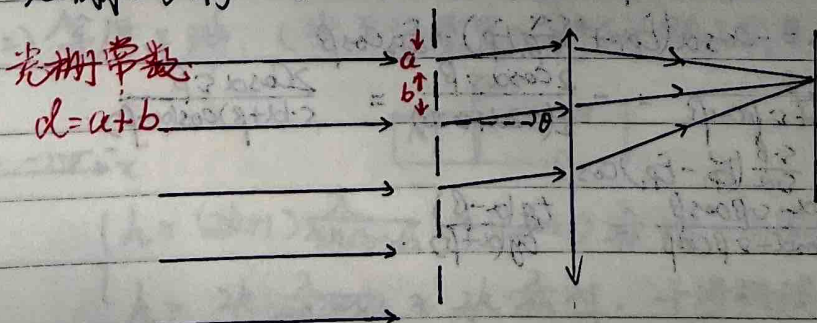
解得 $\sin \theta = 0$, $\sin \theta = \pm 1.43 \frac{\lambda}{a}$, $\pm 2.46 \frac{\lambda}{a}$, $\pm 3.47 \frac{\lambda}{a}$...

暗纹: $\beta = \pm n\pi$ 时, 有 $I = 0$.

解得 $\sin \theta = \pm n \frac{\lambda}{a}$

定义中央明纹宽为两侧一级暗纹中心线间距, 则 $\Delta x \approx 2f \cdot \theta \approx 2f \cdot \frac{\lambda}{a}$ ($n=1$)

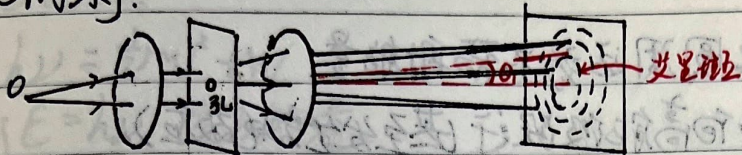
② 光栅衍射 (大量等宽等间距平行狭缝构成的光学元件称为光栅)



主极大: $d \sin \theta = \pm k \lambda$

(即 $\delta = 2k \frac{\lambda}{2}$)

② 圆孔衍射



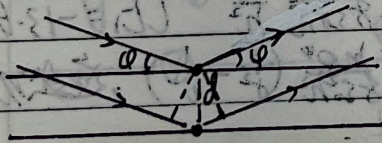
$$d \sin \theta_1 = 1.22 \lambda \Rightarrow \theta_1 \approx 1.22 \frac{\lambda}{d}$$

按几何光学的观点, 只要透镜有适当焦距总能把任何微小物体放大到任何程度, 但事实并非如此! 因为一个物点 \$S\$ 发出的光经过透镜(圆孔), 它的像不再是一个点, 而是艾里斑.

故人眼能分辨的两物点的最小间距 $\Delta l = d \cdot \theta_1 = d \cdot 1.22 \frac{\lambda}{d}$

(d : 明视距离 25cm, λ : 瞳孔直径 2-3mm, λ : 入射光波长)

④ X射线的衍射: 通过X射线在晶格中的衍射研究晶体内部结构.

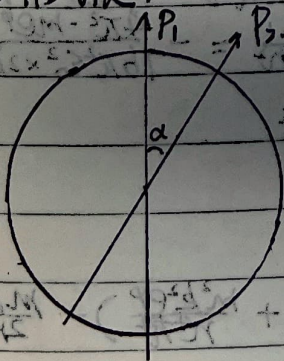


$$\delta = 2d \sin \phi$$

$$\therefore 2d \sin \phi = k\lambda \text{ 干涉相长}$$

— 布拉格公式

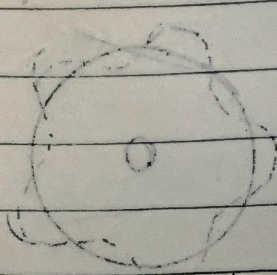
3. 光的偏振



$$I_1 = \sqrt{\epsilon_0} \sum E_{1i}^2$$

$$I_2 = \sqrt{\epsilon_0} \sum (E_{1i} \cos \alpha)^2$$

$$I_1, I_2 = I_1 \cos^2 \alpha, I_1 \sin^2 \alpha$$



$\mu = \frac{v}{c} = \frac{c}{v} = \frac{1}{v/c}$
 $v = \frac{c}{\mu} = \frac{c}{n}$
 $\lambda = \frac{v}{f} = \frac{c}{n f} = \frac{\lambda_0}{n}$

五. 量子光学.

1. 波尔原子理论.

① 假设: 1) 电子做匀速圆周运动不辐射能量.

2) 电子吸收光子向高能级跃迁 (甚至发生光电效应).

电子辐射光子向低能级跃迁 (基态: $n=1$).

3) $mvr = n \frac{h}{2\pi}$, $n=1, 2, 3, \dots$

② 理论与推导:

$$r = \frac{\epsilon_0 h^2}{\pi m e^2} n^2 = n^2 r_1, \quad v = \frac{e^2}{2\epsilon_0 h} \frac{1}{n} = \frac{1}{n} v_1, \quad E = -\frac{m e^4}{8\epsilon_0^2 h^2} \frac{1}{n^2} = \frac{1}{n^2} E_1.$$

$$1) \quad E = \frac{1}{2} m v^2 - \frac{k e^2}{r}$$

$$\because k \frac{e^2}{r} = m v^2, \quad \therefore \frac{1}{2} m v^2 = \frac{k e^2}{2r}, \quad v = \sqrt{\frac{k e^2}{m r}}$$

$$\therefore E = -\frac{k e^2}{2r}$$

$$\text{将 } v = \sqrt{\frac{k e^2}{m r}} \text{ 代入 } m v r = n \frac{h}{2\pi} \text{ 得 } m^2 r^2 \frac{k e^2}{m r} = n^2 \frac{h^2}{4\pi^2}$$

$$\text{解得 } r = \frac{\epsilon_0 h^2}{\pi m e^2} n^2, \quad E = -\frac{m e^4}{8\epsilon_0^2 h^2} \frac{1}{n^2} \quad (E_1 = -13.6 \text{ eV}).$$

$$v = \frac{e^2}{2\epsilon_0 h} \frac{1}{n}, \quad \therefore h\nu = \frac{m e^4}{8\epsilon_0^2 h^2} \left(\frac{1}{j} - \frac{1}{i} \right), \text{ 逸出功 } i \rightarrow \infty, \quad W = \frac{m e^4}{8\epsilon_0^2 h^2}$$

2). $\because p r = n \hbar$

$$\therefore E = \frac{p^2}{2m} - \frac{k e^2}{r} = \frac{p^2}{2m} - \frac{k e^2 p}{n \hbar} = \frac{1}{2m} \left(p - \frac{k m e^2}{n \hbar} \right)^2 - \frac{k^2 m e^4}{2 \hbar^2} \frac{1}{n^2}$$

$$\because \text{能量最小时最稳定}, \quad \therefore E_{\min} = -\frac{k^2 m e^4}{2 \hbar^2} \frac{1}{n^2} = -\frac{4\pi^2 \cdot m e^4}{16\pi^2 \epsilon_0^2 \times 2 \hbar^2} \frac{1}{n^2}$$

$$= -\frac{m e^4}{8\epsilon_0^2 h^2} \frac{1}{n^2}$$

3). 由不确定关系: $\Delta p \cdot \Delta r = h$, $p r = n \hbar$.

$$\therefore E = \frac{p^2}{2m} - \frac{k e^2}{r}$$

$$= \frac{1}{2m} \frac{n^2 \hbar^2}{r^2} - \frac{k e^2}{r} = \frac{n^2 \hbar^2}{2m} \left(\frac{1}{r^2} - \frac{2m k e^2}{n^2 \hbar^2} \frac{1}{r} + \frac{m^2 k^2 e^4}{n^4 \hbar^4} \right) - \frac{m k^2 e^4}{2 \hbar^2} \frac{1}{n^2}$$

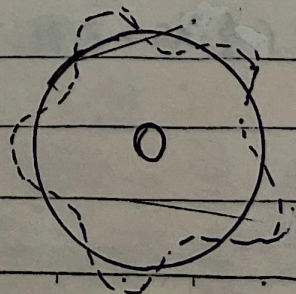
$$\geq -\frac{k m e^4}{2 \hbar^2} \frac{1}{n^2}$$

4) 驻波 (物质波) 条件: $2\pi r = n\lambda$.

$$\therefore r = \frac{n\lambda}{2\pi} = \frac{n\hbar}{2\pi p} \quad \therefore p r = \frac{n\hbar}{2\pi} = n\hbar$$

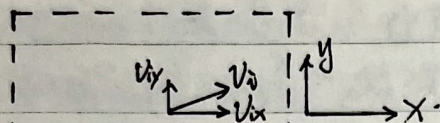
(物质波: 德布罗意波 $E = mc^2 = h\nu$)

$$p = \frac{h\nu}{c} = \frac{h}{\lambda} = mv$$



六. 理想气体.

1. 压强:



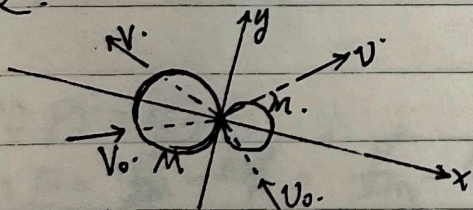
$$p = \frac{\Delta F}{\Delta S} = \frac{\sum l_1}{\Delta S \Delta t} = \frac{\frac{1}{2} \sum (m n_i v_{ix} \Delta t \cdot \Delta S) \cdot 2 v_{ix}}{\Delta S \cdot \Delta t}$$

上式中 $m(n_i v_{ix} \Delta t \Delta S)$ 为 Δt 时间内一个长方体中撞击容器壁的质量。
 $\frac{1}{2}$ 表示 v_{ix} 在 $\pm x$ 方向上概率都是 $\frac{1}{2}$, 由于现在只研究分子撞击右壁的情况, 故只取 $\frac{1}{2}$, $\therefore p = nm \sum \frac{v_{ix}^2}{n}$

$$\therefore \overline{v_x^2} = \frac{\sum v_{ix}^2 n_i}{n} = \frac{1}{3} \overline{v^2}$$

$$\therefore p = \frac{1}{3} n m \overline{v^2} = \frac{2}{3} n \left(\frac{1}{2} m \overline{v^2} \right)$$

2. 温度:



两分子弹性碰撞后, 分子 M 损失动能:

$$\Delta \varepsilon = \frac{1}{2} M (v_0^2 - v^2) \quad (v_{0y} = v_y)$$

$$= \frac{1}{2} M (v_{0x} - v_x)(v_{0x} + v_x)$$

由动量守恒: $v_x = \frac{M v_{0x} + m u_{0x}}{M+m} - \frac{m(v_{0x} - u_{0x})}{M+m} = \frac{(M-m)v_{0x} + 2m u_{0x}}{M+m}$

$$\therefore v_{0x} - v_x = \frac{2m(v_{0x} - u_{0x})}{M+m}, \quad v_{0x} + v_x = \frac{2(M v_{0x} + m u_{0x})}{M+m}$$

$$\therefore \Delta \varepsilon = \frac{2mM}{(M+m)^2} [M v_{0x}^2 - m u_{0x}^2 - (M-m) v_{0x} v_x]$$

对大量 M 取平均, 有 $\overline{\Delta \varepsilon} = \frac{2mM}{(M+m)^2} [M \overline{v_{0x}^2} - m \overline{u_{0x}^2} - (M-m) \overline{v_{0x} v_x}]$

$$\because \overline{v_{0x}} = \overline{u_{0x}} = 0, \quad \therefore \overline{v_{0x} v_x} = 0$$

$$\therefore \overline{\Delta \varepsilon} = \frac{2mM}{3(M+m)^2} (M \overline{v_0^2} - m \overline{u_0^2}) \quad (\overline{v_x^2} = \frac{1}{3} \overline{v^2})$$

$$\propto \frac{1}{2} M \overline{v_0^2} - \frac{1}{2} m \overline{u_0^2}$$

由热力学第零定律, 分子平均动能在宏观上有温度特性, 故设

$$\frac{1}{2} m \overline{v^2} = B \cdot T$$

3. 理想气体状态方程:

由 $p = \frac{2}{3}n(\frac{1}{2}m\bar{v}^2)$ 和 $BT = \frac{1}{2}m\bar{v}^2$, 有

$$p = \frac{2}{3}nBT = \frac{2}{3} \frac{N}{V} BT = \frac{2}{3} \frac{N_A}{V} BT \quad (n: \text{数密度}, \nu: \text{摩尔数})$$

$$\therefore pV = \frac{2}{3} \nu N_A BT \quad (\text{令 } R = \frac{2}{3} N_A B, \text{得})$$

$$pV = \nu RT \quad \therefore T = \frac{1}{B}(\frac{1}{2}m\bar{v}^2) = \frac{2N_A}{3R}(\frac{1}{2}m\bar{v}^2)$$

推论: $pV = \frac{M}{\mu}RT = \frac{pV}{\mu}RT, \therefore \mu p = pRT$

对于同-气体: $\frac{p_1 V_1}{T_1} = \frac{p_2 V_2}{T_2}, \frac{p_1}{T_1} = \frac{p_2}{T_2}$

对于同-系统的所有气体: $\frac{p_1 V_1}{T_1} = R \sum n_i = \sum \frac{p_i V_i}{T_i}$

4. 热力学第一定律应用于理想气体 (ν : 摩尔数)

① 热力学过程: 热力学系统状态不随时间变化的过程 (参量: p, T, V)

{ 准静态: 每一中间态都近似为平衡态

{ 非静态: 中间态不能视为平衡态 (不能用 $p-V$ 图表示)

1) 功: $dW = Fdl = pSdl = pdV$

2) 热量: $dQ = ncdT$ (c : 摩尔热容, 对于固体不变, 对气体可能变)

3) 内能: $dU = \frac{i}{2} nRdT$ (分子热运动: 平动、转动、振动 + 分子内原子间键能)

$i = t + r + 2s$ (t : 平动自由度 = 3, 2, 1, 0; r : 转动自由度 = $3N-6$)

对于单原子分子, $U = N \cdot (\frac{1}{2}m\bar{v}^2) = N \cdot \frac{3}{2}k_B T = \frac{3}{2} nRT$

热力学第一定律: $U_0 + Q - W = U_1, dQ = dU + dW$

(吸热 Q 为正, 对外做功 W 为正)

② 各过程的热解: $dQ = pdV + \frac{i}{2} nRdT$

$pV = nRT$

等容过程: $p = \frac{nR}{V} T$

{ 系统对外界做功: $W = \int pdV = 0$

{ 系统内能变化: $\Delta U = \frac{i}{2} nR\Delta T$

{ 系统从外界吸热: $Q = \frac{i}{2} nR\Delta T = nC_V \Delta T$

2) 等压过程: $V = \frac{nR}{P} \cdot T$

系统对外界做功: $W = \int p dV = p \Delta V = nR \Delta T$

系统内能变化: $\Delta U = \frac{1}{2} nR \Delta T = nC_V \Delta T$

系统从外界吸热: $Q = n(C_V + R) \Delta T = nC_p \Delta T$

3) 等温过程: $p = nRT \cdot \downarrow$

系统对外界做功: $W = \int_{V_1}^{V_2} p dV = nRT \int_{V_1}^{V_2} \frac{dV}{V} = nRT \ln \frac{V_2}{V_1} = -nRT \ln \frac{P_2}{P_1}$

系统内能变化: $\Delta U = \frac{1}{2} nR \Delta T = 0$

系统从外界吸热: $Q = nRT \ln \frac{V_2}{V_1}$

4) 绝热过程: $PV^{\frac{C_p}{C_V}} = P_0 V_0^{\frac{C_p}{C_V}}$

由 $PdV + Vdp = nRdT$ 和 $nC_V dT + PdV = dU + dW = 0$ 得

$$\frac{C_V}{R} (RdV + Vdp) + PdV = 0, \quad R \frac{C_p}{C_V} dV = -C_V \frac{dP}{P}$$

积分得 $\ln \frac{V_2}{V_1} = -\frac{C_V}{C_p} \ln \frac{P_2}{P_1} = \ln \left(\frac{P_1}{P_2} \right)^{\frac{C_V}{C_p}}$, $\therefore PV^{\frac{C_p}{C_V}} = P_0 V_0^{\frac{C_p}{C_V}}$

系统对外界做功: $W = \int_{V_1}^{V_2} P dV = \int_{V_1}^{V_2} \frac{P_0 V_0^{\frac{C_p}{C_V}}}{V^{\frac{C_p}{C_V}}} dV$
 $= P_0 V_0^{\frac{C_p}{C_V}} \int_{V_1}^{V_2} V^{-\frac{C_p}{C_V}} dV = P_0 V_0^{\frac{C_p}{C_V}} \cdot \frac{1}{1 - \frac{C_p}{C_V}} V^{1 - \frac{C_p}{C_V}} \Big|_{V_1}^{V_2} = -\frac{C_V}{R} P_0 V_0^{\frac{C_p}{C_V}} (V_2^{-\frac{R}{C_V}} - V_1^{-\frac{R}{C_V}})$

$= \left[\frac{C_V}{R} P_1 V_1^{\frac{C_p}{C_V}} (V_1^{-\frac{R}{C_V}} - V_2^{-\frac{R}{C_V}}) \right] = \frac{C_V}{R} P_1 V_1 \left[1 - \left(\frac{V_2}{V_1} \right)^{\frac{R}{C_V}} \right]$

$\left[\frac{C_V}{R} P_2 V_2^{\frac{C_p}{C_V}} (V_1^{-\frac{R}{C_V}} - V_2^{-\frac{R}{C_V}}) \right] = \frac{C_V}{R} P_2 V_2 \left[\left(\frac{V_1}{V_2} \right)^{\frac{R}{C_V}} - 1 \right]$

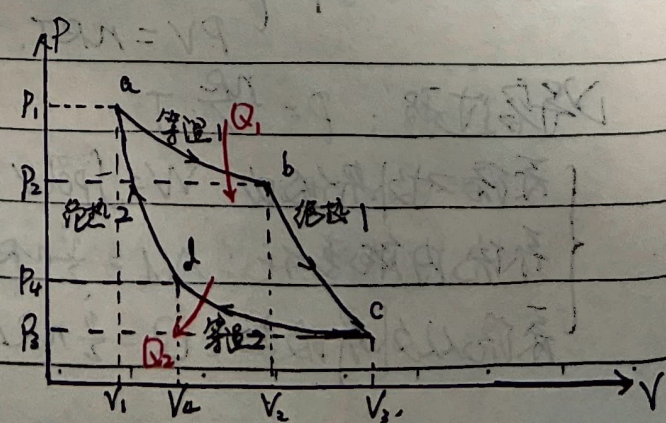
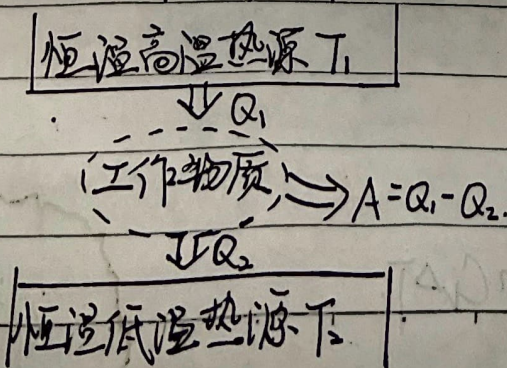
$\therefore P_1 V_1 \left[1 - \left(\frac{V_2}{V_1} \right)^{\frac{R}{C_V}} \right] = P_2 V_2 \left[\left(\frac{V_1}{V_2} \right)^{\frac{R}{C_V}} - 1 \right]$ 解得 $\left(\frac{V_2}{V_1} \right)^{\frac{R}{C_V}} = \frac{P_1 V_1}{P_2 V_2}$

$\therefore W = \frac{C_V}{R} P_1 V_1 \left(1 - \frac{P_2 V_2}{P_1 V_1} \right) = \frac{C_V}{R} (P_1 V_1 - P_2 V_2) = nC_V (T_1 - T_2)$

系统内能变化: $\Delta U = nC_V (T_2 - T_1) = -nC_V \Delta T$

系统从外界吸热: $Q = 0$

5) 理想气体的卡诺循环



(1) $Q_1 = nRT_1 \ln \frac{V_2}{V_1}$: 等温膨胀 ab 中从高温热源吸热 Q_1 .

(2) $T_1 V_2^{\gamma-1} = T_2 V_3^{\gamma-1}$: 绝热过程 bc

(3) $Q_2 = nRT_2 \ln \frac{V_4}{V_3}$: 等温压缩 cd 中向低温热源放热 Q_2 .

(4) $T_2 V_4^{\gamma-1} = T_1 V_1^{\gamma-1}$: 绝热过程 da.

由 (2) (4) 得: $\frac{V_2}{V_1} = \frac{V_4}{V_3}$, 代入 (3), 得

$Q_2 = nRT_2 \ln \frac{V_2}{V_1}$, 与 (1) 比较, 得

$$\frac{Q_2}{T_2} = \frac{Q_1}{T_1}$$

$$\therefore \eta = \frac{A}{Q_1} = \frac{Q_1 - Q_2}{Q_1} = 1 - \frac{T_2}{T_1}$$

5. 饱和汽和未饱和汽. ($n_{\text{总}} = n_{\text{液}} + n_{\text{气}} > n_{\text{液}}$)

性质: ① 同温度下, 不同液体饱和汽压一般不同:

② 一定液体饱和汽压随温度升高而迅速升高.

故当饱和汽体积减小或温度降低时, 汽将液化.

③ 液体沸腾的条件是液体在该温度下的饱和汽压等于外界压强.

计算: 根据道尔顿分压定律, 密闭容器中的气压 $P = P_{\text{液}} + P_{\text{气}}$,

当容器内仍有液态水并处于平衡态时, $P_{\text{气}} = P_{\text{液}}$, 即相对湿度为 100%.

对于空气和水蒸汽共存的混和气体, 当蒸汽未饱和时, 近似遵循

理想气体状态方程, 即 $P_{\text{气}} V = n_{\text{气}} R T$, $P_{\text{液}} V = n_{\text{液}} R T$,

及 $P V = (n_{\text{气}} + n_{\text{液}}) R T$, 当温度降低时, 水蒸汽变成饱和水蒸汽, 再降温或

加压时, 水蒸汽将部分液化, 此时 $P_{\text{液}} V = \frac{P_{\text{液}} V'}{T}$, 而

$$\frac{P_{\text{液}} V}{T R} = \frac{P_{\text{液}} V'}{T R} + n_{\text{液}}'$$

对于空气和水蒸汽共存, 并没有液态水存在时, 可用理想气体状态方程计算.

$$\rho = \frac{\mu_{\text{气}} \cdot n_{\text{气}} + \mu_{\text{液}} \cdot n_{\text{液}}}{V} \quad (\mu_{\text{气}} = 28.8 \text{ g/mol}, \mu_{\text{液}} = 18 \text{ g/mol})$$

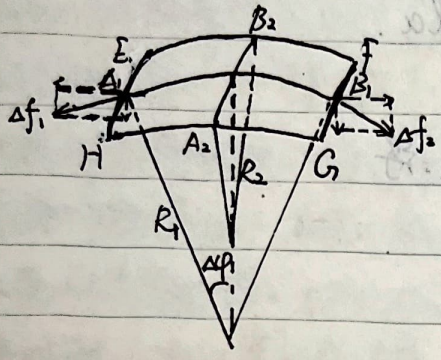
并定义: 绝对湿度 = $P_{\text{液}}$, 相对湿度 = $\frac{P_{\text{液}}}{P_{\text{液}}}$ ($P_{\text{液}}$: 液时实际蒸汽压; $P_{\text{液}}$: 该温度下饱和汽压)

七. 液体与固体.

1. 液体的表面张力

$F = \sigma L$ 方向: 沿所划线法向, 液面切向.

性质: 对于非平面液体表面, 表面张力会引起内外压强差. 如图:



设 $\overline{A_1B_1} = \overline{EF} = \overline{HG} = \Delta l_1$

$\overline{A_2B_2} = \overline{HE} = \overline{GF} = \Delta l_2$

由于 Δf_1 和 Δf_2 的水平分量互相抵消,

$\therefore \Delta f_1$ 与 Δf_2 的合作用为 $(\Delta f_1 + \Delta f_2) \Delta l$

$$= 2\sigma \Delta l_1 \Delta l_2 = 2\sigma \Delta l_1 \cdot \frac{\Delta l_1}{2R_1} = \sigma \Delta l_1 \Delta l_2 = \sigma \Delta S$$

同理对于 A_2B_2 也有合作用 $\sigma \Delta S$.

$\therefore \Delta f_{总} = \sigma(\frac{1}{R_1} + \frac{1}{R_2}) \Delta S$, \therefore 弯曲液面引起的内外压强差 $p = \frac{\Delta f_{总}}{\Delta S} = \sigma(\frac{1}{R_1} + \frac{1}{R_2})$

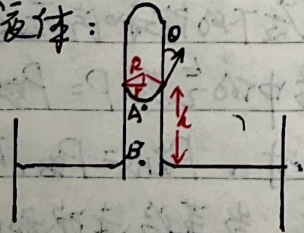
其中 R_1, R_2 为一对相垂直的正截曲面的曲率半径.

对球面, 附加压强 $p_1 = \frac{2\sigma}{R}$

对球膜, 附加压强 $p_2 = 2p_1 = \frac{4\sigma}{R}$.

① 毛细现象

对于浸润液体:

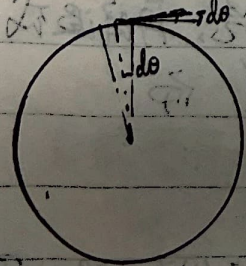


$$P_A = P_0 - \frac{2\sigma}{R}$$

$$P_B = P_A + \rho gh = P_0$$

$$\therefore h = \frac{2\sigma}{\rho g R} \quad \text{又} \because R \cos \theta = r, \therefore h = \frac{2\sigma \cos \theta}{\rho g r}$$

② 肥皂泡的振动



当肥皂泡径向膨胀 x 时, 面上有.

$$dF_{总} = P_0 ds + \frac{4\sigma}{R+x} ds - P' ds \quad (P_0 \text{ 为大气压})$$

平衡时, 有 $P_0 ds + \frac{4\sigma}{R} ds = P' ds$, $\therefore P = P_0 + \frac{4\sigma}{R}$.

由于等温变化, $\therefore P \cdot \frac{4}{3}\pi R^3 = P' \cdot \frac{4}{3}\pi (R+x)^3$, $\therefore P' = (\frac{R}{R+x})^3 \cdot (P_0 + \frac{4\sigma}{R})$

$$\therefore dF_{总} = P_0 [1 - (\frac{R}{R+x})^3] ds + 4\sigma [\frac{1}{R+x} - \frac{R^2}{(R+x)^3}] ds$$

$$\approx P_0 [1 - \frac{R^3}{R^3 + 3Rx^2}] ds + 4\sigma [\frac{1}{R+x} - \frac{R^2}{R^2 + 3Rx^2}] ds$$

$$\approx P_0 (1 - \frac{R^3 x^2}{R^3}) ds + 4\sigma (\frac{R-x}{R^2} - \frac{R-3x}{R^2}) ds$$

$$= \frac{3x}{R} \rho_0 ds + \frac{2x}{R} \cdot \frac{4\sigma}{R} ds$$

$$\therefore dk = \frac{3\rho_0 ds}{R} + \frac{8\sigma ds}{R^2}$$

$$\therefore T = 2\pi \sqrt{\frac{dm}{dk}} = 2\pi \sqrt{\frac{\frac{ds}{4\pi R^2} m}{\left(\frac{3\rho_0}{R} + \frac{8\sigma}{R^2}\right) ds}} = 2\pi \sqrt{\frac{m}{12\pi R \rho_0 + 32\pi \sigma}}$$

此过程中表面张力做功 $W = \int_{R_1}^{R_2} \frac{4\sigma}{R} \cdot 4\pi R^2 \cdot dR = 16\pi\sigma \int_{R_1}^{R_2} R dR = 8\pi\sigma(R_2^2 - R_1^2)$

同样，用表面自由能计算： $W = (2\sigma)(S_2 - S_1) = 2\sigma(4\pi R_2^2 - 4\pi R_1^2) = 8\pi\sigma(R_2^2 - R_1^2)$

(因为液面有两层，每层做功 $\sigma \Delta S$ ，两层则表面张力做功为 $2\sigma \Delta S$)

2. 固体：

① 单晶体：各向异性。

多晶体：各向同性。

非晶体：各向同性。

液体：各向同性。

液晶：各向异性。

② 热膨胀：设固体在 t_0 和 t 时长度分别为 l_0 和 l ，有

$$l = l_0(1 + \alpha t), \quad dl = \alpha l_0 dt$$

设固体在 t_0 和 t 时体积分别为 V_0 和 V ，有

$$V = V_0(1 + \beta t), \quad dV = \beta V_0 dt$$

$$\text{且 } \beta = 3\alpha$$

③ 对于同一固体，溶解热 $Q_1 = \lambda m$ ，汽化热 $Q_2 = Lm$ ，

$$\text{升华热 } Q_3 = Q_1 + Q_2 = (\lambda + L)m$$

④ 热传导：设一块横截面积为 S 、厚度为 x 的板，板两边保持不同温度 ΔT 。

在 dt 时间内垂直于板两面流过的热量为 dQ ，有

$$H = \frac{dQ}{dt} = -ks \frac{\Delta T}{x}$$

$$\left[\text{多层板串联：} H = \frac{-S\Delta T}{\sum (x_i/k_i)} \right.$$

$$\left[\text{多层板并联：} H = -\frac{\Delta T}{x} \sum (k_i S_i) \right.$$

(类比电阻、电容、电感、弹簧的串并联)

八. 静电场

1. 电场力: $\vec{F} = \frac{1}{4\pi\epsilon_0} \frac{q_1 q_2}{r^2} \cdot \vec{r}$

2. 场强: $E = \frac{F}{q_0}$
 $E_0 = \sum E_i$ (对于离散点电荷系统)
 $E_0 = \int dE$ (对于连续带电体)

在静电场中, 高斯定理: $\oint_S E \cdot dS = \frac{q}{\epsilon_0}$ (q为高斯面包围的净电荷)

环路定理: $\oint_L E \cdot dl = 0$

① 点电荷场强分布:

$E = \frac{Q}{4\pi\epsilon_0 r^2}$

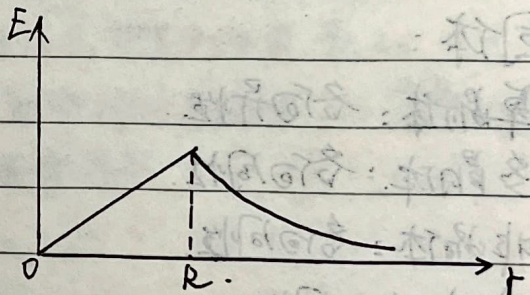
② 实心球 (均匀带电实心球, 电荷体密度处处相等, 电荷不能自由移动) 场强分布

$r < R$ 时, $E \cdot 4\pi r^2 = \frac{1}{\epsilon_0} \frac{4\pi r^3}{3} \rho$

$\therefore E = \frac{Q}{4\pi\epsilon_0 R^3} r$

$r \geq R$ 时, $E \cdot 4\pi r^2 = \frac{1}{\epsilon_0} Q$

$\therefore E = \frac{Q}{4\pi\epsilon_0 r^2}$



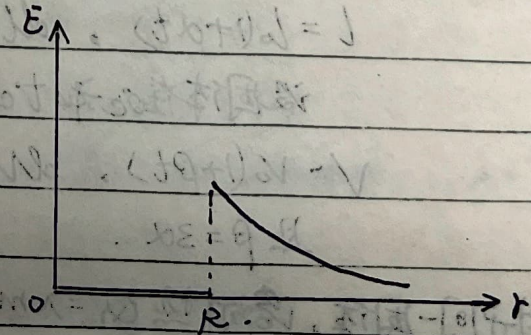
③ 空球壳 (薄导体球壳或空心导体球), 电荷于静电平衡分布于外表面, 电荷可自由移动) 场强分布

$r < R$ 时, $E \cdot 4\pi r^2 = 0$

$\therefore E = 0$

$r \geq R$ 时, $E \cdot 4\pi r^2 = \frac{1}{\epsilon_0} Q$

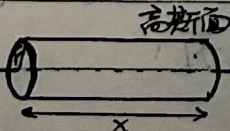
$\therefore E = \frac{Q}{4\pi\epsilon_0 r^2}$



④ 无限长导线 (电荷线密度 λ) 场强分布

$E \cdot 2\pi r \cdot x = \frac{1}{\epsilon_0} \lambda \cdot x$

$\therefore E = \frac{\lambda}{2\pi\epsilon_0 r}$



⑤ 无限宽平板 (电荷面密度 σ) 场强分布.



$$2E \cdot S = \frac{1}{\epsilon_0} S \cdot \sigma$$

$$\therefore E = \frac{\sigma}{2\epsilon_0}$$

⑥ 静电平衡导体表面

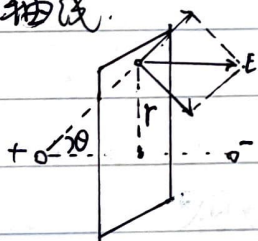


$$E \cdot \Delta S = \frac{1}{\epsilon_0} \Delta S \cdot \sigma$$

$$\therefore E = \frac{\sigma}{\epsilon_0}$$

⑦ 电偶极子 (电矩 $\vec{p} = q\vec{l}$, \vec{E} 由 $-q$ 指向 $+q$).

1) 轴线.

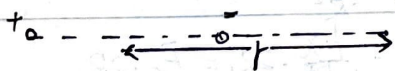


$$E = 2E^+ \cos\theta = 2 \frac{kq}{r^2 + (\frac{l}{2})^2} \cdot \frac{\frac{l}{2}}{\sqrt{r^2 + (\frac{l}{2})^2}} = \frac{kqL}{(r^2 + \frac{l^2}{4})^{\frac{3}{2}}}$$

当 $r \gg l$ 时, 有 $r_+ = r_- = r$.

$$\therefore E \approx \frac{kqL}{r^3} = \frac{kp}{r^3}$$

2) 连线

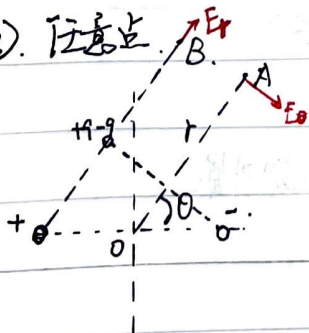


$$E = \frac{kq}{(r - \frac{l}{2})^2} - \frac{kq}{(r + \frac{l}{2})^2}$$

$$= kq \frac{r^2 + r + \frac{l^2}{4} - r^2 + r - \frac{l^2}{4}}{[r^2 - (\frac{l}{2})^2]^2} \approx kq \frac{2r}{r^4} = \frac{2kqL}{r^3}$$

$$\therefore E \approx \frac{2kp}{r^3}$$

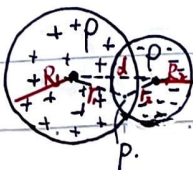
3) 任意点



以 OA 为对称轴作出 $-q$ 的对称电荷 $+q$. 在同处再加 $-q$.
于是组成两个电偶极子. $\therefore E_0 \approx \frac{kqL \cos\theta}{r^3}$, $E_r \approx \frac{2kqL \cos\theta}{r^3}$

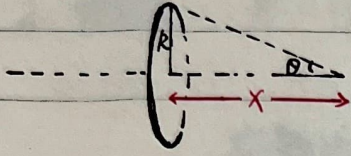
$$\therefore E = \sqrt{E_0^2 + E_r^2} = \frac{kqL}{r^3} \sqrt{\cos^2\theta + 4\cos^2\theta} = \frac{kqL}{r^3} \sqrt{1+3\cos^2\theta}$$

⑧ 重叠实心球重合部分场强 (体密度 ρ).



在重合部分补在 $+P$ 和 $-P$ 的电荷, 有 $\vec{E} = \frac{k \frac{4\pi R^3 \rho}{3}}{r_1^3} \vec{r}_1 - \frac{k \frac{4\pi R^3 \rho}{3}}{r_2^3} \vec{r}_2$
 $= k \frac{4\pi R^3 \rho}{3} (\vec{r}_1 - \vec{r}_2) = \frac{\rho \vec{a}}{3\epsilon_0}$

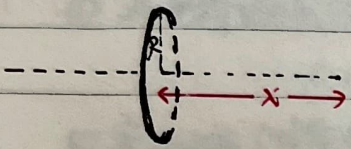
⑨ 带电圆环轴线上场强分布



$$E = \int \frac{k dq}{x^2 + R^2} \cos \theta = \frac{k q}{x^2 + R^2} \frac{x}{\sqrt{x^2 + R^2}}$$

$$= \frac{q x}{4 \pi \epsilon_0 (x^2 + R^2)^{3/2}}$$

⑩ 带电圆板轴线上场强分布



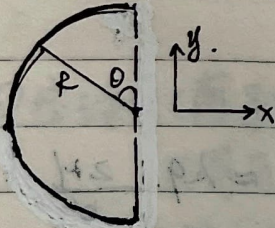
利用上面结论 $E = \int \frac{dq x}{4 \pi \epsilon_0 (x^2 + r^2)^{3/2}}$

$$= \int \frac{(2 \pi r dr \sigma) x}{4 \pi \epsilon_0 (x^2 + r^2)^{3/2}} = \frac{\sigma x}{2 \epsilon_0} \int_0^R \frac{r dr}{(x^2 + r^2)^{3/2}}$$

$$= \frac{\sigma x}{4 \epsilon_0} \int \frac{d(x^2 + r^2)}{(x^2 + r^2)^{3/2}} = \frac{\sigma}{2 \epsilon_0} \left(1 - \frac{x}{\sqrt{x^2 + R^2}} \right)$$

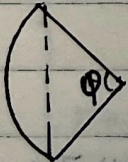
专题: 场强等效求法

1. 由均匀带电半圆环圆心的场强推广为张角为 θ 的弧



$$\begin{cases} dE_y = 0 \text{ (对称性)} \\ dE_x = \frac{k(R dy) \lambda}{R^2} \cos \theta = \frac{k \lambda dy}{R} \cos \theta \end{cases}$$

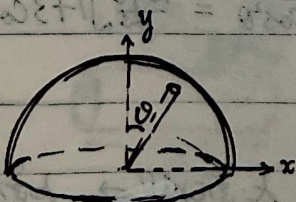
$$\therefore E = \int dE_x = \frac{k \lambda}{R} \int_{-R}^R dy = \frac{k \lambda}{R} \cdot 2R = E_0 \cdot 2R$$



∴ 对张角为 θ 的弧

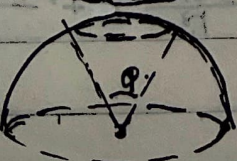
$$E = \frac{k \lambda}{R} \int dy = \frac{k \lambda}{R} \cdot (2R \sin \frac{\theta}{2})$$

2. 由均匀带电半球球心处场强推广为张角为 θ 的球帽



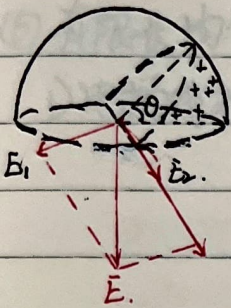
$$\begin{cases} dE_x = 0 \text{ (对称性)} \\ dE_y = \frac{k \sigma ds \cos \theta}{R^2} = \frac{k \sigma ds}{R^2} \cos \theta \end{cases}$$

$$\therefore E = \int dE_y = \frac{k \sigma}{R^2} \int ds_x = \frac{k \sigma}{R^2} \pi R^2 = E_0 \cdot \pi R^2$$



∴ 对张角为 θ 的球帽

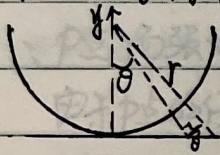
$$E = \frac{k \sigma}{R^2} \int ds_x = \frac{k \sigma}{R^2} \cdot \pi R^2 \left(\sin \frac{\theta}{2} \right)^2$$



$$\therefore \begin{cases} E_1 \cos \theta = E_2 \cos \frac{\pi - \theta}{2} \\ E_1 \sin \frac{\theta}{2} + E_2 \sin \frac{\pi - \theta}{2} = E_0 \cdot \pi R^2 \end{cases}$$

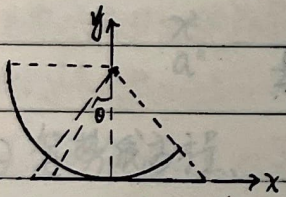
$$\begin{aligned} \text{解得 } E &= (E_0 \cdot \pi R^2) \sin \frac{\theta}{2} \\ &= \frac{kQ}{4\pi R^2} \cdot \pi R^2 \cdot \sin \frac{\theta}{2} \end{aligned}$$

3. 由无限长均匀带电直线外R处场强推广为有限长导线:



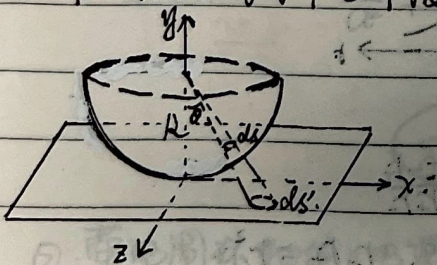
$$\begin{cases} dE_x = 0 \text{ (对称性)} \\ dE_y = \frac{k\lambda dl}{r^2} \cos \theta = \frac{k\lambda \left(\frac{R}{\cos \theta} d\theta\right)}{\left(\frac{R}{\cos \theta}\right)^2} \cdot \cos \theta = \frac{k\lambda R \cos \theta d\theta}{R^2} \\ = \frac{k(\lambda R d\theta)}{R^2} \cos \theta \end{cases}$$

等价于一个半圆导线在其圆心处的场强.



$$\begin{cases} dE_x = \frac{k\lambda dl}{r^2} \cos \theta = \frac{k(\lambda R d\theta)}{R^2} \cos \theta \\ dE_y = \frac{k\lambda dl}{r^2} \sin \theta = \frac{k(\lambda R d\theta)}{R^2} \sin \theta \end{cases}$$

4. 由无限宽均匀带电平板外R处场强推广为长宽有限的平板:

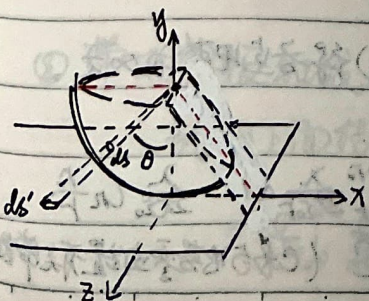


$$\begin{cases} dE_x = dE_z = 0 \text{ (对称性)} \\ dE_y = \frac{k\sigma ds'}{r^2} \cos \theta \end{cases}$$

$$\therefore \frac{ds' \cos \theta}{\left(\frac{R}{\cos \theta}\right)^2} = \frac{ds}{R^2} \quad \therefore ds' = \frac{ds}{\cos^3 \theta}$$

$$\therefore dE_y = \frac{k\sigma \cdot \frac{ds}{\cos^3 \theta} \cdot \cos \theta}{\left(\frac{R}{\cos \theta}\right)^2} = \frac{k\sigma ds}{R^2} \quad (\text{与直导线不同})$$

$$\therefore E = \int dE_y = \frac{k\sigma}{R^2} \cdot 2\pi R^2 = 2\pi k\sigma = \frac{\sigma}{2\epsilon_0}$$



$$\begin{cases} dE_x = \frac{k\sigma ds'}{r^2} \sin \theta \cos \alpha = \frac{k\sigma ds}{R^2} \tan \theta \cos \alpha \\ dE_y = \frac{k\sigma ds'}{r^2} \cos \theta = \frac{k\sigma ds}{R^2} \\ dE_z = 0 \end{cases}$$

3. 电势: $\varphi_a = \int_a^{\infty} \vec{E} \cdot d\vec{l}$ $\left\{ \begin{array}{l} \varphi_a = \frac{1}{4\pi\epsilon_0} \sum \frac{q_i}{r_i} \text{ 离散} \\ \varphi_a = \frac{1}{4\pi\epsilon_0} \int \frac{dq}{r} \text{ 连续} \end{array} \right.$

当无限远无导体时, 无限远处电势为零。
不考虑地球所带电荷时, 大地视为电势为零。

① 点电荷电势分布

$$\varphi_a = \frac{q}{4\pi\epsilon_0} \int_a^{\infty} \frac{dr}{r^2} = \frac{q}{4\pi\epsilon_0} \left(-\frac{1}{r}\right)_a^{\infty} = \frac{q}{4\pi\epsilon_0 a}$$

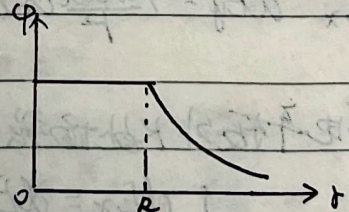
$$U_{ab} = \varphi_a - \varphi_b = \frac{q}{4\pi\epsilon_0} \left(\frac{1}{a} - \frac{1}{b}\right)$$

② 实心球

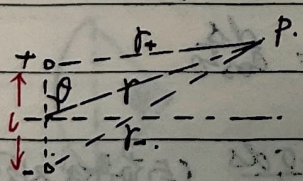
$$\left\{ \begin{array}{l} r \geq R \text{ 时, } \varphi = \int_r^{\infty} E \cdot dl = \frac{q}{4\pi\epsilon_0 r} \\ r < R \text{ 时, } \varphi = \frac{q}{4\pi\epsilon_0 R} + \int_r^R \frac{q}{4\pi\epsilon_0} \cdot \frac{rdl}{R^3} \\ = \frac{q}{4\pi\epsilon_0 R} + \frac{q(R^2 - r^2)}{8\pi\epsilon_0 R^3} = \frac{q(3R^2 - r^2)}{8\pi\epsilon_0 R^3} \end{array} \right.$$

③ 空心球壳

$$\left\{ \begin{array}{l} r \geq R \text{ 时, } \varphi = \frac{q}{4\pi\epsilon_0 r} \\ r < R \text{ 时, } \varphi = \frac{q}{4\pi\epsilon_0 R} \end{array} \right.$$



④ 两根棒子



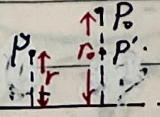
$$\varphi = \frac{q}{4\pi\epsilon_0 r_+} - \frac{q}{4\pi\epsilon_0 r_-} = \frac{q}{4\pi\epsilon_0} \frac{r_- - r_+}{r_+ r_-}$$

当 $r \gg L$ 时, 有 $r_- - r_+ = 2L \cos\theta$, $r_+ r_- = r^2$

$$\therefore \varphi \approx \frac{q}{4\pi\epsilon_0} \frac{2L \cos\theta}{r^2} = \frac{\vec{D} \cdot \vec{r}}{4\pi\epsilon_0 r^2}$$

⑤ 无限长均匀带电直线电势分布

若仍选无限远为电势零点, 则由 $\int_P^{\infty} E \cdot dr$ ($E = \frac{\lambda}{2\pi\epsilon_0 r}$) 得各点电势为无穷大, 故选距带电直线 r_0 的 P 点为电势零点, 如图。

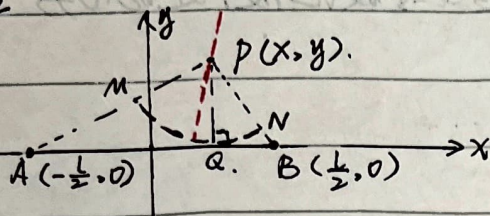


$$\varphi_P = \int_P^{r_0} E \cdot dr + \int_{r_0}^{\infty} E \cdot dr = \int_P^{r_0} E \cdot dr = \int_P^{r_0} \frac{\lambda}{2\pi\epsilon_0 r} dr = \frac{\lambda}{2\pi\epsilon_0} \ln \frac{r_0}{r}$$

$$= -\frac{\lambda}{2\pi\epsilon_0} \ln r + \frac{\lambda}{2\pi\epsilon_0} \ln r_0 = -\frac{\lambda}{2\pi\epsilon_0} \ln r + C \quad (C \text{ 为与电势零点选法有关常数})$$

⑤ 有限长均匀带电直线 电场线与等势线方程.

1) 电场线方程



由前面的推导, AB对P的作用等效于MN (线密度同为 λ)对P的效果.

\therefore P点场强的方向沿 $\angle MPN$ 角平分线方向, 也即电场线的切线方向.

由于P点的任意性, xy平面上任意一点场强方向都沿 $\angle APB$ 的平分线方向.

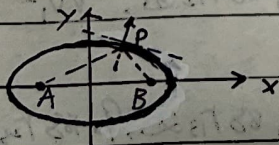
由双曲线的性质 (其上任意一点切线方向与由两焦点到该点连线的夹角平分线方向相同) 可知, 电场线为同焦点的双曲线族, 其方程为

$$\frac{x^2}{a^2} - \frac{y^2}{\frac{1}{4} - a^2} = 1 \quad \text{其中 } 0 < a < \frac{1}{2}.$$

2) 等势线方程

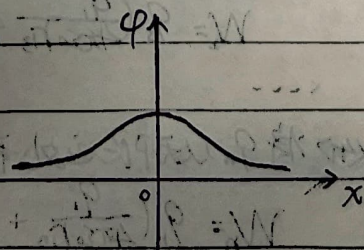
由于电场线方程是双曲线, 而等势线处处与电场线垂直, 故等势线方程

为椭圆: $\frac{x^2}{a^2} + \frac{y^2}{a^2 - \frac{1}{4}} = 1$ 其中 $a > \frac{1}{2}$.



⑦ 带电圆环轴线上电势分布.

$$\varphi = \int \frac{dq}{4\pi\epsilon_0 \sqrt{x^2 + R^2}} = \frac{q}{4\pi\epsilon_0 \sqrt{x^2 + R^2}}$$



⑧ 带电圆板轴线上电势分布.

$$\begin{aligned} \text{利用上面结论 } \varphi &= \int \frac{dq}{4\pi\epsilon_0 \sqrt{x^2 + r^2}} = \int_0^R \frac{2\pi r dr \sigma}{4\pi\epsilon_0 \sqrt{x^2 + r^2}} \\ &= \frac{\sigma}{2\epsilon_0} \int_0^R \frac{r dr}{\sqrt{x^2 + r^2}} = \frac{\sigma}{4\epsilon_0} \int \frac{d(x^2 + r^2)}{\sqrt{x^2 + r^2}} = \frac{\sigma}{2\epsilon_0} (\sqrt{x^2 + R^2} - x) \end{aligned}$$

④无限宽均匀带电平板电势分布

选带电平面本身为电势零点, 故距板上处的电势

$$\varphi = -\int_0^r \frac{\sigma}{\epsilon_0} dr = -\frac{\sigma r}{\epsilon_0}$$

4. 电势能、静电能

①电势能: 由于静电场是保守场, 在静电场中移动电荷时,

静电场力做功与路径无关, 故任一电荷在静电场中都有静电势能

$$W = q\varphi$$

$$A_{12} = W_1 - W_2 = q(\varphi_1 - \varphi_2)$$

一个电荷在外电场中的电势能是属于该电荷与产生电场的电荷系

所共有的, 是一种相互作用能; 同理, 点电荷系对外电场的电势能为

$$W = \sum q_i \varphi_i, \quad \varphi_i \text{ 不包括此电荷系内电荷在该系中其他电荷处产生的电势}$$

②静电能: 1) 互能: 将各电荷从现位置彼此分散到无限远处, 它们之间

静电力所做的功, 即点电荷系的相互作用能

1) 将 q_1 从无限远处移至空间某点, 不做功,

2) 将 q_2 从无限远处移至 q_1 的 r_{12} 处, $W_1 = q_2 \int_{\infty}^{r_{12}} \frac{q_1 dr}{4\pi\epsilon_0 r^2}$

$$= \frac{q_1 q_2}{4\pi\epsilon_0 r_{12}}$$

3) 将 q_3 从无限远处移至 q_1 的 r_{13} 处, q_2 的 r_{23} 处,

$$W_2 = q_3 \left(\frac{q_1}{4\pi\epsilon_0 r_{13}} + \frac{q_2}{4\pi\epsilon_0 r_{23}} \right)$$

...

n) 将 q_n 从无限远处移至 q_1 的 r_{1n} 处, ..., q_{n-1} 的 $r_{(n-1)n}$ 处.

$$W_n = q_n \left(\frac{q_1}{4\pi\epsilon_0 r_{1n}} + \frac{q_2}{4\pi\epsilon_0 r_{2n}} + \dots + \frac{q_{n-1}}{4\pi\epsilon_0 r_{(n-1)n}} \right)$$

$$\therefore E = \sum W_i = \frac{1}{2} \sum q_i \varphi_i$$

2) 自能: 将一带电体分割成无限电荷元, 并分散到彼此的无限远处,

它们之间静电力所做的功.

$$E = \frac{1}{2} \int \varphi dq$$

故空间中的静电能 = 互能 + 自能 = $\frac{1}{2} \int \varphi dq$.

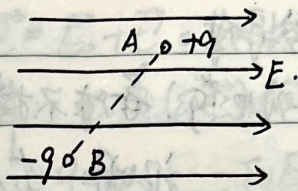
$$= \int w dV = \frac{1}{2} \epsilon_0 \int E^2 dV \quad (w: \text{能量密度}).$$

(3) (1). 电偶极子在外电场(匀强E)中的电势能

$$W = \sum_{i=1}^2 q_i U_i = q\varphi_A + (-q\varphi_B)$$

$$= -qEl \cos\theta$$

$$= -\vec{p} \cdot \vec{E}$$



(2) 平行板电容器静电能:

$$\begin{cases} W = \frac{1}{2} \int \varphi dq = \frac{1}{2} q(U_1 - U_2) = \frac{1}{2} qU \\ W = \frac{1}{2} \epsilon_0 \int E^2 dV = \frac{1}{2} \epsilon_0 E^2 S \cdot d = \frac{1}{2} \epsilon_0 \frac{U^2}{d^2} S \cdot d = \frac{1}{2} CU^2 \\ W = \int q dU = \int \frac{q dq}{C} = \frac{1}{2} \frac{q^2}{C} \end{cases}$$

(3) 实心球

$$\begin{cases} r < R \text{ 时, } W = \frac{1}{2} \epsilon_0 \int_0^R \left(\frac{q}{4\pi\epsilon_0 R^3} r \right)^2 4\pi r^2 dr = \frac{1}{2} \epsilon_0 \left(\frac{q}{4\pi\epsilon_0 R^3} \right)^2 4\pi \int_0^R r^4 dr = \frac{q^2}{40\pi\epsilon_0 R} \\ r > R \text{ 时, } W = \frac{1}{2} \epsilon_0 \int_R^\infty \left(\frac{q}{4\pi\epsilon_0 r^2} \right)^2 4\pi r^2 dr = \frac{1}{2} \epsilon_0 \left(\frac{q}{4\pi\epsilon_0} \right)^2 4\pi \int_R^\infty \frac{dr}{r^2} = \frac{q^2}{8\pi\epsilon_0 R} \\ \therefore W_E = \frac{q^2}{40\pi\epsilon_0 R} + \frac{q^2}{8\pi\epsilon_0 R} = \frac{3q^2}{20\pi\epsilon_0 R} \\ W_E = \frac{1}{2} \int \varphi dq = \frac{1}{2} \int_0^R \frac{R^2 - r^2}{8\pi\epsilon_0 R^3} \cdot \frac{q}{4\pi R^2} 4\pi r^2 dr = \frac{3q^2}{20\pi\epsilon_0 R} \end{cases}$$

(4) 空球壳

$$\begin{cases} r < R \text{ 时, } W = 0 \\ r > R \text{ 时, } W = \frac{1}{2} \epsilon_0 \int_R^\infty \left(\frac{q}{4\pi\epsilon_0 r^2} \right)^2 4\pi r^2 dr = \frac{q^2}{8\pi\epsilon_0 R} \\ \therefore W_E = \frac{q^2}{8\pi\epsilon_0 R} \\ W_E = \frac{1}{2} \int \varphi dq = \frac{1}{2} \cdot \frac{q}{4\pi\epsilon_0 R} \cdot q = \frac{q^2}{8\pi\epsilon_0 R} \end{cases}$$

5. 导体与电介质

①. 静电平衡时的导体:

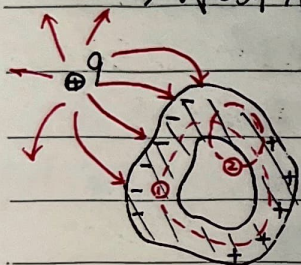
内: $E = E_0(\text{外加}) + E(\text{感应}) = 0$.

外: 导体外部表面场强 $E = \frac{\sigma}{\epsilon_0}$ 垂直于外表面.

导体是等势体, 表面是等势面, 感应电荷分布表面.

带空腔导体:

1) 腔外有电荷, 导体不接地, 内壁无电荷, 腔内无电场.

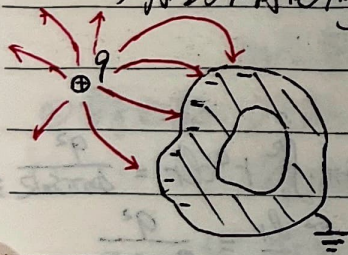


证明: 在导体内部取高斯面①包围空腔, 由于

$$\oint \epsilon_0 \vec{E} \cdot d\vec{S} = 0, \text{ 内壁净电荷为零.}$$

又取一环路②, 根据环路定理, 腔内无电场线, 故内壁无电荷, 腔内无电场.

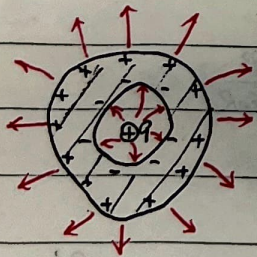
2) 腔外有电荷, 导体接地, 内壁无电荷, 外表面只有一种电荷, 腔内无电场.



证明: 若有正电荷存在于导体外表面(如图), 则其

发出的电场线将伸向无限远(不可能止于导体另一面的负电荷, 因各处电势相等), 而无限远处电势也为零, 与导体与无限远处有电场线相连矛盾.

3) 腔内有电荷, 导体不接地, 内外壁电荷分别为 $-q, +q$, 腔外有电场(如图)

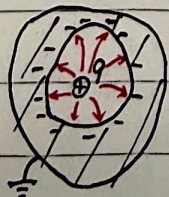


证明: 取一高斯面在导体内部包围空腔, 由于 $\oint \epsilon_0 \vec{E} \cdot d\vec{S} = 0$

内壁电荷为 $-q$ 以抵消空腔内的电荷 $+q$.

又取一高斯面在外部包围导体, 由于电荷守恒, 外表而有 $+q$, 故净电荷为 $+q$, $\oint \epsilon_0 \vec{E} \cdot d\vec{S} = q$, 腔外有电场.

4) 腔内有电荷, 导体接地, 内壁电荷 $-q$, 外壁电荷为 0 , 腔外无电场(如图)



证明: 取一高斯面在导体内部包围空腔, 由于 $\oint \epsilon_0 \vec{E} \cdot d\vec{S} = 0$

内壁有 $-q$ 的电荷; 又由于导体内部, 包括外表面

电势为零, 而无限远处电势也为零, 所以腔外

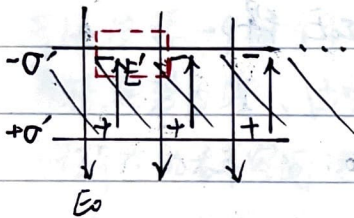
无电场. 综上, 1) 导体中不影响内, 2) 情况内不

影响外, 若内外同时有电荷(导体接地或不接地), 则将各情况叠加.

② 静电平衡下的电介质:

极性分子 \rightarrow 固有电矩 \rightarrow 外电场作用下固有电矩排列较整齐 } 宏观效果:
 非极性分子 \rightarrow 感生电矩 \rightarrow 外电场使感生电荷重心分开 } 产生面极化电荷.

设外加电场为 E_0 , 极化电荷面密度 σ' , 由它感应的场强为 E' , 电介质的相对介电常数为 ϵ_r , 故空间中合场强 $E = E_0 + E'$. 以长方体电介质为例:



由推广的高斯定理: $\epsilon_0 \oint_S (\epsilon_r E) dS = q$, q 为自由电荷.

如图取一高斯面: $\therefore q = 0 \therefore -\epsilon_0 E_0 + \epsilon_0 \epsilon_r (E_0 - E') = 0$

$\therefore E' = \frac{\epsilon_r - 1}{\epsilon_r} E_0$. \therefore 电介质内的合场强

$E = E_0 - E' = \frac{E_0}{\epsilon_r}$. 又由高斯定理:

$$\epsilon_0 (-E_0 \Delta S + E \Delta S) = -\sigma' \Delta S \quad \text{解得: } -\sigma' = -\frac{\epsilon_0 (\epsilon_r - 1)}{\epsilon_r} E_0.$$

综上: 由初始条件 E_0 以及 ϵ_r . 由高斯定理

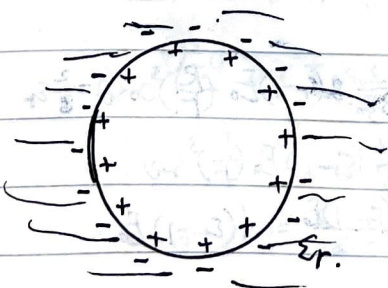
$$\begin{cases} \epsilon_0 \oint_S E dS = q_{\text{自由}} + q_{\text{极化}} \\ \epsilon_0 \oint_S (\epsilon_r E) dS = q_{\text{自由}} \end{cases} \begin{cases} \text{导体一般不是等势体, 表面一般不是} \\ \text{等势面, 极化电荷分布于表面.} \end{cases}$$

可解得

$$E = \frac{E_0}{\epsilon_r}, \quad E' = \frac{\epsilon_r - 1}{\epsilon_r} E_0, \quad \sigma' = \frac{\epsilon_0 (\epsilon_r - 1)}{\epsilon_r} E_0.$$

定义 $\vec{P} = \epsilon_0 (\epsilon_r - 1) \vec{E}$ 为电极化强度, 则 $\sigma' = \frac{\vec{P} \cdot \vec{n}}{\Delta S} = \vec{P} \cdot \vec{n}$.

1). 半径 R , 电量 q 浸在 ϵ_r 的电介质中:



$$\text{由 } \epsilon_0 \oint_S (\epsilon_r E) dS = q \text{ 得}$$

$$\epsilon_0 \epsilon_r E \cdot 4\pi r^2 = q$$

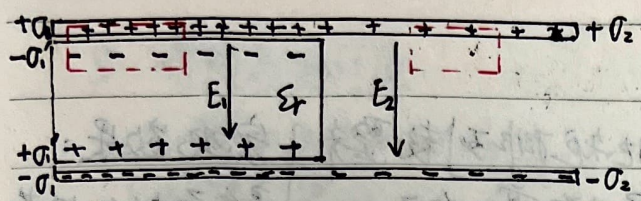
$$\therefore E = \frac{q}{4\pi \epsilon_0 \epsilon_r r^2}.$$

$$\text{由 } \epsilon_0 \oint_S E dS = q + q' \text{ 得}$$

$$q' = \epsilon_0 \cdot \frac{q}{4\pi \epsilon_0 \epsilon_r r^2} \cdot 4\pi r^2 - q = \frac{q}{\epsilon_r} - q = -\frac{\epsilon_r - 1}{\epsilon_r} q.$$

2). 两平行金属板 ($+\sigma_0, -\sigma_0$) 间一半空间充以 ϵ_r 的电介质.

如下页图:



由电荷守恒 $\sigma_1 + \sigma_2 = 2\sigma_0$

由高斯定理:

$$\oint (\sigma_1 \Delta S - \sigma_1' \Delta S) = \epsilon E_1 \Delta S$$

$$\therefore \sigma_1 - \sigma_1' = \epsilon_0 E_1 \quad \langle 2 \rangle \quad \sigma_1 \cdot \Delta S = \epsilon_0 \epsilon_r E_1 \Delta S \quad \therefore \sigma_1 = \epsilon_0 \epsilon_r E_1$$

$$\langle 3 \rangle \quad \sigma_2 \Delta S = \epsilon_0 E_2 \Delta S \quad \therefore \sigma_2 = \epsilon_0 E_2 \quad \because U_1 = U_2 \quad \therefore E_1 = E_2$$

故由 $\sigma_1 + \sigma_2 = 2\sigma_0$, $\sigma_1 - \sigma_1' = \epsilon_0 E_1$, $\sigma_1 = \epsilon_0 \epsilon_r E_1$, $\sigma_2 = \epsilon_0 E_1$ 得

$$\sigma_1 = \frac{2\epsilon_r}{1+\epsilon_r} \sigma_0$$

$$\sigma_2 = \frac{2}{1+\epsilon_r} \sigma_0$$

$$\sigma_1' = \frac{2(\epsilon_r - 1)}{1+\epsilon_r} \sigma_0$$

$$E_1 = E_2 = \frac{2\sigma_0}{\epsilon_0(1+\epsilon_r)} = \frac{2}{1+\epsilon_r} E_0$$

3). 匀强场 E_0 中半径为 R 介电常数为 ϵ_r 的球.

极角 θ 处 $\vec{p} = \epsilon_0 (\epsilon_r - 1) \vec{E}_0$

$$\sigma' = \vec{p} \cdot \vec{s} = p \cos \theta = \epsilon_0 (\epsilon_r - 1) E_0 \cos \theta$$

等效于两个体密度为 p 相距为 d ($d \ll R$) 的球

$$\therefore q_{\Sigma} = \int_{\Sigma} \sigma' R d\omega = \epsilon_0 (\epsilon_r - 1) E_0 R \int_{\Sigma} \cos \theta d\omega$$

$$= 2\epsilon_0 (\epsilon_r - 1) E_0 R = 2\sigma_0 R$$

$$p = \frac{q}{d} = \frac{\epsilon_0 (\epsilon_r - 1) E_0}{d}$$

而两球相距为 d 的球对相当于一对电偶极子.

$$P = q_{\Sigma} d = p \cdot \frac{4}{3} \pi R^3$$

$$\therefore \text{球外电场} \quad \left\{ \begin{aligned} E &= \frac{1}{4\pi\epsilon_0} \frac{2qd \cos \theta}{r^3} = \frac{2}{3} (\epsilon_r - 1) E_0 \left(\frac{R}{r}\right)^3 \cos \theta \\ E_0 &= \frac{1}{4\pi\epsilon_0} \frac{qd \sin \theta}{r^3} = \frac{1}{3} (\epsilon_r - 1) E_0 \left(\frac{R}{r}\right)^3 \sin \theta \end{aligned} \right.$$

$$E_0 = \frac{1}{4\pi\epsilon_0} \frac{qd \sin \theta}{r^3} = \frac{1}{3} (\epsilon_r - 1) E_0 \left(\frac{R}{r}\right)^3 \sin \theta$$

$$\text{球内电场} \quad E = \frac{p}{3\epsilon_0} = \frac{\rho d}{3\epsilon_0} = \frac{\epsilon_0 (\epsilon_r - 1) E_0}{3\epsilon_0} = \frac{1}{3} (\epsilon_r - 1) E_0$$

专题: 电像法

原理：把感应电荷产生的效果用一个或几个点电荷取代。

本质：在原电荷所在空间内，空间场强、电势分布不变。

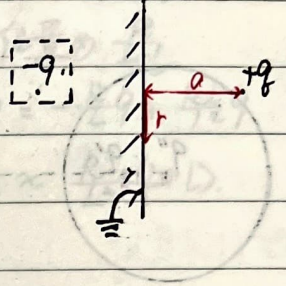
原因：唯一性定理。

1. 无限宽接地平板。

对于平板电势为0，电偶极子中垂直电势也为0。

可以设想 +q 相对平板的像点处有 -q 电荷，保证平板电势为零。由唯一性定理，用 -q 代替接地平板。

+q 所在的右半空间电场不变。



∴ 平板上场强分布 $E = \frac{k \cdot 2aq}{(r^2+a^2)^{3/2}}$ 方向垂直于板

$$\therefore \sigma = \frac{aq}{2\pi(r^2+a^2)^{3/2}}$$

∴ 平板上总电荷 $q' = \int_0^\infty \sigma \cdot 2\pi r dr = -q$ ，故平板左边空间无电场，+q 受到平板上感应电荷的静电力 $F = \frac{kq^2}{(2a)^2}$ ，相当于 -q 对其的力。

2. 接地球壳。

没有正电荷 +q，负电荷 q' ($-q < q$)

存在于空间中，则 $\varphi=0$ 的等势面为一球。

$$\text{证明：} \because U_0=0 \therefore \frac{kq'}{x^2+y^2} + \frac{kq}{\sqrt{(d+l-x)^2+y^2}} = 0$$

$$\therefore q'^2[(d+l-x)^2+y^2] = q^2(x^2+y^2)$$

$$\therefore (q^2-q'^2)x^2 - 2d(d-l)q'^2x + (q^2-q'^2)y^2 = -q'^2(d-l)^2$$

$$\text{配方得 } (q^2-q'^2) \left[x - \frac{(d-l)q'^2}{q^2-q'^2} \right]^2 + (q^2-q'^2)y^2 = \frac{(d-l)^2q^2q'^2}{q^2-q'^2}$$

$$\therefore q' \neq q \therefore \left[x - \frac{(d-l)q'^2}{q^2-q'^2} \right]^2 + y^2 = \frac{q^2q'^2(d-l)^2}{(q^2-q'^2)^2} \quad \text{由对称性可知等势面为球}$$

由图可知，一个导体球壳外有正电荷，这一系统在球外产生的电场可由 -

q' 替代， q' 距球心 $l = \frac{(d-l)q^2}{q^2-q'^2}$ ，球半径 $R = \frac{2q'(d-l)}{q^2-q'^2}$

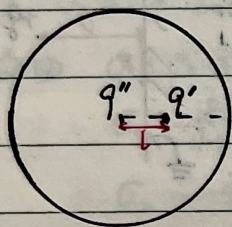
$$\text{解得：} \quad q' = -\frac{q}{2}, \quad l = \frac{R}{2}$$

又 \because 0点 $\varphi=0$, $\therefore \frac{kq}{a} + \frac{kq''}{R} = 0 \therefore q'' = -\frac{R}{a}q = q'$

即球面上感应出的总电荷等于导体球电量.

讨论: ①若开始时球壳不接地也不带电荷, 在球壳外加 $-+q$.

1) 为使球是等势体, 在 $l = \frac{R^2}{a}$ 处加 $q' = -\frac{R}{a}q$, 使球壳电势为零.



2) 由于加了 $+q$, 球壳电势并不为零, 为保证球壳为等势体, 且净电荷为零, 应在球壳表面均匀覆盖一层 $q'' = -q' = \frac{R}{a}q$, 而均匀覆于表面的 q'' 又等效于在球心处.

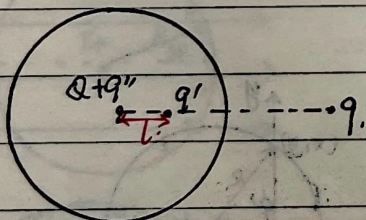
综上, $q' = -\frac{R}{a}q$, $x = \frac{R^2}{a}$; $q'' = \frac{R}{a}q$, $x = 0$.

②若开始时球壳不接地, 且带电量为 Q ($\frac{kQ}{R} = U_0$), 球壳外加 $-+q$.

同理, 在 $l = \frac{R^2}{a}$ 处加 $q' = -\frac{R}{a}q$ 使 $\varphi = 0$

在球心处加 $q'' = \frac{R}{a}q$ 使 $Q = 0$, $\varphi = \frac{kq''}{R}$.

在球心处加 $q''' = Q$, 使 $Q = Q_0$, $\varphi = \frac{k(Q+q''')}{R}$



3. 无限长接地导体圆柱. (圆柱外 d 处有线密度 λ 的直线)

λ 在P点的电势 $\varphi_P = \frac{\lambda}{2\pi\epsilon_0} \ln \frac{d+R}{d-R}$. (以Q点为电势零点)

λ' 在P点的电势 $\varphi'_P = \frac{\lambda'}{2\pi\epsilon_0} \ln \frac{R+l}{R-l}$.

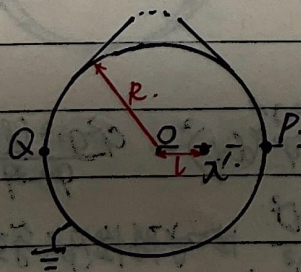
$$\therefore \frac{\lambda}{2\pi\epsilon_0} \ln \frac{d+R}{d-R} + \frac{\lambda'}{2\pi\epsilon_0} \ln \frac{R+l}{R-l} = 0 \quad (1)$$

λ 在Q点的电势 $\varphi_Q = \frac{\lambda}{2\pi\epsilon_0} \ln \frac{d+R}{d-R}$ (以P点为电势零点)

λ' 在Q点的电势 $\varphi'_Q = \frac{\lambda'}{2\pi\epsilon_0} \ln \frac{R+l}{R-l}$.

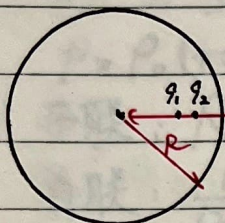
$$\therefore \frac{\lambda}{2\pi\epsilon_0} \ln \frac{d+R}{d-R} + \frac{\lambda'}{2\pi\epsilon_0} \ln \frac{R+l}{R-l} = 0 \quad (2)$$

由(1)(2)两式解得 $\lambda' = -\lambda$, $l = \frac{R^2}{d}$.



4. 电偶极子在不接地导体前 d 处.

电矩 $P = q \cdot 2l$



由图: $+q$ 坐标 $L+l$; $-q$ 坐标 $L-l$.
 $+q$ 像电荷 $q_1 = -\frac{R}{L-l}q$, 位置为 $\frac{R^2}{L-l}$.
 $-q$ 像电荷 $q_2 = +\frac{R}{L+l}q$, 位置为 $\frac{R^2}{L+l}$.

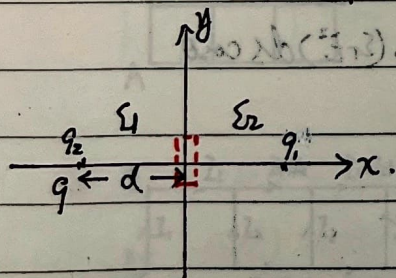
$\because L \gg l, \therefore q_1 \approx -\frac{R}{L}(L-l)q = -\frac{R}{L}q + \frac{R}{L}lq$.
 $x_1 \approx \frac{R^2}{L}(L-l) = \frac{R^2}{L}L - \frac{R^2}{L}l$; $q_2 \approx +\frac{R}{L}(L+l)q = \frac{R}{L}q + \frac{R}{L}lq, x_2 \approx \frac{R^2}{L}(L+l)$.

$\therefore P' \approx \frac{R}{L}q \cdot \frac{2R^2}{L}l = \frac{R^3}{L^3}P$.

且在 q_1, q_2 中点处 ($\frac{R^2}{L}$) 还有一个像点电荷: $q' = q_1 + q_2 = \frac{R}{L}lq$.

像上, 所有像电荷 $\left\{ \begin{array}{l} q_1 = -\frac{R}{L}q + \frac{R}{L}lq, x_1 = \frac{R^2}{L} - \frac{R^2}{L}l \\ q_2 = \frac{R}{L}q + \frac{R}{L}lq, x_2 = \frac{R^2}{L} + \frac{R^2}{L}l \\ q' = \frac{R}{L}lq, x' = \frac{R^2}{L} \end{array} \right\} P' \approx \frac{R^3}{L^3}P$.

5. 点电荷对无限大介电平面的镜像.



① 在介质平面处 $U_{左} = U_{右}$.

② 在原点附近作一高斯面, 由高斯定理

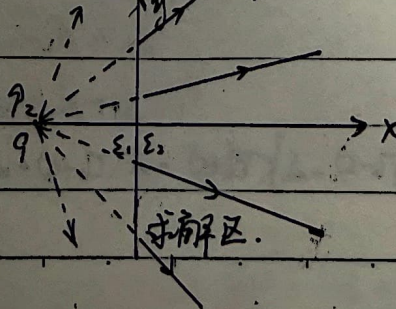
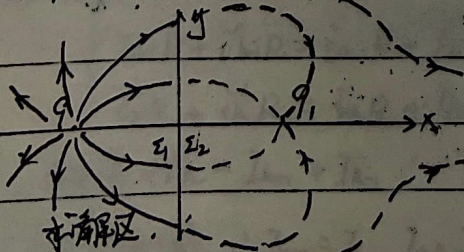
$\oint \epsilon_r E \cdot ds = \sum q_{\text{内}} = 0 \Rightarrow \epsilon_1 E = \epsilon_2 E_2$

设 $x = \pm d$ 处各有一像电荷, 分别是 q_1, q_2 .

由①②条件, 在原点处有 $\frac{q+q_1}{4\pi\epsilon_1 d} = \frac{q+q_2}{4\pi\epsilon_2 d}, \epsilon_1 \frac{q-q_1}{4\pi\epsilon_1 d^2} = \epsilon_2 \frac{q+q_2}{4\pi\epsilon_2 d^2}$

由上两式解得 $q_1 = \frac{\epsilon_1 - \epsilon_2}{\epsilon_1 + \epsilon_2} q, q_2 = -\frac{\epsilon_1 - \epsilon_2}{\epsilon_1 + \epsilon_2} q$

由 q 和 q_1 确定 ϵ_1 空间中的电场. 由 q 和 q_2 确定 ϵ_2 空间中的电场.



专题：静电场中的虚功原理

1. 平行板电容器正负板所受静电力

① Q 不变时:

$$W = \frac{1}{2} \epsilon_0 E^2 \cdot Sd$$

$$= \frac{1}{2} \epsilon_0 \left(\frac{Q}{\epsilon_0 d} \right)^2 Sd$$

$$= \frac{1}{2} \frac{Q^2 d}{\epsilon_0 S}$$

$$\therefore F = -\frac{\partial W}{\partial d} = -\frac{Q^2}{2\epsilon_0 S} = -\frac{\sigma^2 S}{2\epsilon_0} = -\frac{1}{2} \epsilon_0 E^2 \cdot S \quad \text{负号表示吸引力.}$$

② U 不变时:

$$W = \frac{1}{2} \epsilon_0 \left(\frac{U}{d} \right)^2 Sd$$

$$= \frac{1}{2} \frac{\epsilon_0 U^2 S}{d}$$

$$\therefore F = \frac{\partial W}{\partial d} = -\frac{\epsilon_0 U^2 S}{2d^2} = -\frac{1}{2} \epsilon_0 E^2 \cdot S \quad \text{负号表示吸引力.}$$

综上, $|F| = \frac{1}{2} \epsilon_0 E^2 S$, 可推广到任何带电体. $\frac{dF}{dS} = -\frac{1}{2} \epsilon_0 E^2 = -w_e$

$$F = \int_S p ds = \frac{1}{2} \epsilon_0 \int_S \sigma^2 ds, \quad \text{且 } W = \int_V \frac{1}{2} \epsilon_0 \epsilon_r E^2 dV$$

$$F = \int_S \frac{1}{2} \epsilon_0 (\epsilon_r E^2) ds \cos \theta$$

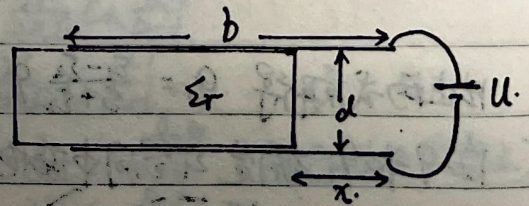
2. 带电导体球上下半球的相互作用力

$$F = \frac{1}{2} \epsilon_0 \int_S \sigma^2 ds \cos \theta = \frac{\sigma^2}{2\epsilon_0} \cdot \pi R^2$$

3. 平行金属板中拉电介质块的力

$$W = \frac{1}{2} \left(\epsilon_0 \epsilon_r \frac{(b-x)l}{d} + \epsilon_0 \frac{x l}{d} \right) U^2$$

$$\therefore F = \frac{\partial W}{\partial x} = \frac{\epsilon_0 (\epsilon_r - 1) l U^2}{2d}$$



九. 电阻 电容 电感

1. 电阻

① $R = \int \rho \frac{dl}{S}$

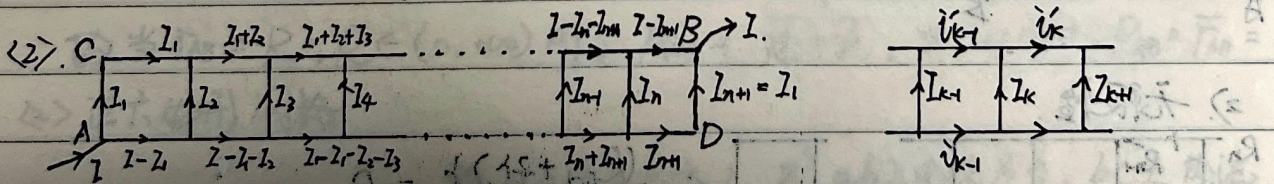
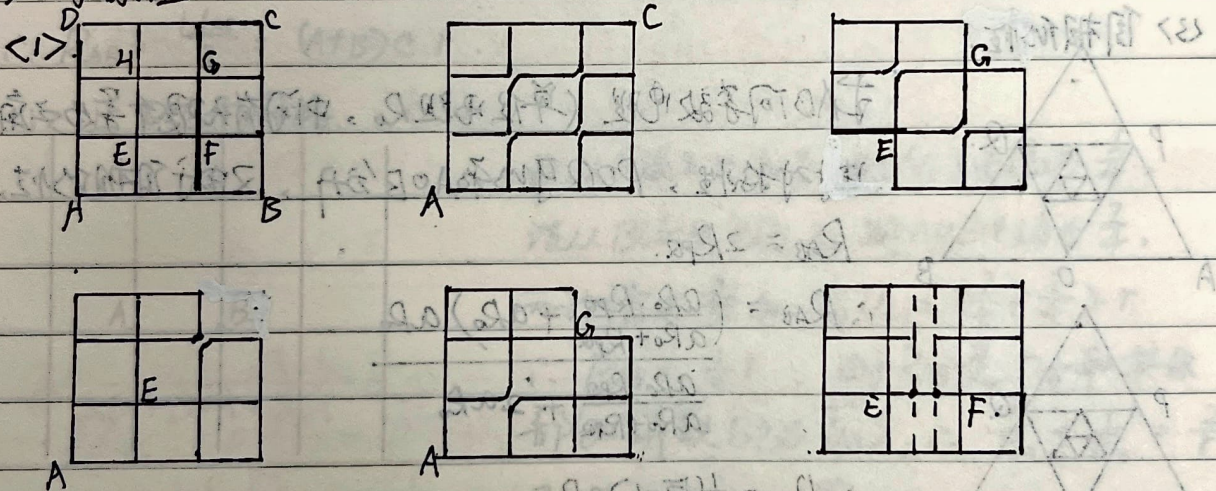
$\rho = \rho_0(1 + \alpha t)$, $d\rho = \alpha \rho_0 dt$, $\therefore R = R_0(1 + \alpha t)$

② 串联: $R_{\Sigma} = \rho \frac{\sum l_i}{S} = \sum \rho \frac{l_i}{S} = \sum R_i$; $R_{\Sigma} = \frac{U_{\Sigma}}{I} = \sum \frac{U_i}{I} = \sum R_i$

并联: $\frac{1}{R_{\Sigma}} = \frac{\sum I_i}{U} = \sum \frac{I_i}{U} = \sum \frac{1}{R_i}$; $\frac{1}{R_{\Sigma}} = \frac{I_{\Sigma}}{U} = \sum \frac{I_i}{U} = \sum \frac{1}{R_i}$

③ 等效电阻

1) 对称性



$$U_{CB} = U_{AD} = [G_1 + (G_1 + G_2) + (G_1 + G_2 + G_3) + \dots + (G_1 + G_2 + \dots + G_n)] R$$

$$= [(G_1 - G_1) + (G_1 - G_1 - G_2) + (G_1 - G_1 - G_2 - G_3) + \dots + G_{n+1}] R$$

$\therefore 2U_{CB} = nIR$

又: $\begin{cases} I_{k-1}R + U_{k-1}R = I_{k-1}R + I_k R \\ I_k R + U_k R = I_k R + I_{k+1} R \end{cases} \Rightarrow \begin{cases} U_{k-1} + I_k = U_k \\ U_{k-1} = I_k + U_k \end{cases}$

解得 $4I_k = I_{k+1} + I_{k-1}$ 变为 $I_{n-1} = (2-\sqrt{3})I_n = (2+\sqrt{3})[I_n - (2-\sqrt{3})I_n]$

∵ 对称性 $\therefore I_{n-1} = I_1, I_n = I_2$

$$\therefore I_2 = \frac{(2+\sqrt{3})^{n-2} - (2-\sqrt{3})^{n-2}}{(2+\sqrt{3})^{n-1} - (2-\sqrt{3})^{n-1} + (2-\sqrt{3}) - (2+\sqrt{3})} I_1$$

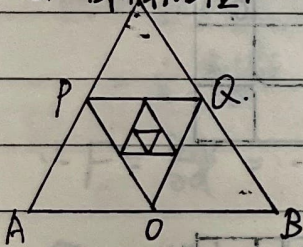
又: 在第一中: $2I_1 R = (I_2 - I_1) R \Rightarrow I_2 = 3I_1 - I_1$

由上式得 $I_1 = \left[3 - \frac{(2+\sqrt{3})^{n-2} - (2-\sqrt{3})^{n-2}}{(2+\sqrt{3})^{n-1} - (2-\sqrt{3})^{n-1} - 2\sqrt{3}} \right]^{-1} I$

$\therefore U_{AB} = I_1 R + U_{BC}$

$$R_{AB} = \frac{U_{AB}}{I} = \left\{ \frac{R}{2} + \left[3 - \frac{(2+\sqrt{3})^{n-2} - (2-\sqrt{3})^{n-2}}{(2+\sqrt{3})^{n-1} - (2-\sqrt{3})^{n-1} - 2\sqrt{3}} \right]^{-1} \right\} R$$

(3) 自相似性.

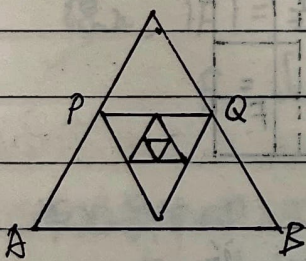


\rightarrow AB 间等效电阻 (单位电阻 R_0 , 中间有无限个等边三角形)

由于对称性, POQ 可以拆成 AOB 部分, 又由于自相似性,

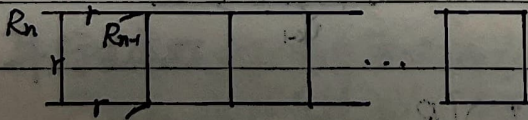
$$R_{AB} = 2R_{POQ}$$

$$\therefore R_{AB} = \frac{(aR_0 \cdot R_{POQ} + aR_0) aR_0}{aR_0 + R_{POQ}} = \frac{aR_0 \cdot R_{POQ}}{aR_0 + R_{POQ}} + 2aR_0$$



$$\therefore R_{AB} = \frac{1}{3}(\sqrt{7}-1)aR_0$$

(2) 无限性.



$$\frac{(R_{n+1} + 2R_n) r}{R_{n+1} + 3r} = R_n$$

$$\frac{(2-\sqrt{3})r [R_{n+1} + (1-\sqrt{3})r]}{R_{n+1} + 3r} = R_n + (1-\sqrt{3})r$$

$$\therefore \frac{1}{(2-\sqrt{3})r} + \frac{(2+\sqrt{3})r}{(2-\sqrt{3})r [R_{n+1} + (1-\sqrt{3})r]} = \frac{1}{R_n + (1-\sqrt{3})r}$$

$$\frac{1}{R_n + (1-\sqrt{3})r} + \frac{1}{2\sqrt{3}r} = 7 + 4\sqrt{3}$$

$$\frac{1}{R_{n+1} + (1-\sqrt{3})r} + \frac{1}{2\sqrt{3}r}$$

$$\text{解得 } R_n = -\frac{1}{2\sqrt{3}r} + \left[\frac{1}{R_n + (4\sqrt{3})r} + \frac{1}{2\sqrt{3}r} \right]^{n-1} + (\sqrt{3}-1)r.$$

当 $n \rightarrow \infty$ 时

$$R_n = (\sqrt{3}-1)r.$$

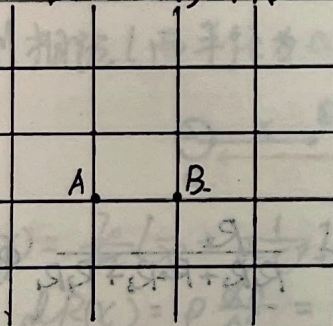
3) 电流叠加法.

设流入电流为 I , 算出所有支路 AB 中流过的电流 I_{AB} ; 设另一点流出的电流为 I , 算出 AB 中电流 I'_{AB} , 若 r_{AB} 是连接 AB 两点的导线的电阻且 $r_{AB} = Cr$,

$$\text{且 } I_{AB} = AI, I'_{AB} = BI. \quad \therefore U_{AB} = (I_{AB} + I'_{AB})r_{AB} = (A+B)C \cdot r \cdot I$$

$$\therefore R_{AB} = \frac{U_{AB}}{I} = (A+B)C \cdot r.$$

(1) 正四边(形)网格.



设从 A 流入电流 I , 则 AB 上电流为 $\frac{1}{4}I$,

设从 B 流出电流 I , 则 AB 上电流为 $\frac{1}{4}I$,

两种情况叠加, 有 $U_{AB} = (\frac{1}{4} + \frac{1}{4})r \cdot I$

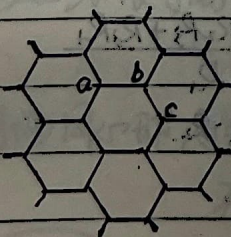
$\therefore R_{AB} = \frac{1}{2}r$, 由于 R_{AB} 是 r_{AB} 和其余

部分的并联(记为 \bar{r}_{AB}), $\therefore \frac{1}{R_{AB}} + \frac{1}{\bar{r}_{AB}} = \frac{2}{r}$

而 $r_{AB} = r$, $\therefore \bar{r}_{AB} = r$.

故当 $r_{AB} = R, R \in (0, +\infty)$ 时, $R_{AB} = \frac{r}{R+r}$; 当 $r_{AB} = 0$ 时, $R_{AB} = \bar{r}_{AB} = r$.

(2) 正六边(形)网格.



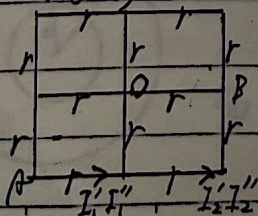
设从 a 流入电流 I , 则 ab 上电流为 $\frac{2}{3}I$, bc 上电流

为 $\frac{1}{3}I$; 设从 c 流出电流 I , 则 bc 上电流为 $\frac{2}{3}I$,

ab 上电流为 $\frac{1}{3}I$. 两种情况叠加, 有

$$U_{ac} = (\frac{2}{3} + \frac{2}{3})r \cdot I = 2r \cdot I, \quad \therefore R_{ac} = r$$

(3) 田字形 (求 AB 等效电阻)



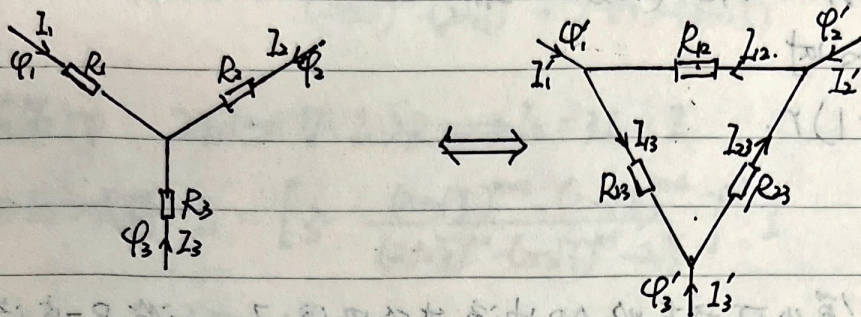
设从 A 流入从 O 流出, 解得 $I_1 = \frac{7}{2}I, I_2 = \frac{7}{8}I$.

设从 O 流入从 B 流出, 解得 $I_1' = \frac{7}{24}I, I_2' = \frac{5I}{24}$.

$$\therefore I_1 = \frac{7}{2}I + \frac{7}{24}I = \frac{13}{24}I; \quad I_2 = \frac{7}{8}I + \frac{5I}{24} = \frac{1}{3}I$$

$$\therefore U_{AB} = I_1 r + I_2 \cdot 2r; \quad \therefore R_{AB} = \frac{U_{AB}}{I} = (\frac{13}{24} + \frac{2}{3})r = \frac{29}{24}r$$

4) Y-Δ变换



等效本质:
$$\begin{cases} I_1 = I_1', I_2 = I_2', I_3 = I_3' \\ \varphi_1 = \varphi_1', \varphi_2 = \varphi_2', \varphi_3 = \varphi_3' \end{cases}$$

Y形中有
$$\begin{cases} \varphi_1 - I_1 R_1 + I_3 R_3 = \varphi_3; \varphi_1 - I_1 R_1 + I_2 R_2 = \varphi_2 \\ I_1 + I_2 + I_3 = 0 \end{cases}$$
 (节点电压法)

(基尔霍夫电流定律)

Δ形中有
$$\begin{cases} \varphi_1' - I_3' R_{31} = \varphi_3'; \varphi_1' + I_2' R_{12} = \varphi_2' \\ I_1' = I_3' - I_2' \end{cases}$$

$\therefore I_1 = I_1', \varphi_1 = \varphi_1', \varphi_2 = \varphi_2', \varphi_3 = \varphi_3'$

而
$$I_1 = \frac{R_2 + R_3}{R_1 R_2 + R_2 R_3 + R_3 R_1} \varphi_1 = \frac{R_3}{R_1 R_2 + R_2 R_3 + R_3 R_1} \varphi_2 - \frac{R_2}{R_1 R_2 + R_2 R_3 + R_3 R_1} \varphi_3$$

$$I_1' = \left(\frac{1}{R_{31}} + \frac{1}{R_{12}}\right) \varphi_1' - \frac{1}{R_{12}} \varphi_2' - \frac{1}{R_{31}} \varphi_3'$$

$$\frac{R_2 + R_3}{R_1 R_2 + R_2 R_3 + R_3 R_1} = \frac{1}{R_{31}} + \frac{1}{R_{12}} \quad \text{解得 } R_{12} = \frac{R_1 R_2 + R_2 R_3 + R_3 R_1}{R_3}$$

$$\frac{R_3}{R_1 R_2 + R_2 R_3 + R_3 R_1} = \frac{1}{R_{12}} \quad R_{31} = \frac{R_1 R_2 + R_2 R_3 + R_3 R_1}{R_2}$$

$$\frac{R_1}{R_1 R_2 + R_2 R_3 + R_3 R_1} = \frac{1}{R_{31}} \quad \text{对称性 } R_{23} = \frac{R_1 R_2 + R_2 R_3 + R_3 R_1}{R_1}$$

$\therefore \frac{R_{12}}{R_{31}} = \frac{R_2}{R_3} \Rightarrow R_3 = \frac{R_{31}}{R_2} R_2, \quad \frac{R_{31}}{R_{23}} = \frac{R_1}{R_2} \Rightarrow R_1 = \frac{R_{31}}{R_{23}} R_2$

$\therefore R_{31} = \frac{R_{31}}{R_{23}} R_2 + \frac{R_{31}}{R_{12}} R_2 + \frac{R_{31}}{R_2} R_2$

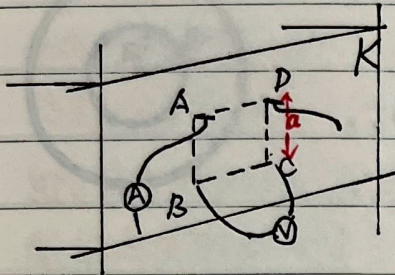
解得
$$R_2 = \frac{R_{23} R_{31}}{R_{12} + R_{23} + R_{31}}$$

对称性
$$R_3 = \frac{R_{31} R_{12}}{R_{12} + R_{23} + R_{31}}$$

$$R_1 = \frac{R_{12} R_{23}}{R_{12} + R_{23} + R_{31}}$$

专题：测电阻率。

1. 测无限大物质电阻率。



在K上划出一正方形ABCD.

在A处注入电流，D处输出同样强度的电流(I_0).

对注入A的电流，有 $j = \frac{I_0}{2\pi r}$ ， $\therefore E = \frac{j}{\sigma} = \frac{I_0 \rho}{2\pi r}$.

$$\therefore \varphi = -\int E dr = -\frac{I_0 \rho}{2\pi r}$$

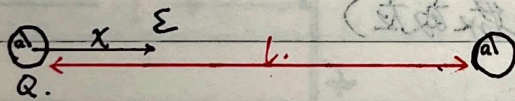
$$\therefore U_{BC} = \frac{I_0 \rho}{2\pi a} - \frac{I_0 \rho}{2\sqrt{2}\pi a} = \frac{(2-\sqrt{2})I_0 \rho}{4\pi a}$$

同样，只考虑D输出的电流时， $U'_{BC} = \frac{(2-\sqrt{2})I_0 \rho}{4\pi a}$ ，利用电流叠加原理。

$$U_0 = U_{BC} + U'_{BC} = \frac{(2-\sqrt{2})I_0 \rho}{2\pi a} = U_0 \rho \quad \Rightarrow \rho = \frac{U_0}{(2-\sqrt{2})I_0}$$

$$\therefore \rho = (2+\sqrt{2})\pi a \frac{U_0}{I_0}$$

2. 测相距 l 两半径为 a ($l \gg a$) 金属棒所在空间电阻率 (万用表测得两棒间 R)



$$j(x) = \frac{I_0}{4\pi} \left[\frac{1}{x^2} + \frac{1}{(l-x)^2} \right] \quad (a < x < l-a)$$

$$\therefore dR(x) = \rho \frac{dx}{\Delta l} = \rho \frac{dx}{\Delta l} j(x) = \frac{dx}{\Delta l} \cdot \frac{I_0 \rho}{4\pi} \left[\frac{1}{x^2} + \frac{1}{(l-x)^2} \right]$$

$$\therefore R = \frac{I_0 \rho}{4\pi \Delta l} \int_a^{l-a} \left[\frac{1}{x^2} + \frac{1}{(l-x)^2} \right] dx = \frac{I_0 \rho}{4\pi \Delta l} \cdot 2 \left(\frac{1}{a} - \frac{1}{l-a} \right) = \frac{I_0 \rho}{2\pi \Delta l} \left(\frac{1}{a} - \frac{1}{l-a} \right)$$

$$\therefore \text{并联的 } \frac{l}{\Delta l} \text{ 根导线的总电阻为 } \frac{R}{I_0 \Delta l} = \frac{\rho}{2\pi} \left(\frac{1}{a} - \frac{1}{l-a} \right) = R_0$$

$$\text{通过万用表可测得 } R_0, \therefore \rho = \frac{2\pi R_0 a (l-a)}{l-2a} \quad \text{当 } l \rightarrow \infty \text{ 时 } \rho = 2\pi R_0 a$$

3. 测两同心球间物质的电阻率。

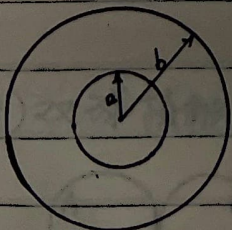
在两球面间取一半径为 r 的高斯面。有

$$\oint E dS = E \cdot 4\pi r^2 = \frac{Q}{\epsilon} = \rho \oint \vec{j} dS = \rho I$$

$$\therefore Q = \epsilon \rho I$$

$$\text{而 } U_{ab} = \frac{Q}{4\pi \epsilon} \left(\frac{1}{a} - \frac{1}{b} \right) = IR \quad \therefore \frac{Q}{\epsilon I} = \frac{4\pi R \cdot ab}{b-a}$$

$$\therefore \rho = \frac{4\pi R ab}{b-a}$$



2. 电容

① $C = \frac{Q}{U}$

U : 两极间电势差
 Q : 用导线将两极相连后通过导线的电量

② 串联: $\frac{1}{C_{总}} = \frac{1}{Q} = \sum \frac{1}{Q_i} = \sum \frac{1}{C_i}$

并联: $C_{总} = \frac{Q_{总}}{U} = \sum \frac{Q_i}{U} = \sum C_i$

③ 电容器的能量:

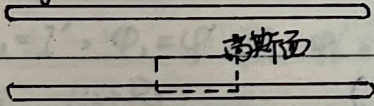
$$W = \int q du = \int_0^Q \frac{dq}{C} = \frac{1}{2} \frac{Q^2}{C} = \frac{1}{2} \frac{Q^2}{\epsilon S} \cdot d = \frac{1}{2} \left(\frac{Q}{\epsilon S} \right)^2 \epsilon \cdot Sd$$

$$= \frac{1}{2} E^2 \epsilon Sd = \frac{1}{2} \epsilon E^2 \cdot V$$

能量密度 $w = \frac{dW}{dV} = \frac{1}{2} \epsilon E^2$

④ 典型电容器电容

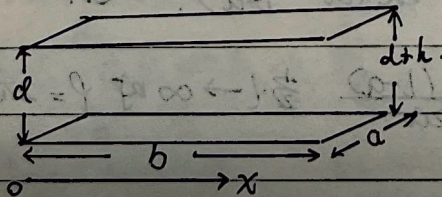
1) 平行板电容器 (忽略边缘效应)



$E_{总} = \frac{\sigma_{总}}{\epsilon_0} \Rightarrow \therefore E = \frac{\sigma}{\epsilon_0} = \frac{1}{\epsilon_0} \frac{q}{S}$

$\therefore C = \frac{q}{U} = \frac{\epsilon_0 S}{d}$

2) 平行板倾斜电容器 ($h \ll d$)

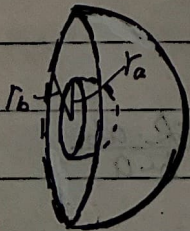


将整个电容器看成无数 dc 并联而成

$dc = \frac{\epsilon_0 \cdot a dx}{d + \frac{h}{b} x}$

$\therefore C = \int_0^b \frac{\epsilon_0 a dx}{d + \frac{h}{b} x} = \frac{\epsilon_0 a d}{h} \ln \left(1 + \frac{h}{d} \right)$

3) 球形电容器

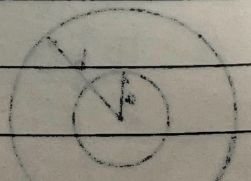


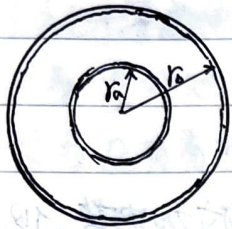
$Q_A = \frac{1}{4\pi\epsilon_0} \left(\frac{q}{r_a} + \frac{-q}{r_b} \right)$

$Q_B = \frac{1}{4\pi\epsilon_0} \left(\frac{q}{r_a} + \frac{q}{r_b} \right)$

$\therefore U_{AB} = Q_A - Q_B = \frac{q}{4\pi\epsilon_0} \left(\frac{1}{r_a} - \frac{1}{r_b} \right)$

$\therefore C = \frac{q}{U_{AB}} = \frac{4\pi\epsilon_0 r_a r_b}{r_b - r_a}$



4) 圆柱形电容器 (长为 l)

在两圆柱中间取一圆柱体高斯面, 半径为 r , 有

$$E \cdot 2\pi r \cdot l = \frac{q}{\epsilon_0} \quad \therefore E = \frac{q}{2\pi\epsilon_0 r l}$$

$$\therefore U_{ab} = \int_a^b E dr = \frac{q}{2\pi\epsilon_0 l} \int_a^b \frac{dr}{r} = \frac{q}{2\pi\epsilon_0 l} \ln \frac{r_b}{r_a}$$

$$\therefore C = \frac{q}{U_{ab}} = \frac{2\pi\epsilon_0 l}{\ln \frac{r_b}{r_a}}, \quad \text{当 } r_b - r_a \ll r_a, r_b \text{ 时}$$

$$C \approx \frac{2\pi\epsilon_0 r_a l}{r_b - r_a}$$

5) 孤立导体球: 将无限远处看成另一极板.

$$\therefore \varphi_\infty = 0, \quad \varphi_R = \frac{q}{4\pi\epsilon_0 R}$$

$$\therefore U = \frac{q}{4\pi\epsilon_0 R} \quad \therefore C = \frac{q}{U} = 4\pi\epsilon_0 R$$

6) 球板电容器 (半径 r , 相距 l , $l \gg r$)

在金属板右边作出金属球的像, 撤去金属板, 在此双球系统中

$$U_{ab} = \frac{kq}{r} - (-\frac{kq}{l}) = \frac{q}{2\pi\epsilon_0 r}$$

$$\therefore C = \frac{q}{U_{ab}} = 2\pi\epsilon_0 r$$

此双球系统恰相当于两个球板电容器串联, 故球板电容器电容

$$C' = 4\pi\epsilon_0 r$$

7) 双球相连电容器 (半径 r_a, r_b , 相距 l , $l \gg r_a, r_b$)

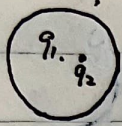
$$\therefore \text{两球用导线相连, } \therefore \varphi_a = \varphi_b \Rightarrow \frac{kq_a}{r_a} = \frac{kq_b}{r_b}$$

$$\text{以无限远处为另一极, } \varphi_\infty = 0 \quad \therefore U = \varphi_a - \varphi_\infty = \frac{kq_a}{r_a}$$

$$\therefore C = \frac{q_1 + q_2}{U} = \frac{q_1 + \frac{r_b}{r_a} q_1}{\frac{kq_1}{r_a}} = 4\pi\epsilon_0 (r_a + r_b)$$

8) 双球接触电容器 (半径 R , 相距 $2R$)

设系统电势为 U_0 . 设想两球电荷集中在球心, 不计相互感应时, 两球电势均为 U_0 , 且 $q_1 = 4\pi\epsilon_0 R U_0$.



q_1

由于相互感应在会使两球电势比 U_0 偏大, 为消除附加电势需在各球内加一个像电荷

$$q_2 = -\frac{R}{2R} q_1 = -\frac{1}{2} q_1$$

$$\text{距各球心距离 } x_2 = \frac{R^2}{2R} = \frac{1}{2} R$$

这样, 各自内部的像电荷可消除对方的附加电势, 但又使自己产生新的附加电势, 需要新的像电荷去抵消.



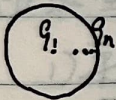
q_1

$$q_3 = -\frac{R}{2R-x_2} q_2 = \frac{1}{3} q_1$$

$$x_3 = \frac{R^2}{2R-x_2} = \frac{2}{3} R$$

以此类推, 每次新加的像电荷能抵消上次产生的附加电势, 而又产生新的附加电势, 又因为 $|q_{n+1}| < |q_n|$,

所以每次产生的新的附加电势比上次少, 当像电荷趋于无穷多时, 能完全修正所产生的递减的附加电势, 使系统电势为 U_0 .



q_1

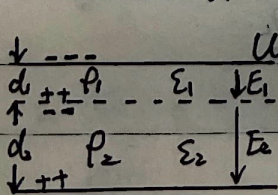
$$\text{即 } \begin{cases} q_n = \left(\frac{-1}{n}\right)^{n-1} q_1 \\ x_n = \frac{n-1}{n} R \end{cases}$$

又由导体球上的总电量就等于 q_1 和像电荷的总电量,

$$Q_{\text{总}} = 2(q_1 + q_2 + \dots) = 2q_1 \left(1 - \frac{1}{2} + \frac{1}{3} - \frac{1}{4} + \dots\right) = 8\pi\epsilon_0 R U_0 \ln 2$$

$$\therefore C = \frac{Q_{\text{总}}}{U_0} = 8\pi\epsilon_0 R \ln 2$$

9) 漏电电容器



由于两极间加了电压 U , $I = \frac{U}{\rho_1 \frac{d_1}{\epsilon_1} + \rho_2 \frac{d_2}{\epsilon_2}} = \frac{U \epsilon_1 \epsilon_2}{\rho_1 d_1 + \rho_2 d_2}$

$$\therefore E_1 = \rho_1 \frac{I}{\epsilon_1} = \frac{\rho_1 U}{\rho_1 d_1 + \rho_2 d_2}, E_2 = \rho_2 \frac{I}{\epsilon_2} = \frac{\rho_2 U}{\rho_1 d_1 + \rho_2 d_2}$$

$$\text{又 } C_1 = \frac{\epsilon_0 \epsilon_1 S}{d_1}, C_2 = \frac{\epsilon_0 \epsilon_2 S}{d_2}$$

$$\therefore q_1 = \epsilon_1 d_1 C_1 = \frac{\rho_1 \epsilon_0 \epsilon_1 S U}{\rho_1 d_1 + \rho_2 d_2}, q_2 = \epsilon_2 d_2 C_2 = \frac{\rho_2 \epsilon_0 \epsilon_2 S U}{\rho_1 d_1 + \rho_2 d_2}$$

\therefore 两个介质交界面上自由电荷面密度

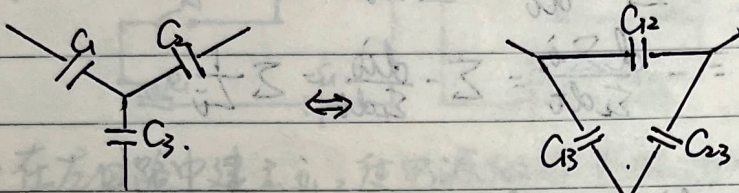
$$\sigma = \frac{\epsilon_0 (\rho_1 \epsilon_1 - \rho_2 \epsilon_2) U}{\rho_1 d_1 + \rho_2 d_2}$$

⑤ 等效电容

类似于等效电阻，有对称性、无限性等解法。又由于二端无源电路中，

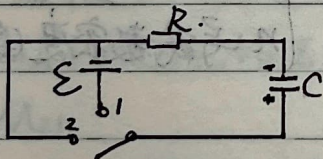
R 与 C 的地位相同，（串联： $R = \sum R_i$, $C = (\sum \frac{1}{C_i})^{-1}$ ；并联： $R = (\sum \frac{1}{R_i})^{-1}$, $C = \sum C_i$ ）

故与 R 有着相反的 $Y-\Delta$ 变换。



$$\begin{cases} C_{12} = \frac{C_1 C_2}{C_1 + C_2 + C_3} \\ C_{23} = \frac{C_2 C_3}{C_1 + C_2 + C_3} \\ C_{31} = \frac{C_3 C_1}{C_1 + C_2 + C_3} \end{cases} \quad \begin{cases} C_3 = \frac{C_{12} C_{23} + C_{12} C_{31} + C_{23} C_{31}}{C_{12}} \\ C_1 = \frac{C_{12} C_{23} + C_{12} C_{31} + C_{23} C_{31}}{C_{23}} \\ C_2 = \frac{C_{12} C_{23} + C_{12} C_{31} + C_{23} C_{31}}{C_{31}} \end{cases}$$

⑥ RC电路



1) 充电: $\mathcal{E} - iR - \frac{q}{C} = 0$, $i = \frac{dq}{dt}$

$$\therefore \mathcal{E} = R \frac{dq}{dt} + \frac{q}{C} \Rightarrow dt = \frac{RC dq}{\mathcal{E}C - q}$$

$$\therefore \int_0^t dt = -RC \int_0^q \frac{d(\mathcal{E}C - q)}{\mathcal{E}C - q} \Rightarrow t = -RC \ln \frac{\mathcal{E}C - q}{\mathcal{E}C}$$

解得 $q = C\mathcal{E}(1 - e^{-\frac{t}{RC}})$, $i = \frac{dq}{dt} = \frac{\mathcal{E}}{R} e^{-\frac{t}{RC}}$

2) 放电: $iR = \frac{q}{C}$, $i = -\frac{dq}{dt}$

$$\therefore R \frac{dq}{dt} + \frac{q}{C} = 0 \Rightarrow dt = -RC \frac{dq}{q}$$

$$\therefore t = -RC \ln \frac{q}{q_0} = -RC \ln \frac{q}{C\mathcal{E}}, \quad i q = C\mathcal{E} e^{-\frac{t}{RC}}$$

$$i = -\frac{dq}{dt} = \frac{C\mathcal{E}}{RC} e^{-\frac{t}{RC}} = \frac{\mathcal{E}}{R} e^{-\frac{t}{RC}} \text{ 与充电的电流曲线一样。}$$

3. 电感

$$\textcircled{1} \quad \Sigma \mathcal{E}_L = - \frac{d\psi}{dt} = - \frac{Nd\phi}{dt} = - \frac{d(Li)}{dt} = -L \frac{di}{dt}$$

$$\therefore L = - \Sigma \mathcal{E}_L \frac{dt}{di}$$

$$\textcircled{2} \text{ 串联: } L_{\text{总}} = - \Sigma \mathcal{E}_L \frac{dt}{di} = \Sigma \mathcal{E}_L \frac{dt}{di} = \Sigma L_i$$

$$\text{并联: } \frac{1}{L_{\text{总}}} = - \frac{d(\Sigma i)}{\Sigma i dt} = - \frac{d \Sigma i}{\Sigma i dt} = \Sigma - \frac{di}{i dt} = \Sigma \frac{1}{L_i}$$

\textcircled{3} 电感的能量:

$$W = \int \Sigma \mathcal{E}_L i dt = \int -L \frac{di}{dt} i dt = \int_{\frac{1}{2}}^1 L i di = \frac{1}{2} L I^2$$

$$= \frac{1}{2} \mu_0 n^2 V I^2 \quad \text{又由 } B = \mu_0 n I \text{ 消去 } n I \text{ 得}$$

$$W = \frac{B^2}{2\mu_0} V$$

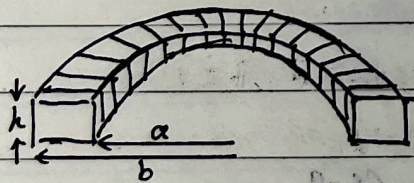
$$\text{能量密度 } w = \frac{dW}{dV} = \frac{B^2}{2\mu_0}$$

\textcircled{4} 自感:

$$1) \text{ 螺线管: } \psi = N\phi = l \cdot n \cdot BS = l n \mu_0 n I S = L I$$

$$\therefore L = \frac{\psi}{I} = \mu_0 n^2 S l = \mu_0 n^2 V \quad [n: \text{导线数密度 (条/m)}]$$

2) 环式螺线管:



对整个环用安培环路定理:

$$B \cdot 2\pi r = \mu_0 N I$$

$$\therefore B = \frac{\mu_0 N I}{2\pi r}$$

$$\therefore \text{磁通匝链数 } \psi = \int_a^b B \cdot h \cdot dr = \frac{\mu_0 N I h}{2\pi} \ln \frac{b}{a}$$

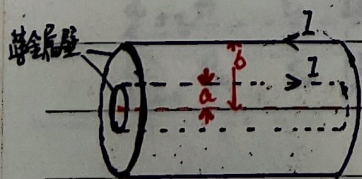
$$\therefore L = \frac{\mu_0 N^2 h}{2\pi} \ln \frac{b}{a}$$

3) 同轴电缆:

对单位长度的电缆, 有

$$\psi = \int_a^b B l dr = \frac{\mu_0 I l}{2\pi} \int_a^b \frac{dr}{r} = \frac{\mu_0 I l}{2\pi} \ln \frac{b}{a}$$

$$\therefore L = \frac{\mu_0 l}{2\pi} \ln \frac{b}{a}$$

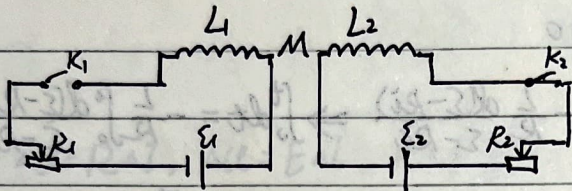


⑤ 互感

$$\varepsilon_{21} = -M_{21} \frac{di_1}{dt}, \quad \varepsilon_{12} = -M_{12} \frac{di_2}{dt}$$

$$\text{且 } M_{12} = M_{21} = M$$

证明:



(1) 在左回路中建立 i_1 , 使电源做功, 在磁场中储能 $W_1 = \frac{1}{2} L_1 I_1^2$.

(2) 在右回路中建立 i_2 , 使电源 ε_2 做功, 储能 $W_2 = \frac{1}{2} L_2 I_2^2$, 但在此过程中 L_1 产生反电动势, 为保持 i_1 不变, ε_1 还应做功 $W_2 = -\int \varepsilon_{12} I_1 dt$
 $= \int M_{12} I_1 \frac{di_2}{dt} dt = M_{12} I_1 \int_0^{I_2} di_2 = M_{12} I_1 I_2$.

(3) 经上述两过程后系统达到电流分别是 I_1 和 I_2 的状态,

$$W_{总} = W_1 + W_2 + W_{12} = \frac{1}{2} L_1 I_1^2 + \frac{1}{2} L_2 I_2^2 + M_{12} I_1 I_2$$

(4) 从在右回路中建立 i_2 起达到同样的结果, 做功同理为:

$$W_{总} = \frac{1}{2} L_1 I_1^2 + \frac{1}{2} L_2 I_2^2 + M_{21} I_1 I_2$$

$$\therefore M_{12} = M_{21}$$

长螺线管与圆环的互感: (管 \gg 环, 环在管轴线上, 轴与环平面垂直)

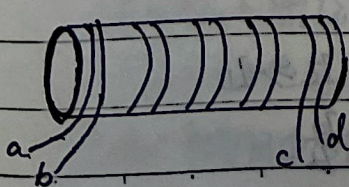
设螺线管内电流为 i_1 , 则通过圆环的全磁通 $\Phi = B_1 \pi r^2 = \mu_0 n i_1 \pi r^2$

$$\therefore M_{21} = \pi r^2 \mu_0 n$$

$$\therefore M_{12} = M_{21} = \pi r^2 \mu_0 n$$

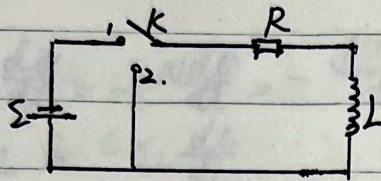
⑥ 等效电感

在互相远离的情况下, 与等效电阻的计算方法类似; 互相影响下的特例:



单独存在时 $\left\{ \begin{array}{l} a-c \text{ 或 } b-d \text{ 接入电路: } L=0 \\ c \text{ 连 } b, a-d \text{ 接入电路: } \psi = (2N)(\mu_0 2n_0 I) S, L=4L_0 \\ a \text{ 连 } b, c \text{ 或 } d \text{ 接入电路: } \psi = N_0 (\mu_0 n_0 \frac{I}{2}) S \times 2, L=L_0 \end{array} \right.$

① RL 电路:



$$1) \quad \Sigma + (-L \frac{di}{dt}) - iR = 0$$

$$\therefore dt = \frac{L di}{\Sigma - Ri} = -\frac{L}{R} \frac{d(\Sigma - Ri)}{\Sigma - Ri} \Rightarrow \int_0^t dt = -\frac{L}{R} \int_0^t \frac{d(\Sigma - Ri)}{\Sigma - Ri}$$

$$\therefore t = -\frac{L}{R} \ln\left(\frac{\Sigma - Ri}{\Sigma}\right) \quad \text{解得 } i = \frac{\Sigma}{R}(1 - e^{-\frac{Rt}{L}})$$

$$\therefore U_L = -L \frac{di}{dt} = -\Sigma \cdot e^{-\frac{Rt}{L}}$$

$$2) \quad -L \frac{di}{dt} - iR = 0$$

$$\therefore dt = -\frac{L}{R} \frac{di}{i} \Rightarrow \int_0^t dt = -\frac{L}{R} \int_{i_0}^i \frac{di}{i}$$

$$\therefore t = -\frac{L}{R} \ln \frac{i}{i_0} \quad \text{解得 } i = \frac{i_0}{R} e^{-\frac{Rt}{L}}$$

$$\therefore U_L = -\frac{d\phi}{dt} = \Sigma e^{-\frac{Rt}{L}}$$

4. 半导体.

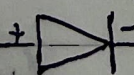
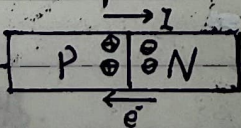
① 二极管.

理想二极管: 正向导通时 $R=0$, 反向 R 为 ∞ .

实际二极管: $i = I_s(e^{\frac{qV}{kT}} - 1)$.

P型半导体: 空穴导电.

N型半导体: 电子导电.

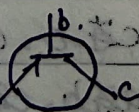
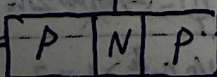


② 三极管.

基极 b

发射极 e

集电极 c



$$\begin{cases} I_e = I_b + I_c, & I_c \gg I_b \\ \beta = \frac{dI_c}{dI_b} \approx \frac{I_c}{I_b} \end{cases}$$

十. 稳恒电流

1. 电流连续性方程: $\oint_S \vec{j} \cdot d\vec{s} = -\frac{dq}{dt}$

稳恒条件: $\oint_S \vec{j} \cdot d\vec{s} = -\frac{dq}{dt} = 0$

2. 欧姆定律

$$U = IR$$

$$\because \Delta l = j \Delta s, \Delta U = R \Delta I, \Delta U = E \Delta l, R = \rho \frac{\Delta l}{\Delta s}$$

$$\therefore j = \frac{\Delta I}{\Delta s} = \frac{\Delta U}{\rho \frac{\Delta l}{\Delta s}} = \frac{E \Delta l}{\rho \frac{\Delta l}{\Delta s}} = \sigma E$$

写成矢量形式 $\vec{j} = \sigma \vec{E}$, 代入高斯定律, $\frac{1}{\sigma} \oint_S \vec{j} \cdot d\vec{s} = \frac{q}{\epsilon_0}$

$\therefore -\frac{dq}{dt} = \frac{q}{\epsilon_0} \sigma$ 解得 $q = q_0 e^{-\sigma t}$, 表示在电路中建立稳恒电流的过程.

3. 全电路欧姆定律. 焦耳定律.

① 对于纯电阻(电能做功全用于发热)电路, 电源电动势 $\mathcal{E} = IR + Ir$.

其中, 路端电压 $U = IR = \mathcal{E} - Ir = -rI + \mathcal{E}$, 是 I 的线性函数.

电源总功率: $P_{总} = \mathcal{E}I = I^2 R + I^2 r$

内阻功率: $P_{内} = I^2 r$

电源输出功率: $P_{输} = I^2 R$

(1) $P_{输} = I^2 R = (\mathcal{E} - Ir)I = -rI^2 + \mathcal{E}I = -r\left(I - \frac{\mathcal{E}}{2r}\right)^2 + \frac{\mathcal{E}^2}{4r}$

当 $I = \frac{\mathcal{E}}{2r}$ 时, $P_{max} = \frac{\mathcal{E}^2}{4r}$

(2) $P_{输} = I^2 R = \left(\frac{\mathcal{E}}{R+r}\right)^2 R = \frac{\mathcal{E}^2 R}{R^2 + 2Rr + r^2} \leq \frac{\mathcal{E}^2}{4r}$

此时 $R = r$ (即 $r = R$)

(3) $P_{输} = UI = U \cdot \frac{\mathcal{E} - U}{r} = -\frac{1}{r}U^2 + \frac{\mathcal{E}}{r}U = -\frac{1}{r}\left(U - \frac{\mathcal{E}}{2}\right)^2 + \frac{\mathcal{E}^2}{4r}$

当 $U = \frac{\mathcal{E}}{2}$ 时, $P_{max} = \frac{\mathcal{E}^2}{4r}$

② 电流的微观解释:

$$\vec{v}_i = \vec{v}_{i0} + \frac{eE}{m} t_i, \text{ 而 } \vec{j} = ne\vec{v}_i, \therefore \vec{j} = ne\vec{v}_{i0} + \frac{ne^2 E}{m} t_i$$

$\because \vec{v}_{i0}$ 为电子热运动产生的向各个方向的初速度 $\therefore n\vec{v}_{i0} = 0$

设电子平均自由飞行时间 $\tau = \frac{\sum t_i n_i}{n}$, $\therefore \vec{j} = \frac{ne^2 \tau}{m} E, \therefore \sigma = \frac{ne^2 \tau}{m}$

$$\vec{v}_i = \vec{v}_{i0} + \frac{e\vec{E}}{m} t_i$$

$$\therefore \frac{1}{2} m \vec{v}_i^2 = \frac{e^2 E^2}{2m} t_i^2 + \frac{1}{2} m v_{i0}^2 + \frac{e t_i}{m} \vec{v}_{i0} \cdot \vec{E}$$

$$\text{对大量电子取平均: } \overline{\frac{1}{2} m \vec{v}_i^2} = \overline{\frac{1}{2} m v_{i0}^2} + \frac{e^2 E^2}{2m} \overline{t_i^2}$$

$$\therefore \Delta E_k = \overline{\frac{1}{2} m v_i^2} - \overline{\frac{1}{2} m v_{i0}^2} = \frac{e^2 E^2}{2m} \overline{t_i^2}$$

$$\text{又: } \overline{t_i^2} = 2\tau^2$$

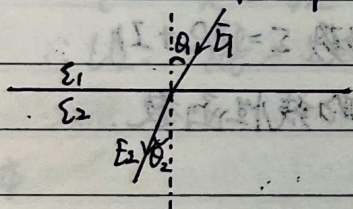
$$\therefore (\text{单位体积中}) \text{热功率密度 } p = \frac{n \Delta E_k}{\tau} = \frac{n e^2 I E^2}{m} = \sigma E^2$$

$$\therefore \text{热功率 } P = p \cdot V = \sigma E^2 l s = j^2 \frac{l s}{\sigma} = \frac{I^2 l}{\sigma} = I^2 R$$

故电流做功 $\left\{ \begin{array}{l} \text{总功: } W = qU = UI t \\ \text{发热: } Q = Pt = I^2 R t \end{array} \right. \left\{ \begin{array}{l} \text{若为纯电阻电路, } W = Q \Rightarrow U = IR \\ \text{若为非纯, } W' = UI t - I^2 R t. \end{array} \right.$

4. 边界条件.

① 场强的边界条件.

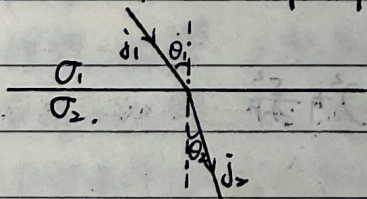


$$\text{高斯定理: } \epsilon_1 E \cos \theta_1 = \epsilon_2 E \cos \theta_2$$

$$\text{环路定理: } E_1 \sin \theta_1 = E_2 \sin \theta_2$$

$$\therefore \frac{\tan \theta_1}{\tan \theta_2} = \frac{\epsilon_1}{\epsilon_2}$$

② 电流密度的边界条件:



$$\text{连续性条件: } j_1 \cos \theta_1 = j_2 \cos \theta_2 \quad \text{欧姆定律: } \vec{j} = \sigma \vec{E}$$

$$\text{环路定理: } \frac{j_1}{\sigma_1} \sin \theta_1 = \frac{j_2}{\sigma_2} \sin \theta_2$$

$$\therefore \frac{\tan \theta_1}{\tan \theta_2} = \frac{\sigma_1}{\sigma_2}$$

$$\therefore \text{交界面处有自由电荷积累: } \sigma_e = \epsilon_0 \left(\frac{j_2}{\sigma_2} \cos \theta_2 - \frac{j_1}{\sigma_1} \cos \theta_1 \right) = \epsilon_0 \frac{j_2}{\sigma_2} \frac{\epsilon_0 (\sigma_1 - \sigma_2)}{\epsilon_0 \sigma_1}$$

5. 解复杂电路

① 基尔霍夫电流定律:

节点: $\sum I_i = 0$ (节点可以是一片区域; 电流流入为正流出为负或相反)

(理论依据: 稳恒条件 $\oint \vec{j} \cdot d\vec{s} = -\frac{dq}{dt} = 0$.)

② 基尔霍夫电压定律:

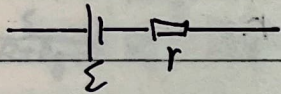
一段: $\sum U_i = \varphi_a - \varphi_b = \sum \mathcal{E}_i + \sum I R_i$ (电势下降为正上升为负或相反)

回路: $\sum U_i = 0$ (电阻上电流方向为电势降落方向, 电源上正极指向负极...)

(理论依据: $U_{ab} = \varphi_a - \varphi_b = \int_a^b \vec{E} \cdot d\vec{l}$, $\oint \vec{E} \cdot d\vec{l} = 0$)

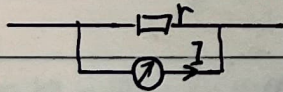
③ 戴维宁定理:

等效电压源 $\left\{ \begin{array}{l} \mathcal{E} = \text{网络开路端电压,} \\ r = \text{除电源留内阻后网络的等效电阻.} \end{array} \right.$



④ 诺尔顿定理:

等效电流源 $\left\{ \begin{array}{l} I = \text{网络两端短接后电流.} \\ r = \text{除电源留内阻后网络的等效电阻.} \end{array} \right.$



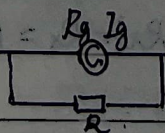
⑤ 叠加原理:

通过电路任一支路的电流等于各电源单独存在时 (其它电源只留内阻) 在该支路产生的电流之代数和

(理论依据: $I = \vec{j} \cdot \vec{s} = \vec{j} \cdot \vec{s} = \vec{j} \cdot (\sum \vec{G}_i) \vec{s} = \sum (\vec{j} \cdot \vec{G}_i \cdot \vec{s})$)

6. 改装电流表 ⑥

① 安培表 A:

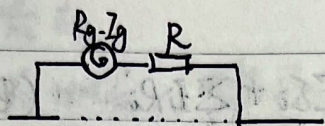


并联分流电阻

$$\text{量程} = I = \frac{I_g R_g}{R_g + R} = \frac{R_g + R}{R} I_g$$

$$\therefore R = \frac{R_g}{n-1}$$

② 伏特表

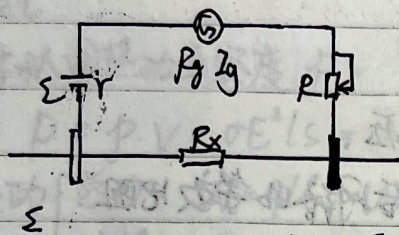


串联分压大电阻

量程: $U = (R_g + R)I_g$

$\therefore R = (n-1)R_g$

③ 欧姆表:



$I_{测} = \frac{E}{r + R_g + R + R_x} \Rightarrow R_x = \frac{E}{I_{测}} - R - R_g - r$

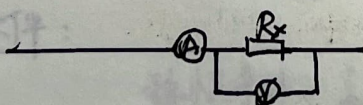
\therefore 电流表刻度均匀,

\therefore 安培表、伏特表刻度均匀, 欧姆表刻度不均匀.

7. 测量电阻、电表内阻.

① 伏安法:

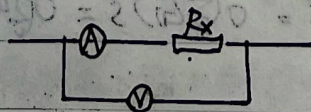
1) ① 外接:



由于①分流, $I_{测} > I_{实}$, $\therefore R_{测} = \frac{U}{I_{测}} < R_{实}$.

$R_{实} = R_{测} - R_{测} = R_x - \frac{U}{I_{测}} = R_x - \frac{R_x R_V}{R_x + R_V} = \frac{R_x^2}{R_x + R_V}$

2) ① 内接:



由于①分压, $U_{测} > U_{实}$, $\therefore R_{测} = \frac{U_{测}}{I} > R_{实}$.

$R_{实} = R_{测} - R_{实} = \frac{U_{测}}{I} - R_x = (R_x + R_A) - R_x = R_A$

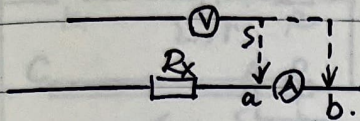
3) 选择①的接法:

令 $\frac{R_x^2}{R_x + R_V} = R_A$, 则 $\frac{R_x}{R_V} = \frac{R_A}{R_x} + \frac{R_A}{R_V}$. $\therefore R_A \ll R_V, \therefore \frac{R_x}{R_V} \approx \frac{R_A}{R_x}$

① 当 $R_x > \sqrt{R_A R_V}$ 时, 用内接法, 使电表分流少.

② 当 $R_x < \sqrt{R_A R_V}$ 时, 用外接法, 使电表分压少.

③ 当 R_x 未知时:



若电流表示数显著变化, S 应接 b .
 (说明接 a 时 ④ 分流不少, 故 R_x 是大电阻, 用内接法)
 若电压表示数显著变化, S 应接 a .
 (说明接 b 时 ④ 分压不少, 故 R_x 是小电阻, 用外接法)

让 S 与 a, b 分别接触一下

④ 欧姆法:

$$R_{测} = \frac{\mathcal{E}}{I_{测}} - R - R_g - r$$

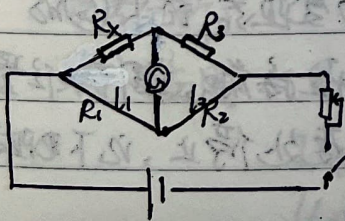
$I_{测} \rightarrow 0$ 时, $R_{测} \rightarrow \infty$.

$I_{测} = \frac{\mathcal{E}}{R + R_g + r}$ 时, $R_{测} = 0$.

$$\therefore R_{中} = \frac{\mathcal{E}}{\frac{I_{测}}{2}} - R - R_g - r = R + R_g + r$$

$\therefore R_{测} = \frac{\mathcal{E}}{I_{测}} - R_{中}$, $R_{中}$ 为欧姆表中最中间刻度处的欧姆值, 可直接读出.

⑤ 电桥法:



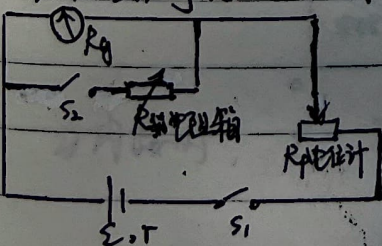
⑥ 中 $I = 0$ 时, 电桥平衡.

$$\text{此时 } U_x = U_1, U_2 = U_3, I_1 = I_2, I_x = I_3$$

$$\therefore R_x I_x = R_1 I_1, R_2 I_2 = R_3 I_3$$

$$\therefore R_x = \frac{R_1}{R_2} \cdot R_3 = \frac{1}{2} \cdot R_3$$

⑦ 半偏法测电流表内阻.



闭合 S_1 , 调节 R_p 使电流表满偏.

再闭合 S_2 , 调节 $R_{箱}$ 使电流表半偏, 设此时 $R_{箱}$ 电流为 I' .

$$\therefore \frac{1}{2} R_g = I' R_{箱} \quad \therefore I' = \frac{R_g}{2R_{箱}} I_g$$

\therefore 路端电压近似不变

$$\therefore I_g R_g + I_g R_p = \frac{1}{2} R_g + (\frac{1}{2} + I') R_p = \frac{1}{2} R_g + (\frac{1}{2} + \frac{R_g}{2R_{箱}} I_g) R_p$$

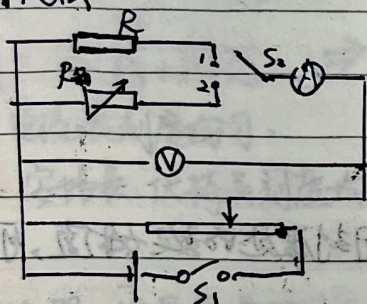
$$\text{化简得: } R_g = \frac{R_{箱} R_p}{R_p - R_{箱}}$$

误差分析:
$$\begin{cases} I_g R_g + I_g (R_p + r) = \Sigma \\ \frac{1}{2} I_g R_g + (\frac{1}{2} I_g + I') (R_p + r) = \Sigma \\ \frac{1}{2} I_g R_g = I' R_{\text{辅}} \end{cases}$$

$$\therefore \frac{\Sigma - I_g R_g}{\Sigma - \frac{1}{2} I_g R_g} = \frac{I_g}{\frac{1}{2} I_g + I'} = \frac{I_g}{\frac{1}{2} I_g + \frac{K_A}{2 R_{\text{辅}}} \cdot I_g} = \frac{2}{1 + \frac{R_g}{R_{\text{辅}}}}$$

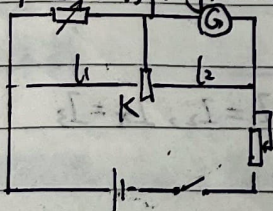
$$\therefore \frac{R_g}{R_{\text{辅}}} = \frac{\Sigma}{\Sigma - I_g R_g} \text{ --- 相对误差.}$$

⑤ 替代法



将 S_2 打至 1, 调节滑动变阻器, 记下 ④ 的读数; 再将 S_2 打至 2, 调节电阻箱阻值, 使 ④ 的读数与刚才一致, 则 $R = R_g$.

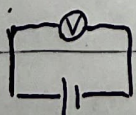
⑥ 惠斯通电桥测微安表内阻



电路接通时, 调节滑动变阻器, 记下 ⑥ 的读数; 再将 K 与半只电阻接触, 调节其位置, 在使 ⑥ 与原先不变的刻度处停止, 记下电阻箱阻值 $R_{\text{辅}}$, $\therefore R_g = \frac{l_1}{l_2} R_{\text{辅}}$.

8. 测量电动势:

① 伏特表法:



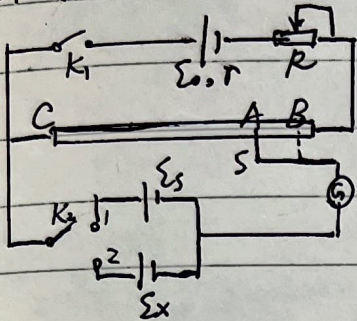
$$\mathcal{E} = U.$$

误差分析: $\Sigma_{\text{测}} = U_{\text{测}}, \mathcal{E}_{\text{实}} = I r + U_{\text{测}} = \frac{\Sigma_{\text{测}} r}{R_v + r} + U_{\text{测}}$

$$\therefore \mathcal{E}_{\text{实}} = \frac{R_v + r}{R_v} \cdot U_{\text{测}}, \text{ 测量值偏小.}$$

$$= \frac{R_v + r}{R_v} \cdot \Sigma_{\text{测}}$$

② 电位计法:



闭合 \$K_1\$, 闭合 \$K_2\$ 至 1.

调节 \$S\$ 至 \$A\$, 调节 \$R\$ 使通过 \$E_s\$ 的电流为 0.

$$\therefore I = \frac{E_0}{R_{AC} + R + r}$$

$$\therefore E_s = I R_{AC} = \frac{E_0 R_{AC}}{R_{AC} + R + r}$$

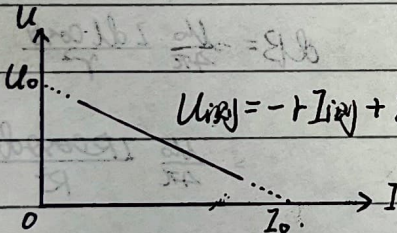
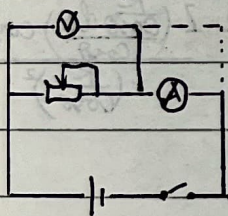
闭合 \$K_2\$ 至 2, 将导线移至 \$B\$ 使通过 \$E_x\$ 的电流为 0.

$$\therefore I' = \frac{E_0}{R_{BC} + R + r}$$

$$\therefore E_x = I' R_{BC} = \frac{E_0 R_{BC}}{R_{AC} + R + r}$$

$$\therefore E_x = \frac{R_{BC}}{R_{AC}} \cdot E_s = \frac{BC}{AC} \cdot E_s$$

③ U-I 图法:



$U_{测} = -r I_{测} + E$ ← 实验结果计算

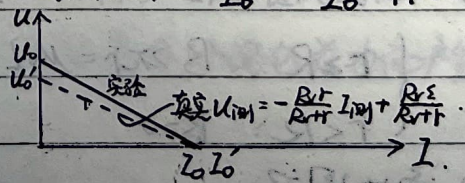
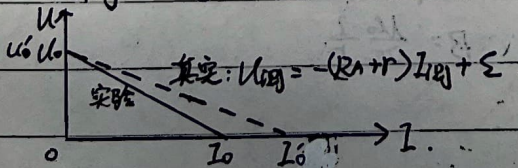
$I_{测} = 0, E = U_0$, 断路
 $U_{测} = 0, r = \frac{U_0}{I_0}$, 短路

误差分析:

1) 外接时, $E = I_{测}(r + R_A) + U_{测}$, $\therefore U_{测} = -(R_A + r) I_{测} + E$.

$I_{测} = 0$ 时, $E_{实} = U_0'$ 真实.

$U_{测} = 0$ 时, $r_{实} = \frac{U_0'}{I_0} - R_A$, 故实验值 $r = \frac{U_0}{I_0} = \frac{U_0'}{I_0}$ 偏大, 如图.



2) 内接时, $E = I_A r + U_{测} = \frac{U_{测}}{\frac{R_V(R_A + R)}{R_V + R_A + R}} \cdot r + U_{测}$

$$= \frac{R_V + r}{R_V} \cdot U_{测} + I_{测} r \quad \therefore U_{测} = -\frac{R_V r}{R_V + r} I_{测} + \frac{R_V E}{R_V + r}$$

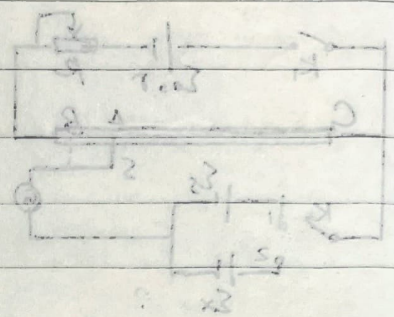
$I_{测} = 0$ 时, $E_{实} = \frac{R_V + r}{R_V} U_0'$, 故实验值 $E = U_0'$ 偏小.

$U_{测} = 0$ 时, $r_{实} = \frac{E}{I_0}$, 故实验值 $r = \frac{U_0'}{I_0} = \frac{E}{I_0}$ 真实 偏大

十一. 静磁场.

1. 毕-萨定律:

$$dB = \frac{\mu_0}{4\pi} \frac{I d\vec{l} \times \vec{r}}{r^2} \quad \vec{B} = \int d\vec{B}$$



2. 高斯定理: $\oint_S \vec{B} \cdot d\vec{S} = 0$

环路定理: $\oint_L \vec{B} \cdot d\vec{l} = \mu_0 \sum I$

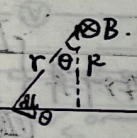
3. 典型载流体系磁场:

① 无限长导线 (电流 I)

$$\therefore B \cdot 2\pi r = \mu_0 I$$

$$\therefore B = \frac{\mu_0 I}{2\pi r}$$

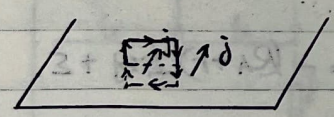
有限长导线 (电流 I)



$$dB = \frac{\mu_0}{4\pi} \frac{I dl \cos\theta}{r^2} = \frac{\mu_0}{4\pi} I \frac{(\frac{R \cos\theta d\theta}{\cos\theta}) \cos\theta}{(\frac{R}{\cos\theta})^2}$$

$$= \frac{\mu_0}{4\pi} \frac{I R \cos\theta d\theta}{R^2}$$

② 无限宽平板 (电流密度 j)



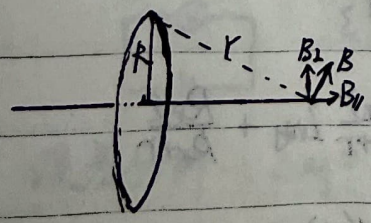
$$\sum B L = \mu_0 j L$$

$$\therefore B = \frac{1}{2} \mu_0 j$$

③ 无限长圆柱面 (半径 R, 表面均匀分布电流 I)

$$\begin{cases} r \geq R: B \cdot 2\pi r = \mu_0 I, \therefore B = \frac{\mu_0 I}{2\pi r} \\ r < R: B = 0. \end{cases}$$

④ 通电圆环

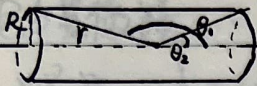


$$dB = \frac{\mu_0}{4\pi} I \frac{dl}{r^2} = \frac{\mu_0}{4\pi} \frac{I \cdot R d\theta}{r^2}$$

$$\therefore B_L = 0, B_r = \frac{\mu_0}{4\pi} \left(\frac{2\pi R I}{r^2} \cdot R \right) = \frac{\mu_0 I R^2}{2r^3}$$

$$\text{当 } r=R \text{ 时, } B = \frac{\mu_0 I}{2R}$$

⑤ 通电螺线管 (单位长度匝数 n, 总匝数 N, 每匝电流 I)



$$\therefore dl = nI dl, \quad \therefore dB = \frac{\mu_0 R^2 n I dl}{2r^3}$$

$$\text{又} \because dl = \left(\frac{R}{\sin \theta} d\theta \right) / \epsilon_0 = \frac{R}{\epsilon_0} d\theta, \quad \text{且 } r = \frac{R}{\cos \theta}$$

$$\therefore dB = \frac{\mu_0 n I}{2} \epsilon_0 d\theta \quad \therefore B = \frac{\mu_0 n I}{2} (\cos \theta_2 - \cos \theta_1)$$

当管无限长时, $B = \mu_0 n I$.

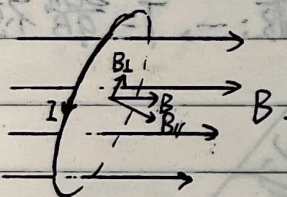
4. 洛伦兹力.

$$\vec{F} = q \vec{v} \times \vec{B}$$

对于一段导线元, $d\vec{F} = dq \vec{v} \times \vec{B} = nSe dl \cdot \vec{v} \times \vec{B} = nSev d\vec{l} \times \vec{B} = I d\vec{l} \times \vec{B}$

$\therefore \vec{F} = \int I d\vec{l} \times \vec{B}$ — 安培力.

① 安培力矩.



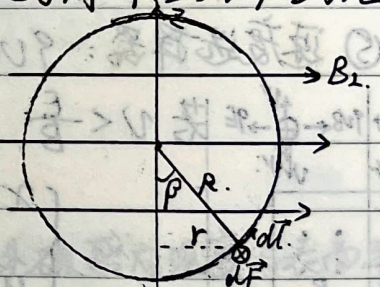
$dF_1 = I dl B_{\parallel}$ 与线圈处于同一平面, 不产生力矩.

$$dF_2 = I dl B_{\perp} \sin \beta$$

$$\therefore dM = dF_2 \cdot r$$

$$= I dl B_{\perp} \sin \beta \cdot r$$

$$= I R d\beta B_{\perp} \sin \beta R \sin \beta$$



$$\therefore M = I R^2 B_{\perp} \int_0^{\pi} \sin^2 \beta d\beta = \pi \cdot I R^2 B_{\perp} \quad \text{写成矢量形式 } \vec{M} = I \vec{S} \times \vec{B}.$$

定义磁矩 $\vec{m} = I \vec{S}$, $\therefore \vec{M} = \vec{m} \times \vec{B}$.

② 洛伦兹力不做功

$$P = \vec{F} \cdot \vec{v} = (q \vec{v} \times \vec{B}) \cdot \vec{v}$$

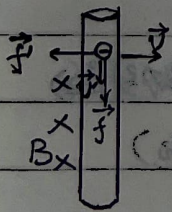
由于电子随导线在磁场中的 \vec{v} 运动, 电子受到沿导线的洛伦兹力而产生速度 \vec{v}' .

$$P = (\vec{F} + \vec{F}') \cdot (\vec{v} + \vec{v}')$$

$$= \vec{F} \cdot \vec{v} + \vec{F}' \cdot \vec{v}'$$

$$= e v B \cdot v' - e v B v'$$

$$(v' = v \times B) \quad \therefore (v' \cdot v) = 0$$



3. 应用

① 霍尔效应.

$$(-E_H = vB, \quad U_H = E_H h = vBh, \quad \text{又} \because I = n b h q v, \quad \therefore U_H = \frac{IB}{nqB})$$

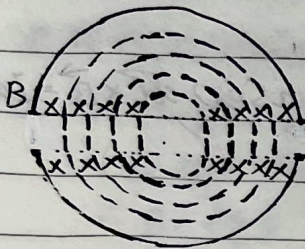
① 霍尔电阻 $R_H = \frac{B}{nqb}$

② 电流表: $BIS = kD$

③ 质谱仪: $m\frac{v^2}{r} = qvB$

$\therefore r = \frac{mv}{qB}, T = \frac{2\pi m}{qB}$

④ 回旋加速器



$qU = \frac{1}{2}mv_1^2, r_1 = \frac{mv_1}{qB}, v_1 = \sqrt{\frac{2qU}{m}}$

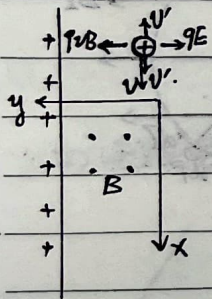
$qU = \frac{1}{2}mv_2^2 - \frac{1}{2}mv_1^2, r_2 = \frac{mv_2}{qB}, v_2 = \sqrt{\frac{4qU}{m}}$

$qU = \frac{1}{2}mv_3^2 - \frac{1}{2}mv_2^2, r_3 = \frac{mv_3}{qB}, v_3 = \sqrt{\frac{6qU}{m}}$

....

$\therefore v_1 : v_2 : v_3 : \dots = r_1 : r_2 : r_3 : \dots = 1 : \sqrt{2} : \sqrt{3} : \dots, T = \frac{2\pi m}{qB}$ 不变

⑤ 速度选择器: $qUB = qE, \therefore v = \frac{E}{B}$



若 $v < \frac{E}{B}$, $qB(v+U) = qE, \therefore v = \frac{E}{B} - U$

$x = \frac{E}{B}t - \frac{m(\frac{E}{B} - U)}{qB} \sin(\frac{qB}{m}t)$

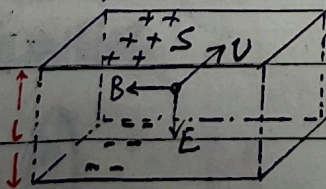
$y = \frac{m(\frac{E}{B} - U)}{qB} \cos(\frac{qB}{m}t) - \frac{m(\frac{E}{B} - U)}{qB}$

若 $v > \frac{E}{B}$, $qBv = qE + qBU', \therefore v' = v - \frac{E}{B}$

$x = \frac{E}{B}t + \frac{m(v - \frac{E}{B})}{qB} \sin(\frac{qB}{m}t)$

$y = \frac{m(v - \frac{E}{B})}{qB} - \frac{m(v - \frac{E}{B})}{qB} \cos(\frac{qB}{m}t)$

⑥ 磁流体发电机



非静电力: $E_{nc} = \frac{f}{q} = vB$ (由洛伦兹力引起)

静电力: E_s (由上下电荷积累引起)

$\therefore I = \sigma(E_{nc} - E_s) \cdot S$ (σ : 电导率)

总功率: $P = IE_{nc}l$

内阻功率: $P = I(E_{nc} - E_s)l$

输出功率: $P = IE_s l = \sigma(vB - E_s)E_s V \leq \frac{1}{4}\sigma v^2 B^2 V$ (V 为电极间总体积)

① 电子显微镜:

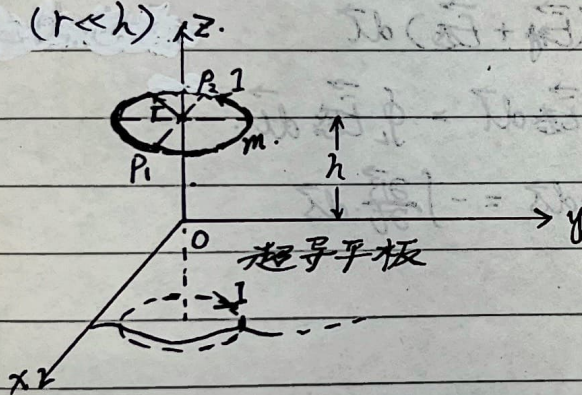
$$\text{螺距: } h = v \cdot T = \frac{2\pi m}{9B} \cdot v \approx \frac{2\pi m}{9B} \cdot v$$

② 磁镜:

$$|\vec{m}| = |\vec{S} \cdot \vec{I}| = \frac{\pi R^2 q}{T} = \frac{\pi \frac{mv^2}{9B^2} \cdot 8}{\frac{2\pi m}{9B}} = \frac{4mv^2}{B}$$

$$\text{由于磁矩守恒, } \frac{mv_{\perp}^2}{2B_0} = \frac{mv^2 \sin^2 \theta}{2B_0} = \frac{mv^2}{2B} \quad \therefore \sin \theta = \sqrt{\frac{B_0}{B_m}}$$

③ 像电流: ($r \ll h$)



由于 $r \ll h$, 且超导体内部磁感应强度为零, 外表面外磁感应强度与表面平行, 故等效于一个 $z = -h$ 处的环状像电流, 两环状电流反向平行.

$$mg = \frac{\mu_0 I}{2\pi} \frac{1}{2h} \cdot 2\pi r \cdot I$$

$$\therefore I = \sqrt{\frac{2mgh}{\mu_0 r}}$$

1) 若圆环上下微振动, $F = \frac{\mu_0 I^2}{2(h-x)} - mg \approx -mg + \frac{\mu_0 I^2}{2h} (1 + \frac{x}{h}) \approx \frac{\mu_0 I^2}{2h} x$

$$\therefore T = 2\pi \sqrt{\frac{2mI^2}{\mu_0 I^2}} = 2\pi \sqrt{\frac{h}{g}}$$

2) 若以 P_1, P_2 为轴微摆动, $M \approx \frac{\mu_0 I^2}{2} \left(\frac{1}{2h-r\theta} - \frac{1}{2h+r\theta} \right) \cdot r \approx \frac{\mu_0 I^2 r^2}{4h^2} \theta$

$$= \frac{mgr^2}{2h} \theta, \quad \therefore T = 2\pi \sqrt{\frac{\frac{1}{2}mr^2}{\frac{mgr^2}{2h}}} = 2\pi \sqrt{\frac{h}{g}}$$

十二. 电磁感应与交流电.

1. 法拉第电磁感应定律.

$$\varepsilon = - \frac{d\phi}{dt} = - \frac{d}{dt} \int \vec{B} \cdot d\vec{s}$$

\vec{s} 方向由右手螺旋定则应用于环流方向上确定;

若 ϕ 随时间变大, 则 ε 与环流方向相反; 反之, 则与环流同向.

① 动生: $|\varepsilon| = \frac{d\phi}{dt} = \frac{d}{dt} (B l v) = B l v$

对于一般导体: $\varepsilon_{ab} = \int_a^b (\vec{v} \times \vec{B}) \cdot d\vec{l}$

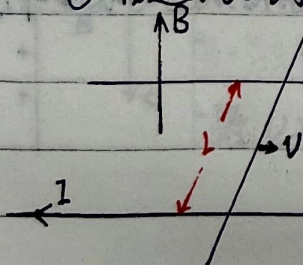
② 感生: $|\varepsilon| = \oint_L \vec{E} \cdot d\vec{l} = \oint_L (\vec{E}_{\text{静}} + \vec{E}_{\text{感}}) \cdot d\vec{l}$

$$= \oint_L \vec{E}_{\text{静}} \cdot d\vec{l} + \oint_L \vec{E}_{\text{感}} \cdot d\vec{l} = \oint_L \vec{E}_{\text{感}} \cdot d\vec{l}$$

$$\therefore \oint_L \vec{E}_{\text{感}} \cdot d\vec{l} = - \frac{d}{dt} \int \vec{B} \cdot d\vec{s} = - \int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

2. 典例:

① 初速为 v_0 的导体棒.



$$\therefore F = B l I$$

$$\text{动量: } m \frac{dv}{dt} = B l \frac{B l v}{R} = \frac{B^2 l^2 v}{R}$$

$$\therefore \frac{dv}{v} = \frac{B^2 l^2}{m R} dt$$

$$\therefore \ln \frac{v}{v_0} = \frac{B^2 l^2}{m R} t$$

$$\therefore v = v_0 e^{-\frac{B^2 l^2}{m R} t}$$

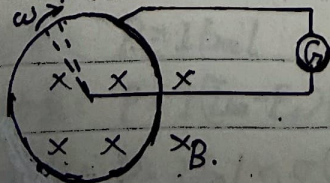
$$\text{能量: } dW = I \varepsilon dt = I B l v dt$$

$$\text{而 } F dt = B l I dt = m dv$$

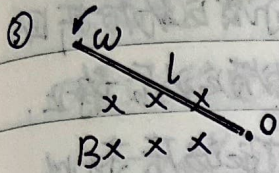
$$\therefore dW = I B l v \frac{m dv}{B l I} = m v dv$$

$$\therefore \int I \varepsilon dt = \frac{1}{2} m v_0^2 - \frac{1}{2} m v^2. \text{ 能量守恒.}$$

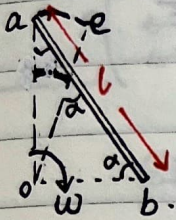
② 旋转圆盘.



$$\varepsilon = \frac{B ds}{dt} = \frac{B \cdot \frac{1}{2} d\theta \cdot R^2}{dt} = \frac{1}{2} B \omega R^2$$

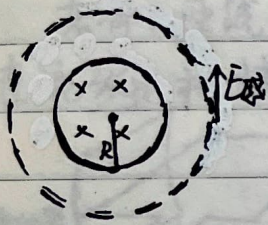


$$\Sigma = \int B v dl = \int B v l d\alpha = \frac{1}{2} B v l^2$$



$$\begin{aligned} \Sigma_{ab} = \Sigma_{ac} = U_a - U_b &= \frac{1}{2} B \omega l^2 (\cos \alpha)^2 - \frac{1}{2} B \omega l^2 (\sin \alpha)^2 \\ &= \frac{1}{2} B \omega l^2 \cos 2\alpha \end{aligned}$$

④ 圆环导线的感生电动势



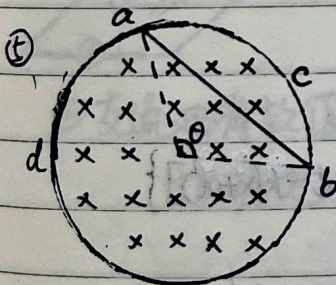
$$\oint \vec{E} \cdot d\vec{l} = E \cdot 2\pi r$$

$$r > R \text{ 时, } E \cdot 2\pi r = \pi R^2 \frac{dB}{dt}$$

$$\therefore E = \frac{R^2}{2r} \frac{dB}{dt}$$

$$r < R \text{ 时, } E \cdot 2\pi r = \pi r^2 \frac{dB}{dt}$$

$$\therefore E = \frac{r}{2} \frac{dB}{dt}$$

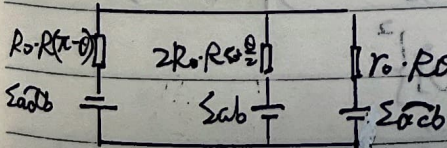


$$\Sigma_{acb} = \frac{1}{2} \pi R^2 \frac{dB}{dt}$$

$$\text{在 } \Delta abc \text{ 中, } \Sigma = \frac{d\phi}{dt} = \left(\frac{1}{2} \pi R^2 - \frac{1}{2} \pi r^2 \right) \frac{dB}{dt}$$

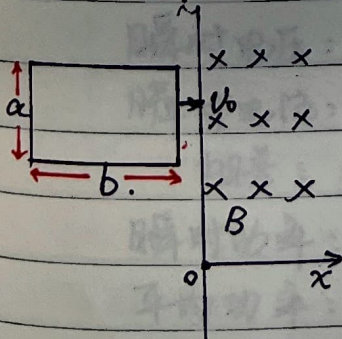
$$\therefore \Sigma_{ab} = \Sigma_{acb} - \Sigma = \frac{1}{2} \pi R^2 \frac{dB}{dt} - \frac{1}{2} \pi r^2 \frac{dB}{dt} + \frac{1}{2} \pi r^2 \frac{dB}{dt}$$

$$= \frac{1}{2} \pi r^2 \frac{dB}{dt}$$



其中: Σ 为环路 acba 的总电动势

⑥ 超导线圈进磁场 (自感 L)



$$\text{磁通量 } \Phi = B a x = L i$$

$$\text{则 } F = -B a i = m \frac{dx}{dt}$$

$$\therefore B a x + \frac{mL}{Ba} \frac{dx}{dt} = 0 \quad \text{即 } \frac{B^2 a^2}{L} x + m \frac{dx}{dt} = 0$$

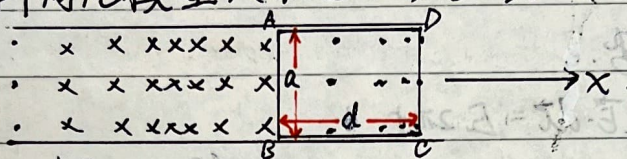
$$\therefore x = A \sin \left(\sqrt{\frac{B^2 a^2}{mL}} t \right) \quad \therefore v = \frac{dx}{dt} = A \sqrt{\frac{B^2 a^2}{mL}} \cos \left(\sqrt{\frac{B^2 a^2}{mL}} t \right)$$

$$\text{当 } t=0 \text{ 时, } v = A \sqrt{\frac{B^2 a^2}{mL}} = v_0 \quad \therefore A = v_0 \sqrt{\frac{mL}{B^2 a^2}} = \frac{v_0}{Ba} \sqrt{mL}$$

$$\therefore x = \frac{v_0 \sqrt{mL}}{Ba} \sin \left(\frac{Ba}{\sqrt{mL}} t \right) \quad v = v_0 \cos \left(\frac{Ba}{\sqrt{mL}} t \right)$$

- 1) 当 $A = \frac{v_0 \sqrt{mL}}{Ba} < b$, 即 $v_0 < \frac{Bab}{\sqrt{mL}}$ 时, 线圈做半个周期的简谐运动后折回;
 2) 当 $A = \frac{v_0 \sqrt{mL}}{Ba} = b$, 即 $v_0 = \frac{Bab}{\sqrt{mL}}$ 时, 线圈做完半个周期简谐运动后静止.
 3) 当 $A = \frac{v_0 \sqrt{mL}}{Ba} > b$, 即 $v_0 > \frac{Bab}{\sqrt{mL}}$ 时, 线圈在完成本周期简谐运动后就以
 匀速直进. $\frac{1}{2} m v_0^2 = \frac{1}{2} \frac{B^2 a^2}{L} b^2 + \frac{1}{2} m v^2$, $v = \sqrt{v_0^2 - \frac{B^2 a^2 b^2}{mL}}$

⑦ 磁悬浮列车简化模型. (轨道磁场 $B = B_0 \cos(\omega t - kx)$)



设此时线圈速度为 v , AB 边坐标为 x , 时刻为 t .

$$\begin{aligned} \therefore \varepsilon_{总} &= - \int_s \frac{\partial B}{\partial t} ds = \omega B_0 \int_x^{x+d} \sin(\omega t - kx) \cdot a dx \\ &= - \frac{\omega B_0 a}{k} \int_x^{x+d} \sin(\omega t - kx) d(\omega t - kx) \\ &= \frac{\omega B_0 a}{k} \{ \cos(\omega t - k(x+d)) - \cos(\omega t - kx) \}. \end{aligned}$$

$$\begin{aligned} \varepsilon_{动} &= [B(x, t) - B(x+d, t)] a v \\ &= B_0 a v \{ \cos(\omega t - kx) - \cos(\omega t - k(x+d)) \} \end{aligned}$$

$$\therefore \varepsilon_{总} = \varepsilon_{动} + \varepsilon_{感} = \left(\frac{B_0 a \omega}{k} + B_0 a v \right) \{ \cos(\omega t - kx) - \cos[\omega t - k(x+d)] \}$$

$$\begin{aligned} F_{总} &= [B(x+d, t) - B(x, t)] I \cdot a \\ &= -B_0 \{ \cos[\omega t - k(x+d)] + \cos(\omega t - kx) \} \left(\frac{B_0 a \omega}{k} + B_0 a v \right) \\ &= \frac{B_0^2 a^2 (\frac{\omega}{k} - v)}{R} \{ \cos(\omega t - kx) - \cos[\omega t - k(x+d)] \}^2 \end{aligned}$$

和差化积, 得 $F = \left[\frac{4B_0^2 a^2 (\frac{\omega}{k} - v)}{R} \varepsilon^2 \left(\frac{kd}{2} \right) \right] \sin^2 \left[(\omega t - kx) - \frac{kd}{2} \right] = F_0 \varepsilon^2 \left(\omega t - kx - \frac{kd}{2} \right)$

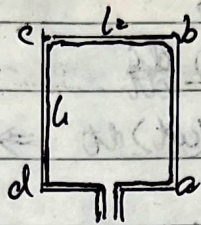
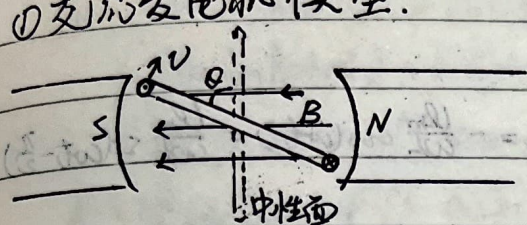
1) 当 $kd = 2n\pi$ 时, $(F_0)_{min} = 0$

2) 当 $kd = (2n+1)\pi$ 时, $(F_0)_{max} = \frac{4B_0^2 a^2 (\frac{\omega}{k} - v)}{R}$

3) 当 d 取其它值时, $F_0 \in (0, \frac{4B_0^2 a^2 (\frac{\omega}{k} - v)}{R})$

3. 交流电.

① 交流发电机模型.



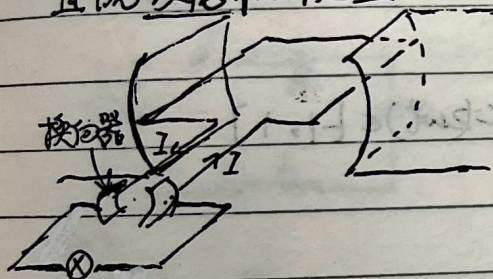
旋转电枢(线圈)式
旋转磁极式.

$$e_{\text{总}} = e_{ab} + e_{cd} = 2Blv \sin(\omega t)$$

$$= 2Bl \cdot \omega \frac{l}{2} \sin(\omega t) = Bl^2 \omega \sin(\omega t) = BS \omega \sin(\omega t) = \Phi_m \omega \sin(\omega t) = \varepsilon_m \sin(\omega t)$$

若有 n 匝线圈 $e = 2nBlv \sin(\omega t)$.

直流发电机模型:



对于直流电动机:

$$I = \frac{U - \varepsilon}{R} \quad (\varepsilon \text{ 为反电动势})$$

$$\therefore U = \varepsilon + IR \quad (U \text{ 为电源电压})$$

$$\therefore UI = \varepsilon I \text{ (机械能)} + I^2 R \text{ (热能)}$$

② 交流电有效值: 一个周期内有数值电流(直流恒定)发热量与实际相当.

根据定义, $I_{\text{有效}}^2 RT = R \int_0^T i^2 dt = R I_m^2 \int_0^T \sin^2(\omega t) dt$

$$\therefore I_{\text{有效}}^2 T = \frac{I_m^2}{\omega} \int_0^{\omega T} \sin^2(\omega t) d(\omega t) = \frac{I_m^2}{2\omega} [\omega T - \frac{1}{2} \sin(2\omega T)]$$

$$\therefore T = \frac{2\pi}{\omega} \quad \therefore \sin(2\omega T) = \sin(4\pi) = 0$$

$$\therefore I_{\text{有效}}^2 T = \frac{I_m^2}{2\omega} \cdot \omega T = \frac{1}{2} I_m^2 T$$

$$\therefore I_{\text{有效}} = \frac{I_m}{\sqrt{2}}$$

③ 纯电阻电路:

瞬时电压: $u = U_m \sin(\omega t)$.

瞬时电流: $i = \frac{U_m}{R} \sin(\omega t)$.

相差: u 与 i 同相.

瞬时功率: $P = ui = U_m I_m \sin^2(\omega t) = \frac{U_m I_m}{2} [1 - \cos(2\omega t)] = U_{\text{有效}} I_{\text{有效}} [1 - \cos(2\omega t)]$

平均功率: $\bar{P} = U_{\text{有效}} I_{\text{有效}} [1 - \cos(2\omega t)] \quad \because \cos(2\omega t) \in [-1, 1]$

$$\therefore \bar{P} = U_{\text{有效}} I_{\text{有效}}$$

④ 纯电感电路:

瞬时电压: $u_L = U_m \sin(\omega t)$.

瞬时电流: $\because u_L = -\varepsilon = L \frac{di}{dt}$

$$\therefore di = \frac{U_m}{L} \sin(\omega t) dt \Rightarrow i = -\frac{U_m}{\omega L} \cos(\omega t) = \frac{U_m}{\omega L} \sin(\omega t - \frac{\pi}{2})$$

相差: u_L 比 i 超前 $\frac{\pi}{2}$.

感抗: 令 $X_L = \omega L$, 则 $i = \frac{U_m}{X_L} \sin(\omega t - \frac{\pi}{2})$

即 $X_L = 2\pi f L$.

瞬时功率: $P = u_L i = -U_m I_m \sin(\omega t) \cos(\omega t)$

$$= -\frac{1}{2} U_m I_m \sin(2\omega t)$$

$$= -U_m I_m \sin(2\omega t)$$

平均功率: $\bar{P} = -U_m I_m \overline{\sin(2\omega t)}$

$$\because \sin(2\omega t) \in [-1, 1]$$

$$\therefore \bar{P} = 0$$

⑤ 纯电容电路:

瞬时电压: $u_C = U_m \sin(\omega t)$.

瞬时电流: $\because dq = C du_C$

$$\therefore \frac{dq}{dt} = i = C \frac{du_C}{dt} = C \omega U_m \cos(\omega t) = \frac{U_m}{\omega C} \sin(\omega t + \frac{\pi}{2})$$

相差: i 比 u_C 超前 $\frac{\pi}{2}$.

容抗: 令 $X_C = \frac{1}{\omega C}$, 则 $i = \frac{U_m}{X_C} \sin(\omega t + \frac{\pi}{2})$

即 $X_C = \frac{1}{2\pi f C}$

瞬时功率: $P = u_C i = U_m I_m \sin(\omega t) \cos(\omega t)$

$$= \frac{1}{2} U_m I_m \sin(2\omega t)$$

$$= U_m I_m \sin(2\omega t)$$

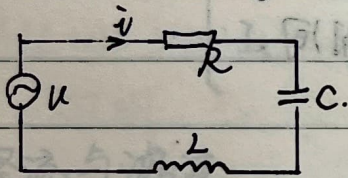
平均功率: $\bar{P} = \int_0^T P dt = 0$

⑥ 交流电功率：(设 U 比 i 超前 φ)

$$\begin{aligned}
 P &= UI = U_m \sin(\omega t) \cdot I_m \sin(\omega t - \varphi) \\
 &= U_m I_m [\sin(\omega t) \cdot \sin(\omega t) \cos \varphi - \sin(\omega t) \cos(\omega t) \sin \varphi] \\
 &= U_m I_m \cos \varphi \cdot \frac{1}{2} [1 - \cos(2\omega t)] - U_m I_m \sin \varphi \cdot \frac{1}{2} \sin(2\omega t) \\
 \bar{P} &= \frac{1}{2} U_m I_m \cos \varphi [1 - \cos(2\omega t)] - \frac{1}{2} U_m I_m \sin \varphi \sin(2\omega t) \\
 &= \frac{1}{2} U_m I_m \cos \varphi = U_{\text{eff}} I_{\text{eff}} \cos \varphi.
 \end{aligned}$$

⑦ 阻抗 (Z)

1) RCL 串联:



由于串联, 各元件电流矢量相同.

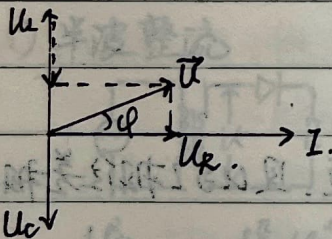
电压矢量满足 $\vec{U} = \vec{U}_R + \vec{U}_L + \vec{U}_C$, 如图

$$|\vec{U}| = \sqrt{U_R^2 + (U_L - U_C)^2}$$

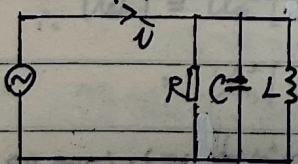
$$= \sqrt{(IR)^2 + (I\omega L - I\frac{1}{\omega C})^2}$$

$$= I \sqrt{R^2 + (\omega L - \frac{1}{\omega C})^2}$$

$$\therefore Z = \frac{U}{I} = \sqrt{R^2 + (\omega L - \frac{1}{\omega C})^2} \quad \text{其中, } U, I \text{ 皆为有效值.}$$



2) RCL 并联:



由于并联, 各元件电压矢量相同.

电流矢量满足 $\vec{i} = \vec{i}_R + \vec{i}_C + \vec{i}_L$, 如图.

$$|\vec{i}| = \sqrt{i_R^2 + (i_C - i_L)^2}$$

$$= \sqrt{(\frac{U}{R})^2 + (\frac{U}{\omega C} - \frac{U}{\omega L})^2}$$

$$= U \sqrt{\frac{1}{R^2} + (\frac{1}{\omega C} - \omega C)^2}$$

$$\therefore Z = \frac{U}{i} = \left[R^2 + (\frac{1}{\omega C} - \omega C)^2 \right]^{-\frac{1}{2}} \quad \text{其中, } U, i \text{ 为有效值.}$$

3) 串联谐振:

$$\varphi = \arctg \frac{U_C - U_L}{U_R} = \arctg \frac{\omega L - \frac{1}{\omega C}}{R}$$

当 $\omega L - \frac{1}{\omega C} = 0$, 即 $\omega = \sqrt{\frac{1}{LC}}$ 时, 发生串联谐振。

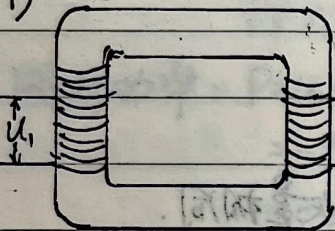
4) 并联谐振:

$$\varphi = \arctg \frac{U_C - U_L}{U_R} = \arctg \frac{\omega C - \frac{1}{\omega L}}{R}$$

当 $\omega C - \frac{1}{\omega L} = 0$, 即 $\omega = \sqrt{\frac{1}{LC}}$ 时, 发生并联谐振。

⑧ 变压器

1)



原线圈外加电压 $U_1 = U_m \sin(\omega t)$,

当 U_1 随时间作周期变化时, 铁芯中相应产生变化的磁通量, 由于铁芯完全导磁 (理想) 原副线圈中 $\frac{d\Phi}{dt}$ 相同。

$$\text{原线圈中感应电动势 } \mathcal{E}_1 = U_1 - I_1 R_1, \quad \mathcal{E}_2 = U_2$$

$$\because R_1 \text{ 很小, } \therefore \mathcal{E}_1 \approx U_1$$

$$\text{又 } \because \mathcal{E}_1 = N_1 \frac{d\Phi}{dt}, \quad \mathcal{E}_2 = N_2 \frac{d\Phi}{dt}$$

$$\therefore \frac{\mathcal{E}_1}{\mathcal{E}_2} = \frac{N_1}{N_2} = \frac{U_1}{U_2}$$

又: 理想状态下, 原副线圈中电流功率不变, 且 U 与 I 相位差相同。

$$\therefore U_1 I_1 \cos \varphi_1 = U_2 I_2 \cos \varphi_2$$

$$\therefore \frac{I_1}{I_2} = \frac{U_2}{U_1} = \frac{N_2}{N_1}$$

若有多个副线圈, 由能量守恒: $U_1 I_1 = \sum_{i=1}^n U_i I_i$

$$\therefore \frac{U_1}{N_1} = \frac{U_2}{N_2} \quad \therefore N_1 I_1 = \sum_{i=1}^n N_i I_i$$

由副线圈连接的部分, 相当于一阻抗, 可通过调整这部分电路的总阻抗, 达到原线圈连接部分的阻抗匹配。

$$\therefore R' = \frac{U_1}{I_1}, \quad R = \frac{U_2}{I_2}$$

$$\text{而 } \frac{U_1}{U_2} = \frac{N_1}{N_2}, \quad \frac{I_1}{I_2} = \frac{N_2}{N_1}$$

$$\therefore R' = \left(\frac{N_1}{N_2}\right)^2 R; \text{ 即等效电阻。}$$

